

7664 – 10 Street N.E. Calgary, Alberta T2E 8W1 Tel (24hr): 403 295-5855 Fax: 403 571-6187 Toll-free:1 800 555-9439

www.startec.ca

TO WHOM IT MAY CONCERN:

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GASFRAC ENERGY SERVICES P.O. 014932

5 mmscfd Trailer Mounted Dewpoint Plant 250 HP Marathon / Howden XRV 204/193

SERIAL NO. DPC-1002



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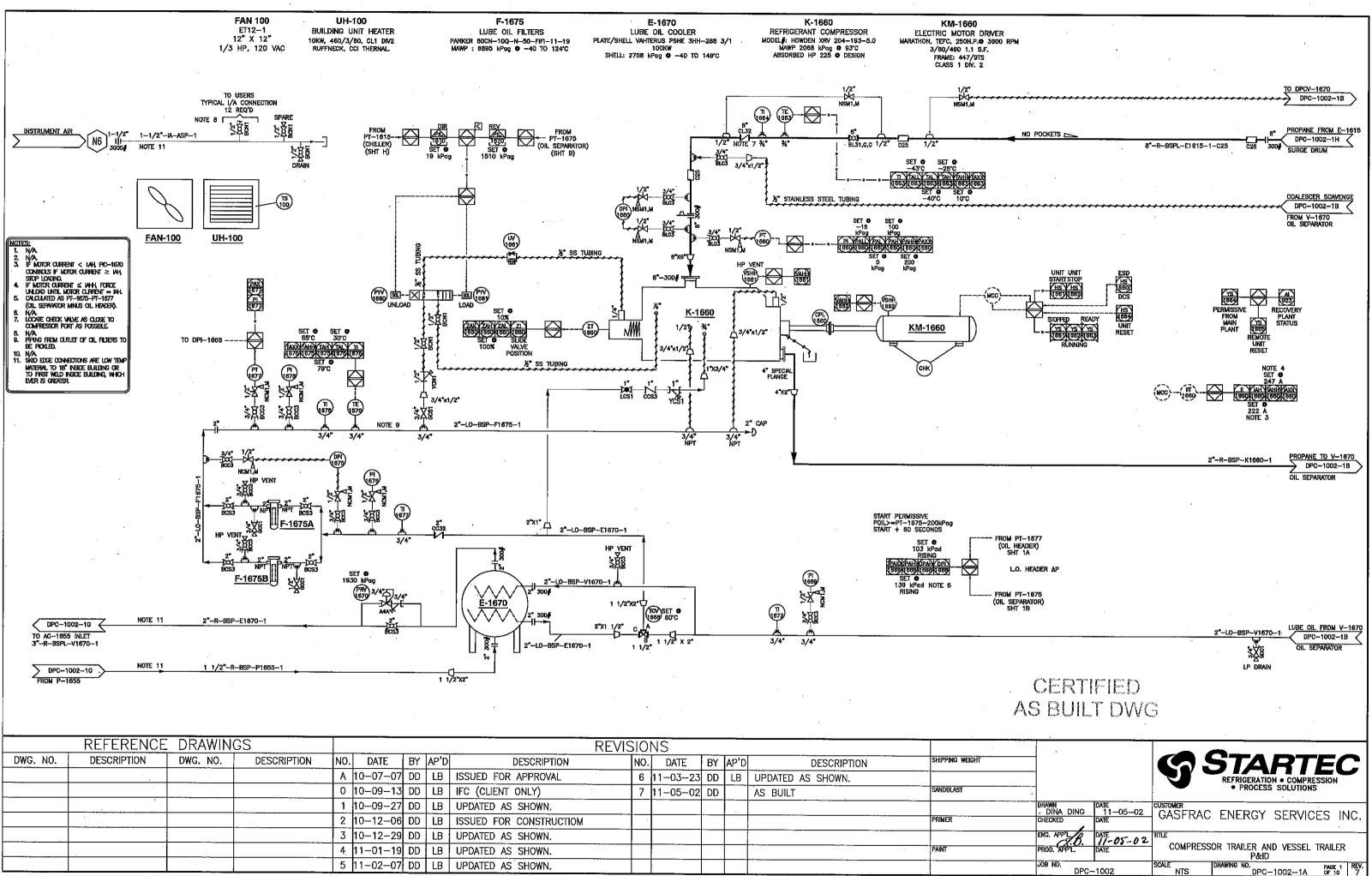
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5 mmscfd Trailer Mounted Dewpoint Plant 250 HP Marathon / Howden 204/193

SERIAL NO. DPC-1002

OPERATING MANUAL

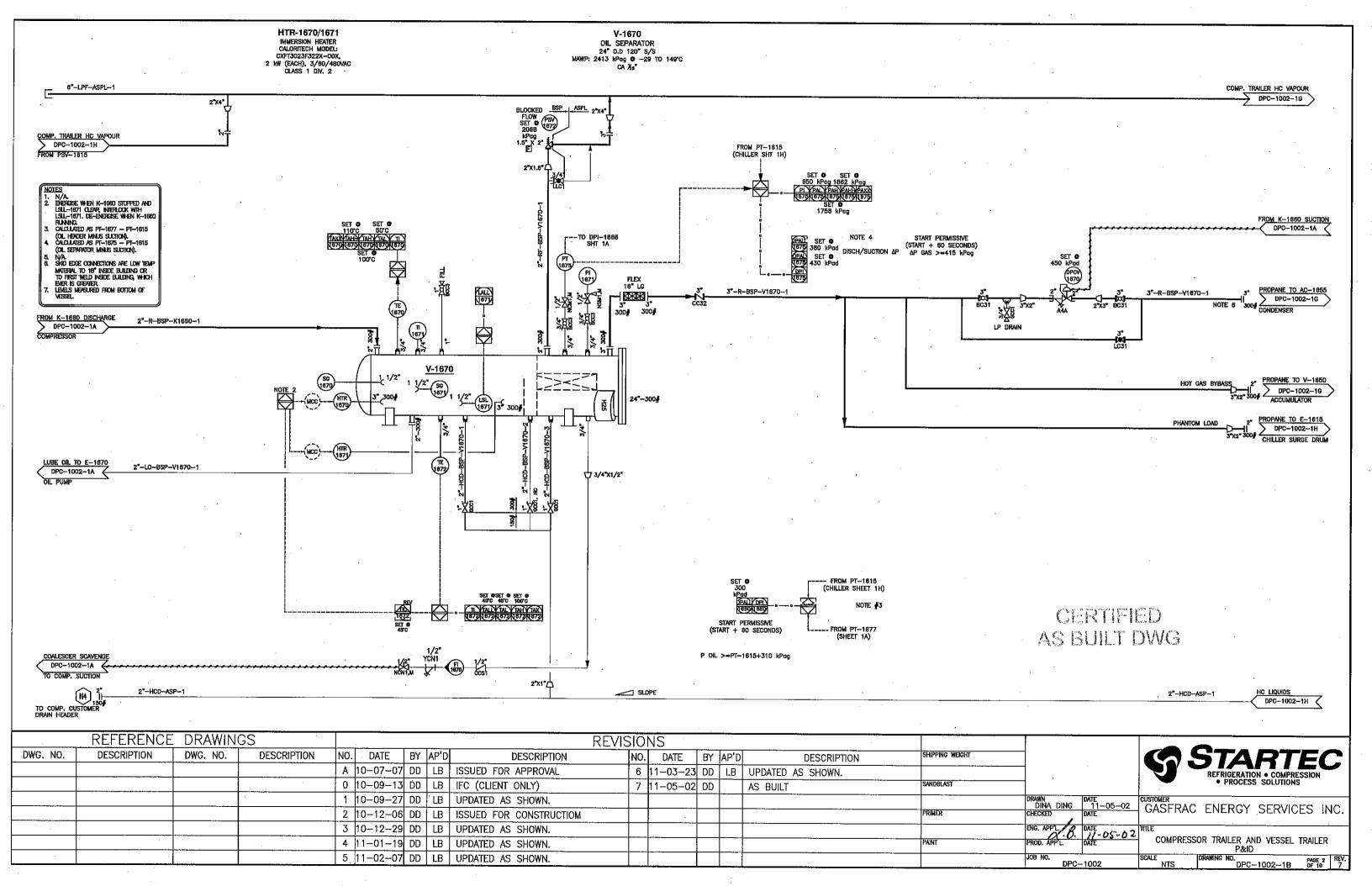
Volume 1
Volume 1
Volume 2
Volume 2

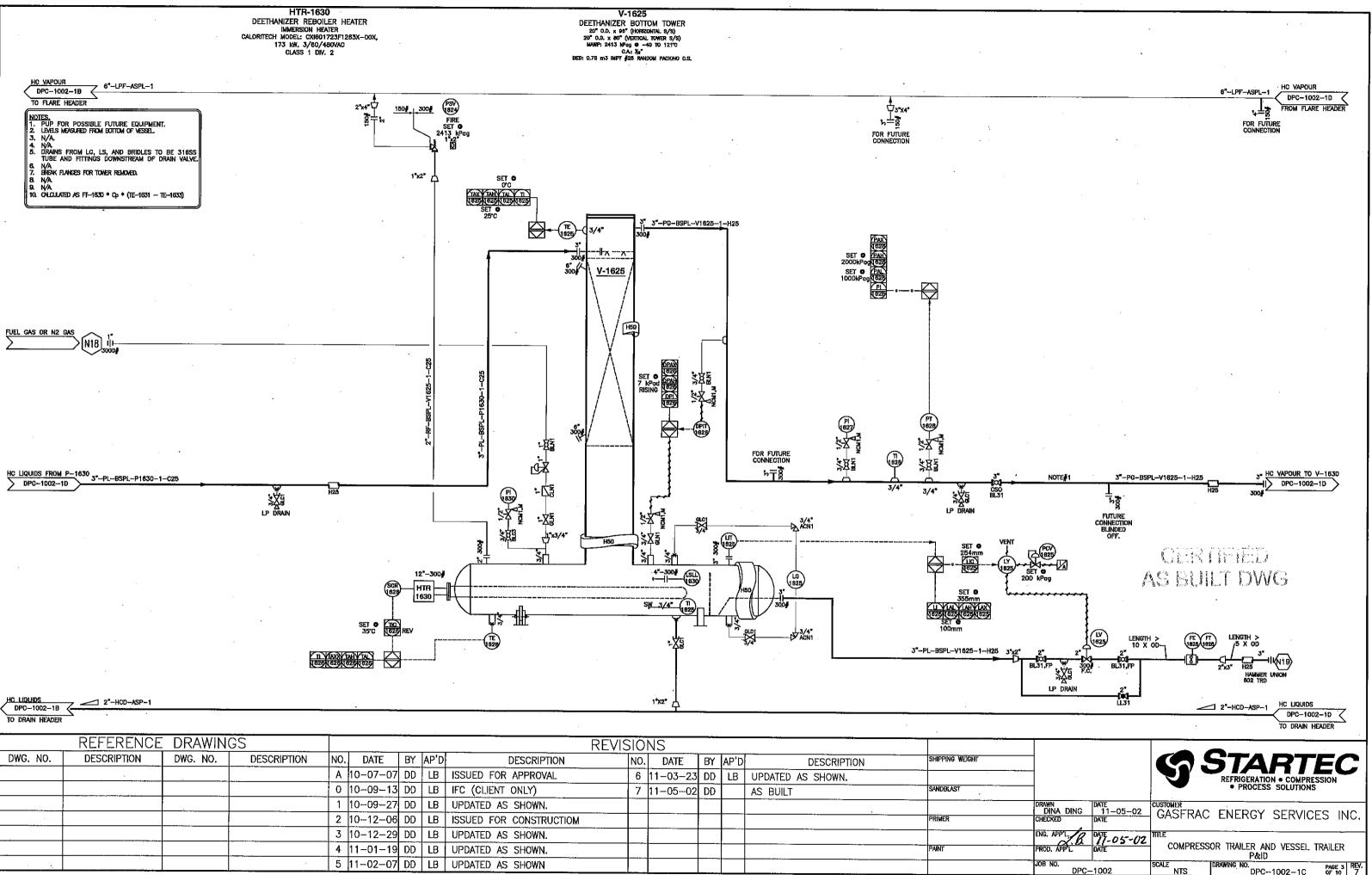


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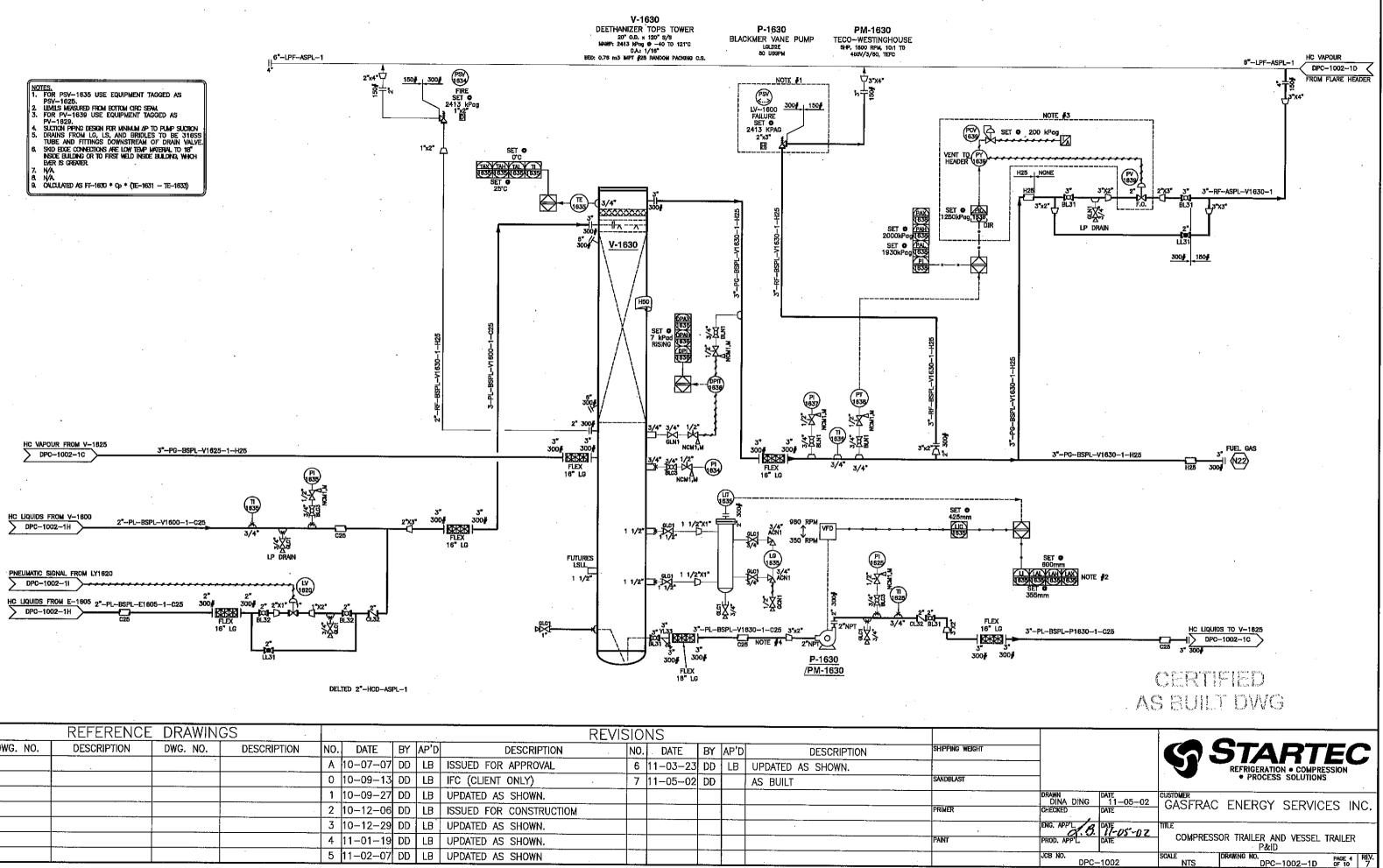
DPC-1002-1A

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DWG. NO.	DESCRIPTION	DWG, NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION		NO.	DATE	BY	AP'D	DESCRIPTION	Shipping Weight
				Α	10-07-07	DD	LB	ISSUED FOR APPROVAL		6	11-03-23	DD	LB	UPDATED AS SHOWN.	
	,			0	10-09-13	DD	LB	IFC (CLIENT ONLY)		7	11-05-02	DD		AS BUILT	SANDBLAST
				1	10-09-27	DD	LB	UPDATED AS SHOWN.							
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM							PRIMER
				3	10-12-29	DD	LB	UPDATED AS SHOWN.							
				4.	11-01-19	DD	LB	UPDATED AS SHOWN.							PAINT
				5	11-02-07	DD	LB	UPDATED AS SHOWN.							

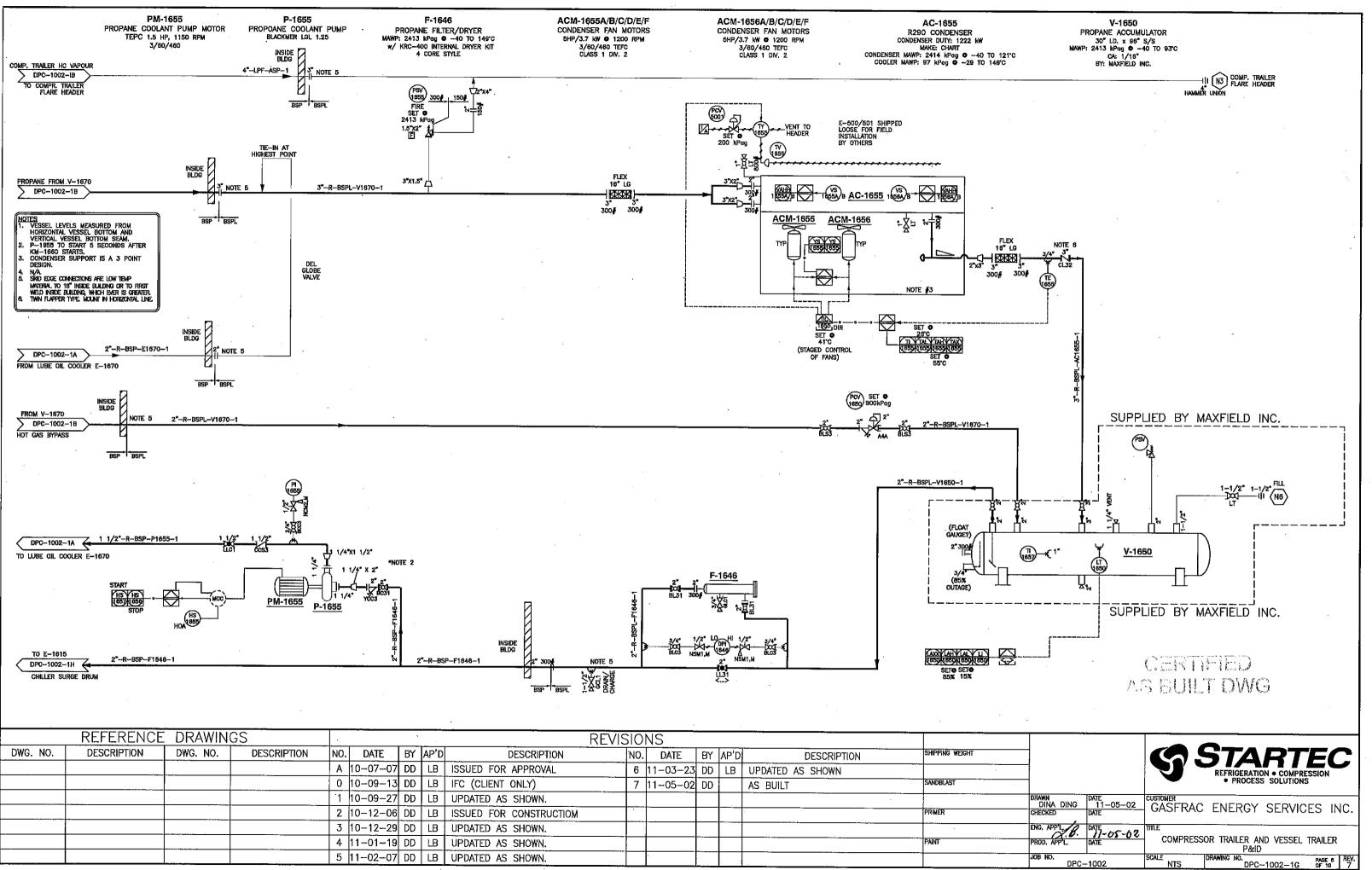




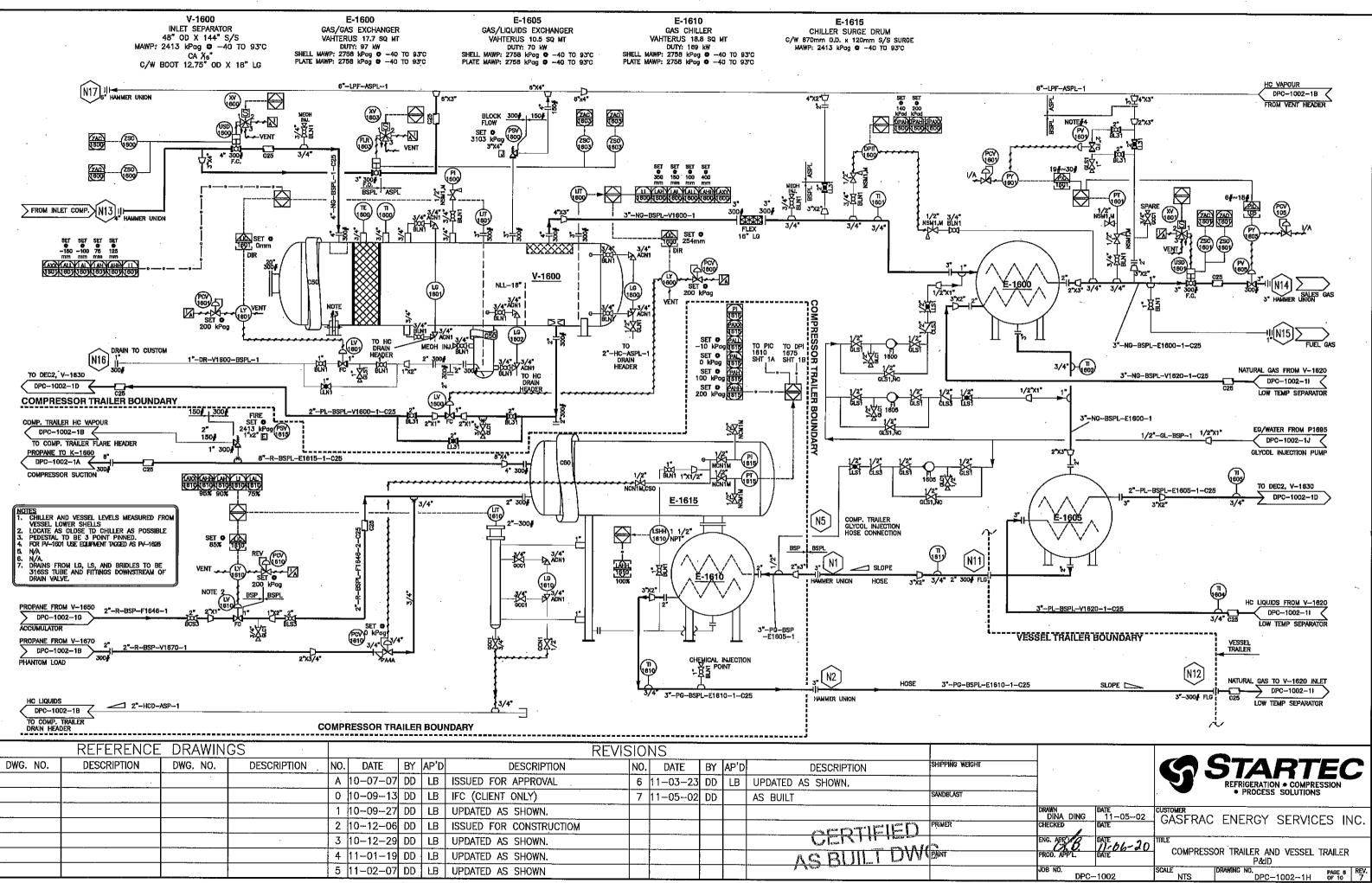
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DWG. NO.	DESCRIPTION	DWG. NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
	· · · · · · · · · · · · · · · · · · ·		wi.w	A	10-07-07	DD	LB	ISSUED FOR APPROVAL	6	11-03-2	3 DD	LB	UPDATED AS SHOWN.	
				0	100913	DD	LB	IFC (CLIENT ONLY)	7	11-05-0	2 DD		AS BUILT	SANDBLAST .
				1	10~09-27	DD	LB	UPDATED AS SHOWN.						
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM					······································	PRIMER
				3	10-12-29	DD	LB	UPDATED AS SHOWN.						
				4	11-01-19	DD	LB	UPDATED AS SHOWN.			<u> </u>	-		PAINT
				5	11-02-07	DD	LB	UPDATED AS SHOWN		*				

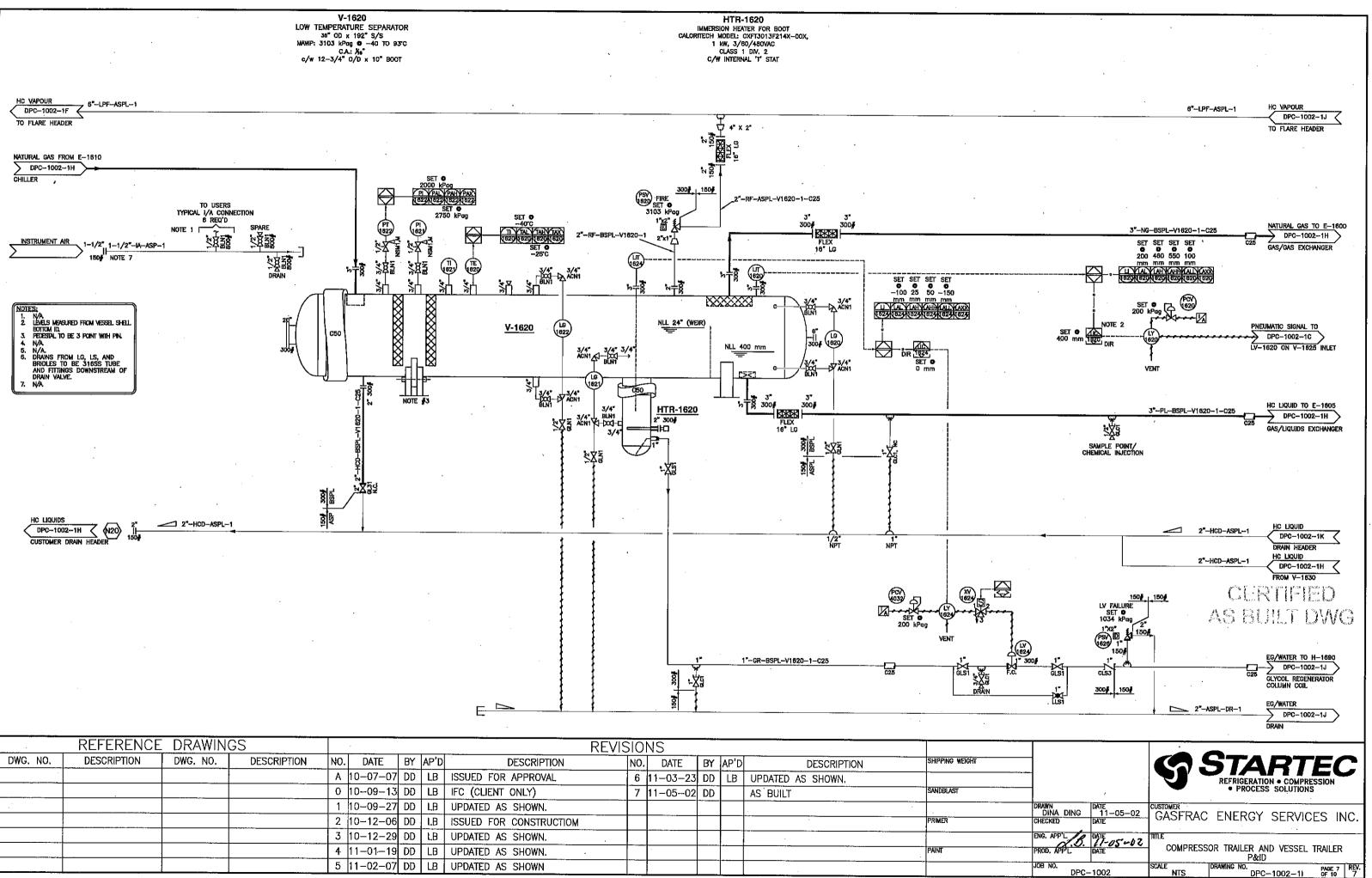


	REFERENCE	DRAWING	<u> SS</u>				-	R	REVIS	sioi	٧S	-		· · · · · · · · · · · · · · · · · · ·	····
DWG. NO.	DESCRIPTION	DWG, NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION		NO.	DATE	BY	AP'D	DESCRIPTION	Shipping Weight
					0-07-07					6	11-03-23	DD	LB	UPDATED AS SHOWN.	
	í.			0 1	0-09-13	DD	LB	IFC (CLIENT ONLY)		7	11-05-02	DD		AS BUILT	SANDBLAST
				1 1	0-09-27	DD	LB	UPDATED AS SHOWN.				*			
				2 1	0-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM						· · · · ·	PRIMER
				3 1	0-12-29	DD	LB	UPDATED AS SHOWN.							
				4 1	1-01-19	DD	LB	UPDATED AS SHOWN.							PAINT
				5 1	1-02-07	DD	LB	UPDATED AS SHOWN							

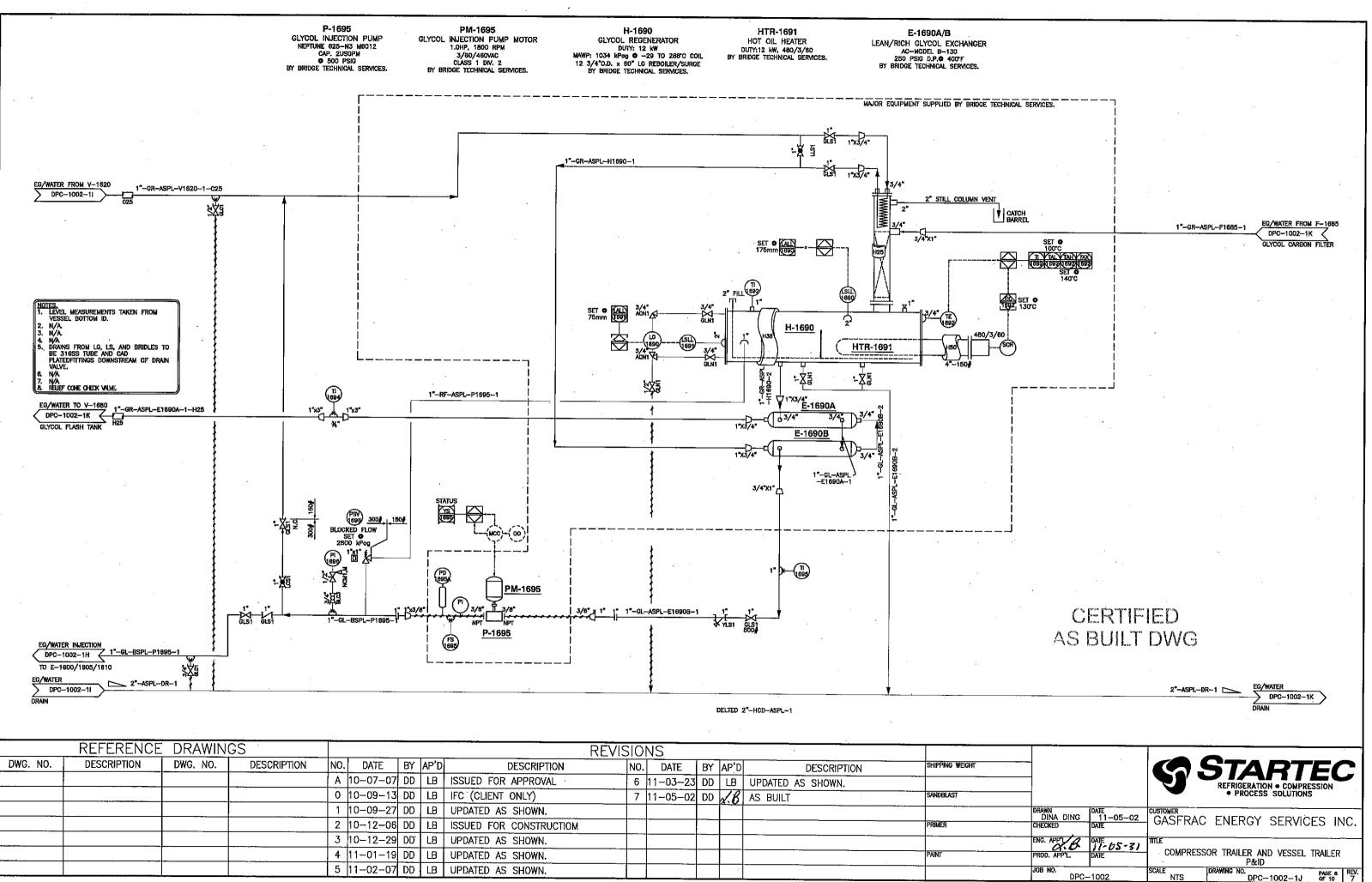


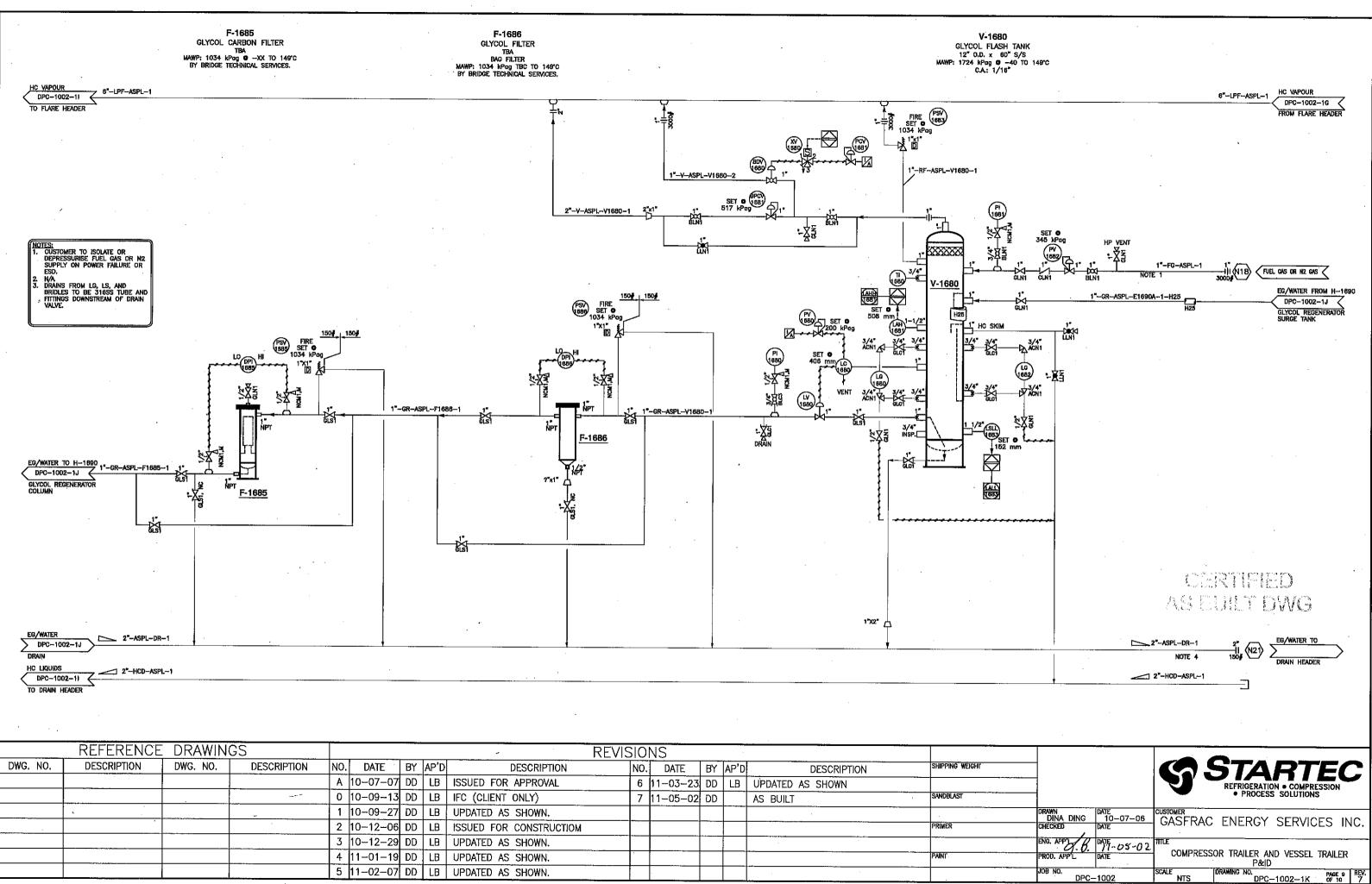
	REFERENCE	GS			,		REV	/ISIO	NS					
DWG. NO.	DESCRIPTION	DWG, NO,	DESCRIPTION	NO,	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
				A	10-07-07	DD	LB	ISSUED FOR APPROVAL	6	11-03-23	DD	LB	UPDATED AS SHOWN	
				0	10-09-13	DD	LB	IFC (CLIENT ONLY)	7	11-05-02	DD		AS BUILT	SANDBLAST
		· .		1	10-09-27	DD	LB	UPDATED AS SHOWN.						
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM	,					PRIMÉR
				3	10-12-29	DD	LB	UPDATED AS SHOWN.						· ·
				4	11-01-19	DD	LB	UPDATED AS SHOWN.						PAINT
				5	11-02-07	DD	LB	UPDATED AS SHOWN.						





	REFERENCI	GS					REV	SIO	NS					
DWG. NO.	DESCRIPTION	DWG, NO,	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
·								ISSUED FOR APPROVAL	6	11-03-23	5 DD	LB	UPDATED AS SHOWN.	
				0	1009-13	DÐ	LB	IFC (CLIENT ONLY)	7	11-05-02	2 DD		AS BUILT	SANDBLAST
				1	10-09-27	DD	L.B	UPDATED AS SHOWN.						· .
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM						PRIMER
				3	10-12-29	DD	LB	UPDATED AS SHOWN.						
				4	11-01-19	DD	LB	UPDATED AS SHOWN.				1		PAINT
				5	11-02-07	DD	LB	UPDATED AS SHOWN						, , , ,, , ,, , ,, , ,, , , , , , , , , , , , , , , , , , , ,





	REFERENCE	DRAWING	GS					- RE'	/ISI0I	٧S				
DWG. NO.	DESCRIPTION	DWG. NO,	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
				A	10–07–07	DD	LB	ISSUED FOR APPROVAL	6	11-03-23	ĐD	LB	UPDATED AS SHOWN	
				0	10-09-13	DD	LB	IFC (CLIENT ONLY)	7	11-05-02	DD		AS BUILT	SANDBLAST
	•		L.F.	1	10-09-27	DD	LB	UPDATED AS SHOWN.					· · · ·	
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM						PRIMER
				3	10-12-29	DD	LB	UPDATED AS SHOWN.						
				4	11-01-19	DD	LB	UPDATED AS SHOWN.	ľ					PAINT
				5	11-02-07	DD	LB	UPDATED AS SHOWN.					- u- .	

DPC-1002

NTS

DPC-1002-1K

INSTRUMENT		CATION - SECOND AND SUCCEEDING LETTER	\$		SELF ACTUATED VALVES	CONTROL VALVES		
IDENTIFICATION PRIMARY READ OUT FIRST LETTER ELEMENT DEVICES	TRANSMITTERS CONTROLLERS FINAL ELEMENT T. IT DT IC C CV V	ALARMIS SH A AL ALL AH AHH S SL SLL	TCHES SH SHH Y Q	MISCELLANEOUS	BPV		PIPING LINE SYMBOLS	LINE COMMODITY CODE
			S S			CONTROL VALVE (TWO WAY)		AGF ACID GAS FLARE NID AMINE DRAIN
MEASURED/ CONTROLLED	5 5 7 5 8 8 8 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		UN UN		SELF CONTAINED	CONTROL VALVE		MIL LEAN AMINE MIR RICH AMINE
VARIABLE SALIDA		R HSH R	HIGH DUCE		PCV	WITH HANDWHEEL		BD BLOWDOWN BFW BOILER FEED WATER
	Indexemple Indexemple		HIGH HIGH	AFET	PRESSURE REGULATOR	CONTROL VALVE		BG BLANKET GAS CA COMBUSTION AIR
ANALYZER AE AR AI	AT AIT ARC AIC AC			N0 >0	SELF CONTAINED		PIGGING BALL VALVE	CD CLOSED DRAIN
BURNER BE BR BI		BA		BG	PSV BLOCKED FLOW			CH HIGH PRESSURE STEAM CONDENSATE CL LOW PRESSURE STEAM CONDENSATE
DENSITY OR SP. GR. DE DR DI VOLTAGE EE	ERC EIC EC	EA	EY		SIZE: 33x48 SF: 9930 kPa	DOUBLE ACTING		CH MED. PRESSURE STEAM CONDENSATE CW COOLING WATER
	FT FIT FDT FRC FIC FC FCV FV		SH FSHH FY FQ	FG	PRESSURE SAFETY VALVE	CONTROL VALVE		DR DRAIN DW DRINKING WATER (POTABLE)
HAND CURRENT IE IR II		IA			OR PRESSURE RELIEF VALVE WITH QUALIFIER	(HCV)		EX EXHAUST GAS FG FUEL GAS
POWER JE JR JI TIME KE KR KI	KT KIT KRC KIC KC	JA	KY		<u>→</u> 妤#			FO FUEL OIL FRP FIBREGLASS REINFORCED PLASTIC
MOISTURE OR HUMIDITY ME MR MI	LT LIT LDT LIC LIC LCV LV	LA LAL LALL LAH LAHH LSL LSL MAL MAL MAH	SH LSHH LY		VACUUM RELIEF VALVE			FW FIRE WATER G GLYCOL
					PVSV	r ⁺ (− [×])		GL GLYCOL LEAN
QUANTITY QE QR QI		PA PAL PALL PAH PAHHI PSL PSL T	SH PSHH PY	PSV		DIAPHRAGM OPERATED VALVE		GR GLYCOL REGENERATION
RADIATION RE RR RI SPEED SE SR SI	ST SIT SRC SIC SC					(-Y) [5] 3 WAY	BLINDED CONNECTION	HCD HYDROCARBON DRAIN HMR HEAT MEDIUM RETURN
MULTIVARIABLE	TT THE TDT TRC TIC TC TCV TV		SH TSHH TY		RELIEF VALVE	SoleNoid WALVE		HMS HEAT MEDIUM SUPPLY HPF HIGH PRESSURE FLARE
WBRATION VE VR VI WEIGHT WE WR WI						TYPICAL THREE-WAY SOLENOID	INSULATION	HS HIGH PRESSURE STEAM
					W/ EXTERNAL SENSING	INSTALLATION (FAIL OPEN)		5 JN JACKET WATER
GENERAL SYMBOLS	ZT ZIT ZRC ZIC ZC ZCV ZV FLOW DIAGRAM SYMBOLS						Inacing	G UF LOW PRESSURE FLARE
PRIMARY LINE		LOGIC SUBSCRIPTS & SYMBOLS		LANEOUS	FLOW METERS	ACTUATORS	Y TYPE STRAINER	LS LOW PRESSURE STEAM
	(XXX) LOCAL MOUNTED DEVICE	LOW SIGNAL SELECTOR				$ \begin{array}{ccc} FO &= FAIL OPEN \\ \hline KI & FC &= FAIL CLOSED \\ FO & FI &= FAIL LAST POSITION \end{array} $	CONE TYPE STRAINER	WS MEDIUM PRESSURE STEAM
SECONDARY LINE			VIBR	ATION DAMPENER	TURBINE METER			N NITROGEN P INCOMING STREAM (GAS, EUKILSION, OIL)
PACKAGED EQUIPMENT BOUNDARY	XXX REMOTE MOUNTED DEVICE: XXX CONTROL ROOM PANEL	HIGH SIGNAL SELECTOR			(FE)	DOUBLE ACTING SOLENOID VALVE	(WELDED)	P0 PROCESS OIL PG PROCESS HYDROCARBON GAS
	XXX REMOTE MOUNTED DEVICE: XXX LOCAL PANEL		PURC	GE OR FLUSHING DEVICE			D WELD CAP.	PGS SOUR PROCESS GAS PL PROCESS LIQUIDS
EXISTING	LOCAL PANEL	GENERALIZED FOR DEFINED OR COMPLEX INTERLOCK LOGIC		CONTINUATION SYMBOL	METER	ELECTRIC SOLENOID		PLS SOUR PROCESS LIQUIDS PS SOUR PROCESS
INSTRUMENT LINE SYMBOLS	XXX ALARM ANNUNCIATION; XXXX CONTROL ROOM PANEL		DRAM	Cating Reference Wing Where Line or RUMENT SIGNAL IS	RO			PU PURGE GAS
ELECTRONIC SIGNAL		SIGNAL CONDITIONER		TINUED	FIXED RESTRICTION	S VALVE OPERATOR ?w?/ MANUAL RESET		R REFRIGERANT (PROPANE, ETC.)
-00- DATA LINK	ALARM ANNUNCIATION;			CONTINUATION ON	(FE)	FTT FTTT LATCH TYPE ACTUATOR	ADJUSTABLE RESTRICTION ORIFICE	RF RELIEF FLARE RW RAW WATER (WELL/RIVER WATER)
	^		SAME	E DRAWING		S-R MANUAL RESET	SAMPLE CONNECTION	SRF SOUR RELIEF FLARE SA START AIR
PNEUMATIC SIGNAL	ESD INTERLOCK W/ ESD LOGIC	SIGNAL CONDITIONER		PERATURE INDICATOR	TE		▲ VENT OR DRAIN	SG START GAS
X X X CAPILLARY TUBING	INTERLOCK W/ SD LOGIC			RMOWELL	Υ.	EQUIPMENT TAGS	150 300 ANSI SPECIFICATION BREAK	TW TREATED WATER (DEMINERALIZED)
L L HYDRAULIC SIGNAL	SD INTERLOCK W/ SD LOGIC				VENTURI FLOW ELEMENT			UW UTILITY WATER V VENTS/FLARE LINES
GENERAL NOTES	RTU OR PLC CONTROL/LOGIC CONTROL/PANEL	EXAMPLES		in tag number		B AIR BLOWER OR FAN (PROCESS) BH BUILDING HEATER	CC CORROSION COUPON ASSEMBLY	
POWER SUPPLY DESIGNATIONS: W - INSTRUMENT AIR				RUMENT GAS SUPPLY	(F) LOCAL FLOW INDICATOR	BF BUILDING FAN D ENGINE		PIPING CLASS
ES - ELECTRICAL SUPPLY GS - GAS SUPPLY INS - INTERVIEW, SUPPLY	RTU OR PLC CONTROL/LOGIC CONTROL ROOM PANEL	DIGITAL		NOMENT ONS SOFFEI	(FE)	E HEAT EXCHANGER INCLUDING AERIAL COOLERS		S A 150 ANSI L 125# B 300 ANSI W 150#
hs — hydraulic supply hs — nitrogen supply	: CONTROL ROOM PANEL			RUMENT AIR SUPPLY		F FILTER FS FLARE STACK		L C 600 ANS!
	IGNATIONS					G GENERATOR (ELECTRIC) H FIRED HEATER OR BOILER	E CAMLOCK FITTING	S D 900 ANSI S E 1500 ANSI
89-PL-M-XXX-25H-ET T T T T T HEAT TRAC	DE (GT-GLYCOL, ET-ELECTRICAL, OT-HOT OIL,			AY NOZZLE		I INCINERATOR K COMPRESSOR	HPV High Point Vent	E F 2500 ANSI
STSTEAM 7		ANALOG				P PUMP R REACTOR OR CONVERTER		S A −29' to +150°C
J-JACKETED LI	NES, G-GUT LINES)			HING VALVE (AMOT)	· · · · · · · · · · · · · · · · · · ·	T TOWER V VESSEL	LOW POINT DRAIN	∑ B -29' to +260°C ↓ C -45' to +260°C
LINE SEQUENCE NU	WBER					M MOTOR		5 5 -29" to +260"C SOUR SERVICE
PIPING CLASS (see ei LINE COMMODITY CODE			1 1			TK TANK		S - 45" to +260"C SOUR SERVICE & COLD TEMP MATERIAL TO BE USED
LINE SIZE (0.D. in mm)	· · · · · · · · · · · · · · · · · · ·		JL	·				OUTDOORS
REFERENCE DRAV	VINGS	······	RE	VISIONS				
DESCRIPTION DWG. N	and the second sec		CRIPTION	NO. DATE	BY AP'D DESCRIPTI	ON SHIPPING WEIGHT		
	· · · · · · · · · · · · · · · · · · ·	-07-07 DD LB ISSUED FOR AF			DD LB UPDATED AS SHOWN.			REFRIGERATION COMPRESSION
· · · · · · · · · · · · · · · · · · ·		-09-13 DD LB IFC (CLIENT ON		7 11-05-02	DD AS BUILT	SANDELAST		PROCESS SOLUTIONS
		-09-27 DD LB UPDATED AS SH					DINA DING 11-05-02 (NOMER BASFRAC ENERGY SERVICES I
		-12-06 DD LB ISSUED FOR CC				PRIMER		
		-1229 DD LB UPDATED AS SI -0110 DD LB UPDATED AS SI				PAINT	ENG. APP'L. DATE PROD. APP'L. DATE	E COMPRESSOR TRAILER AND VESSEL TRAILER
		-0110 DD LB UPDATED AS SH	17314/NI '					

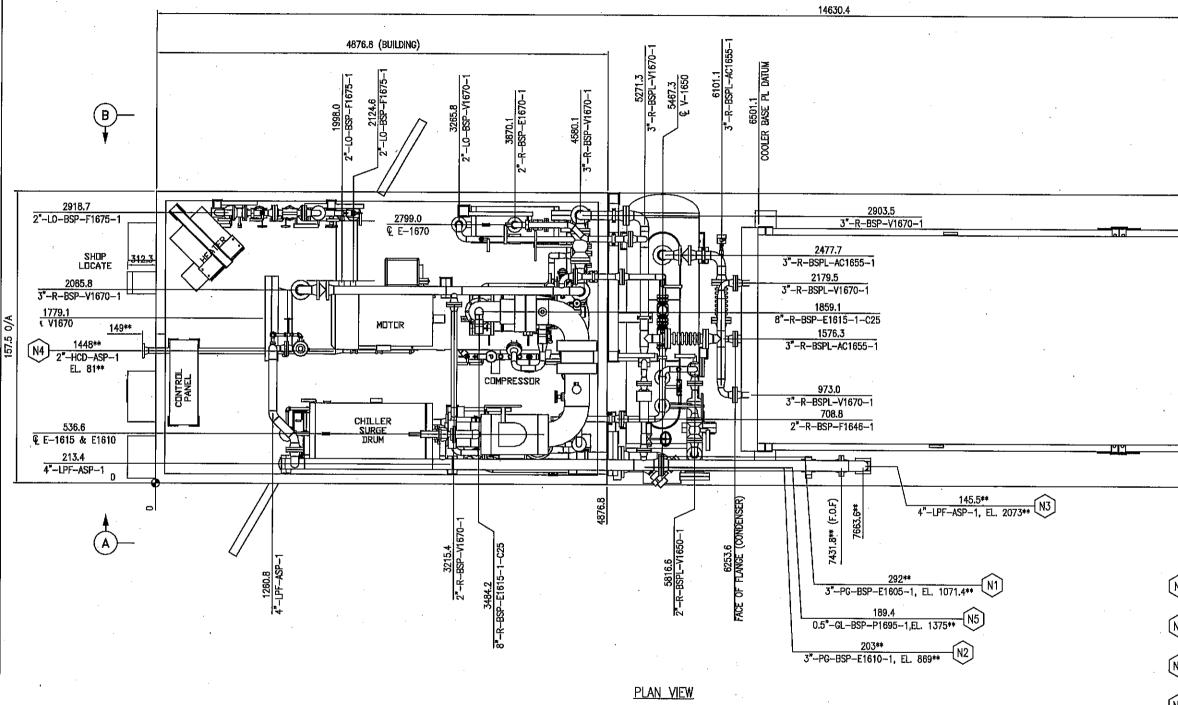
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	REFERENCE	DRAWIN	GS					REV	'ISIO	NS			· · · · · · · · · · · · · · · · · · ·	
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								ISSUED FOR APPROVAL	6	11-03-23	DD	LB	UPDATED AS SHOWN.	
				0	10-09-13	i DD	LB	IFC (CLIENT ONLY)	7	110502	DD		AS BUILT	SANDELAST
				1	10-09-27	' DD	LB	UPDATED AS SHOWN.						
				2	10-12-06	DD	LB	ISSUED FOR CONSTRUCTIOM						PRIMER
				3	10-12-29	DD	LB	UPDATED AS SHOWN.						
				4	11-01- 1 0	DD	LB	UPDATED AS SHOWN.						PAINT
-				5	11-0207	ÐD	LB	UPDATED AS SHOWN.					5100	

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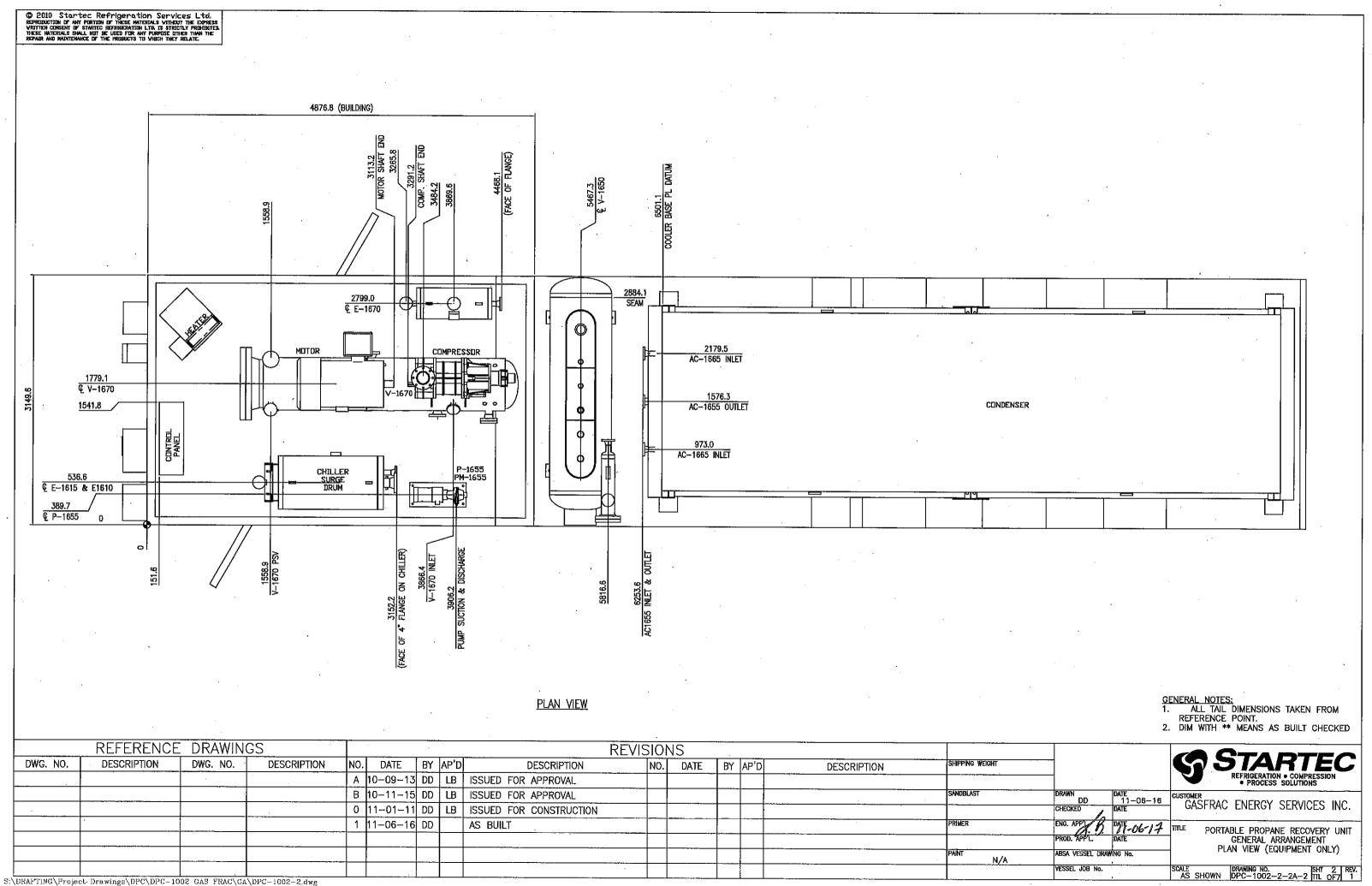
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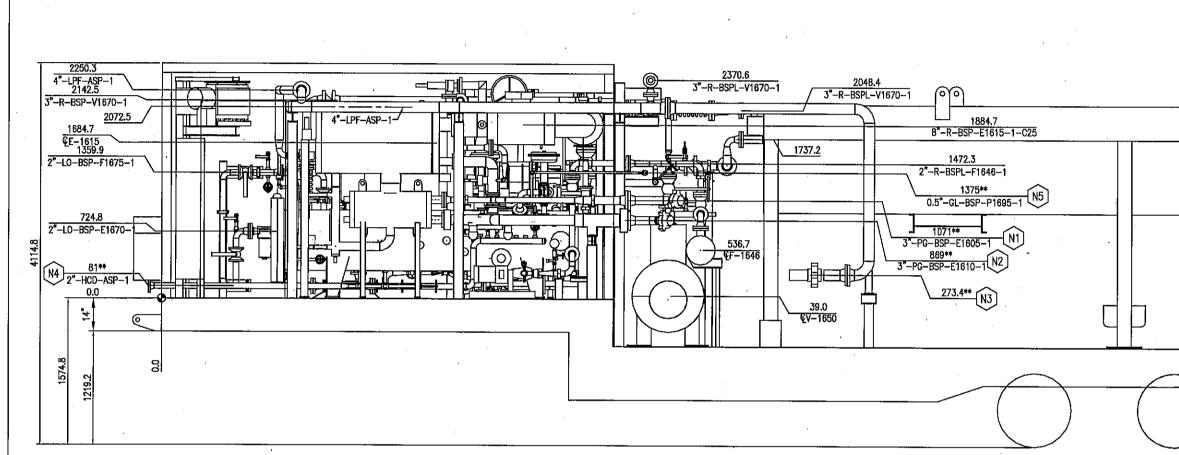
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	REFERENCE	<u>DRAWIN</u>	GS					RE	VISION	1S				
DWG, NO.	DESCRIPTION	DWG. NO.	DESCRIPTION	NO,	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
				A	10-09-13	5 DD	LB	ISSUED FOR APPROVAL					·······	
				В	10-11-15	5 DD	LB	ISSUED FOR APPROVAL	,					SANDBLAST
				0	11-01-1	I DD	LB	ISSUED FOR CONSTRUCTION	·				······································	
	`			1	11-6-16	DD		AS BUILT						PRIMER
													······································	
				_										PAINT

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		SCHEDU	<u>ILE</u>			
N1 E-	CL.300 HAMME 1605 TD E-161 , 1071.4**	R UNILIN 10	N5	1" UNION GLYCOL I EL, 1375*		
N2] 3'	CL.300 HAMME 1610 TD V-16	R UNION				
✓ EL	. 869 ** CL.150 HAMME			-	,	
N3 FL	ARE HEADER	Gi	ENERAL N	OTES:		
	CL.150 RF	1.	REFERE	NCE POIN	NSIONS TAK T.	EN FROM
	., 81**	2.	, son M			
		<u> </u>	6	ST		TEC
	-		V	REFRIC P	GERATION • CO ROCESS SOLU	MPRESSION
	DRAWN DD CHECKED	DATE 11-06-16 DATE	customer GASF	RAC ENE	ERGY SER	VICES INC.
	ENG. APP'L	PMF-06-17	TTTLE F	ORTABLE F	PROPANE RE	COVERY UNIT
٠	PROD. APP'L.	DAIL	-		RAL ARRANG	EMENT
	VESSEL JOB No.		SCALE AS SHO	WN DPC-	ig No. 1002-2-2A	-1 JTL OF7 1





ELEVATION A-A VIEW

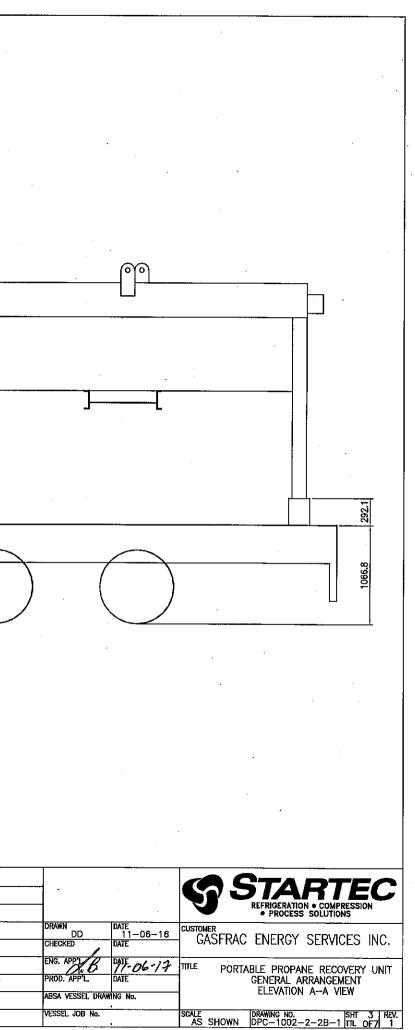
GENERAL NOTES:

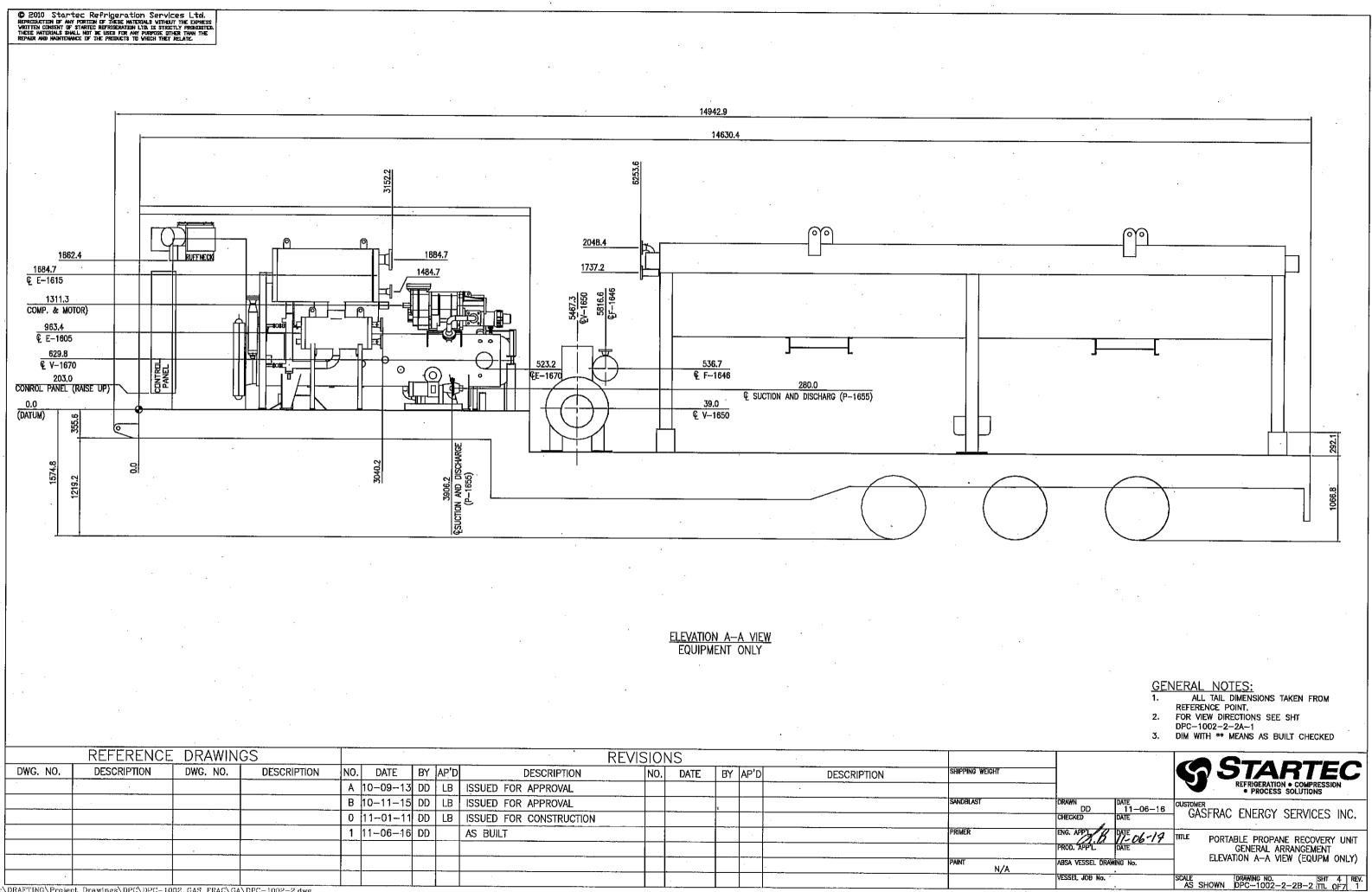
1. ALL TAIL DIMENSIONS TAKEN FROM

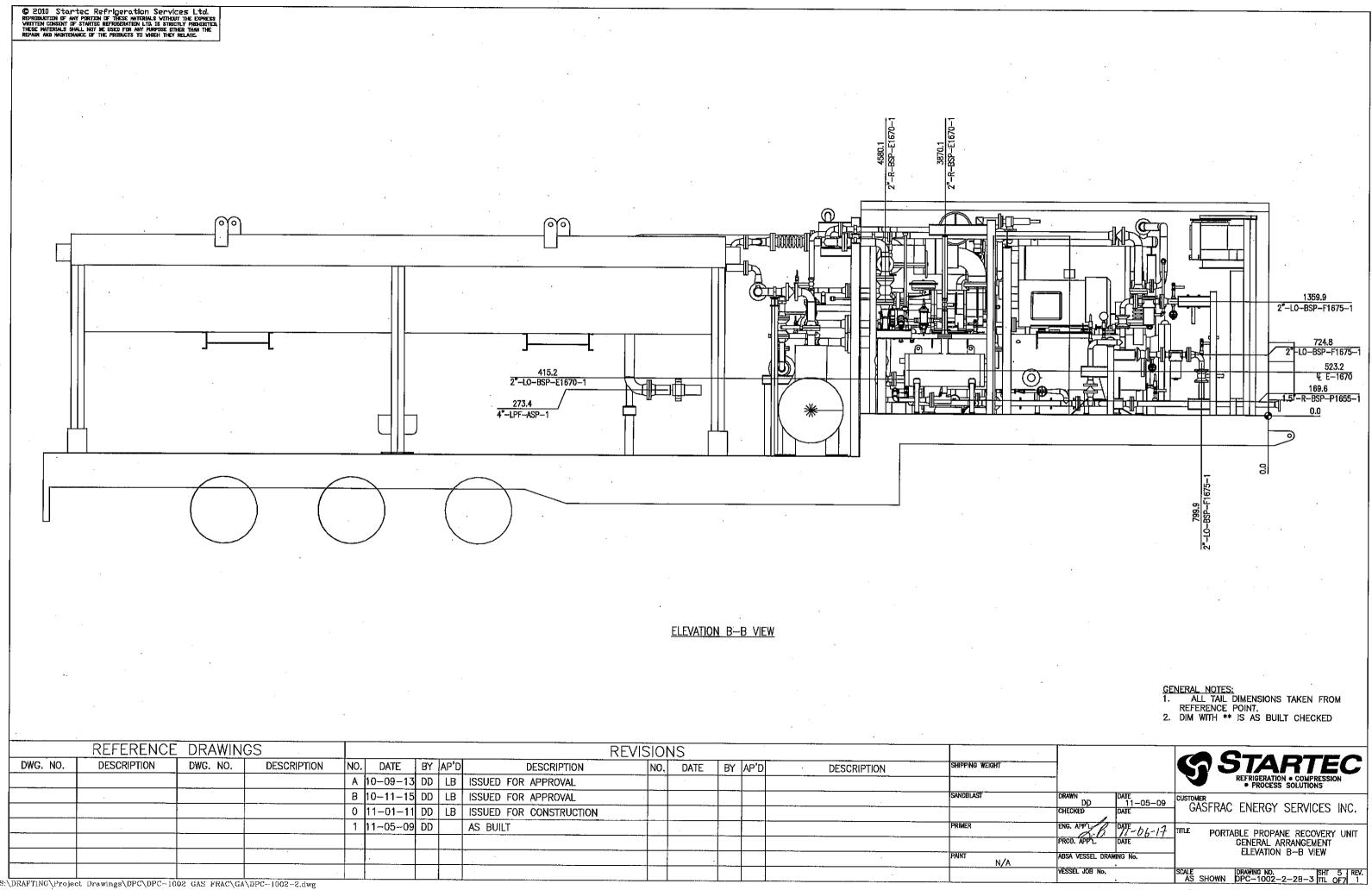
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- REFERENCE POINT.
- 2. FOR VIEW DIRECTIONS SEE SHT
- DPC-1002-2-2A-1
- 3. DIM WITH ** MEANS AS BUILT CHECKED

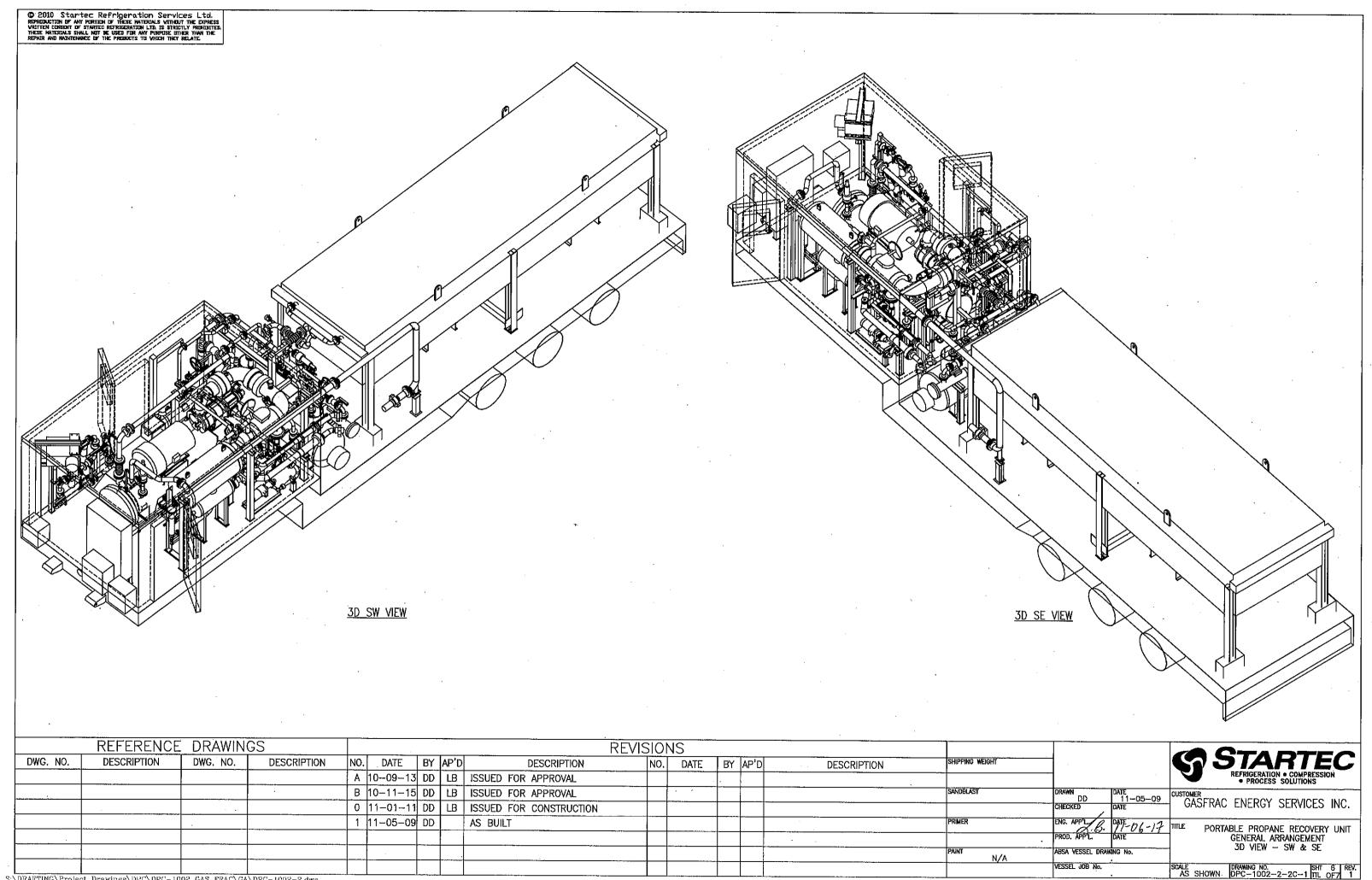
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DWG. NO.	DESCRIPTION	DWG, NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	SHIPPING WEIGHT
				A	10-09-13	5 DD	LB	ISSUED FOR APPROVAL					, and a second	
				В	10-11-15	5 DD	LB	ISSUED FOR APPROVAL			- · ·			SANDBLAST
				0	11-01-11	I DD	LB	ISSUED FOR CONSTRUCTION				1.		
				1	11-06-16	S DD		AS BUILT			-			PRIMER
														PAINT



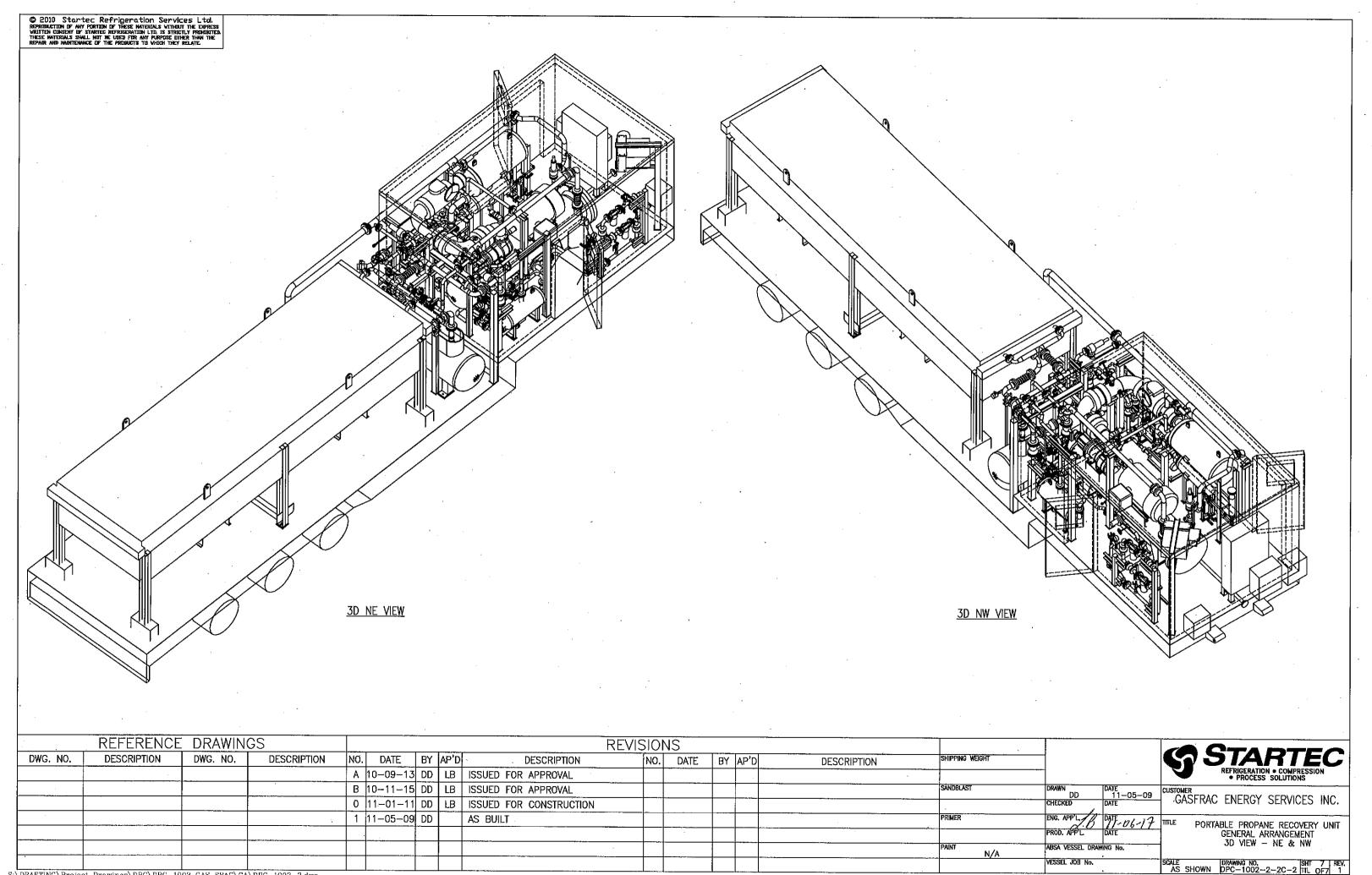


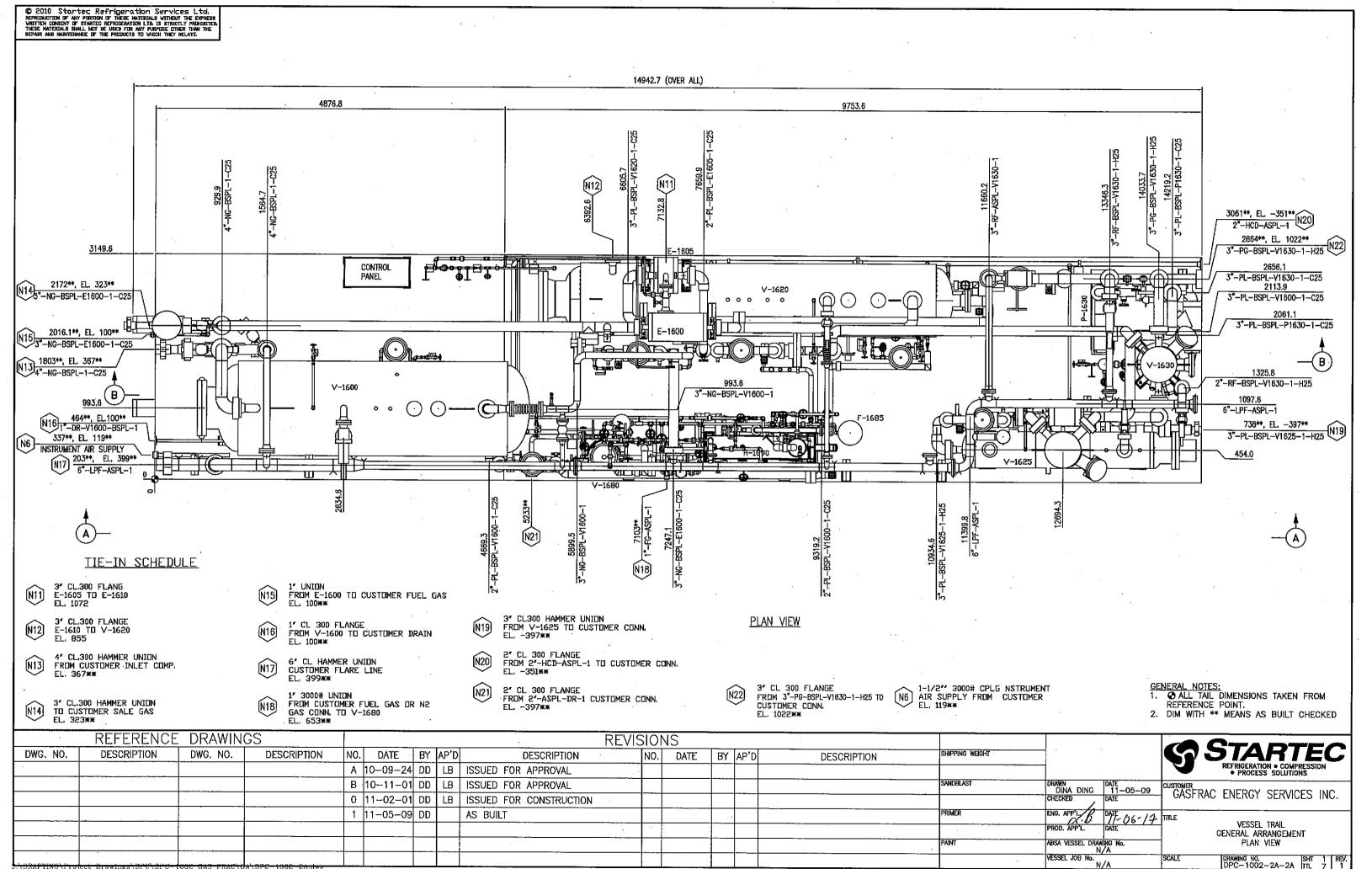


		DRAWIN	GS					RE	/ISION	٧S				
DWG, NO.	DESCRIPTION	DWG. NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	Shipping Weight
				A	10-09-13	DD	LB	ISSUED FOR APPROVAL						
				В	10-11-15	DD	LB	ISSUED FOR APPROVAL					······································	SANDBLAST
				0	11–0 1–1 1	DD	LB	ISSUED FOR CONSTRUCTION						
				1	11-05-09	DD		AS BUILT			1			PRIMER
														· · · ·
								· · · · · · · · · · · · · · · · · · ·						PAINT N/A
													-	

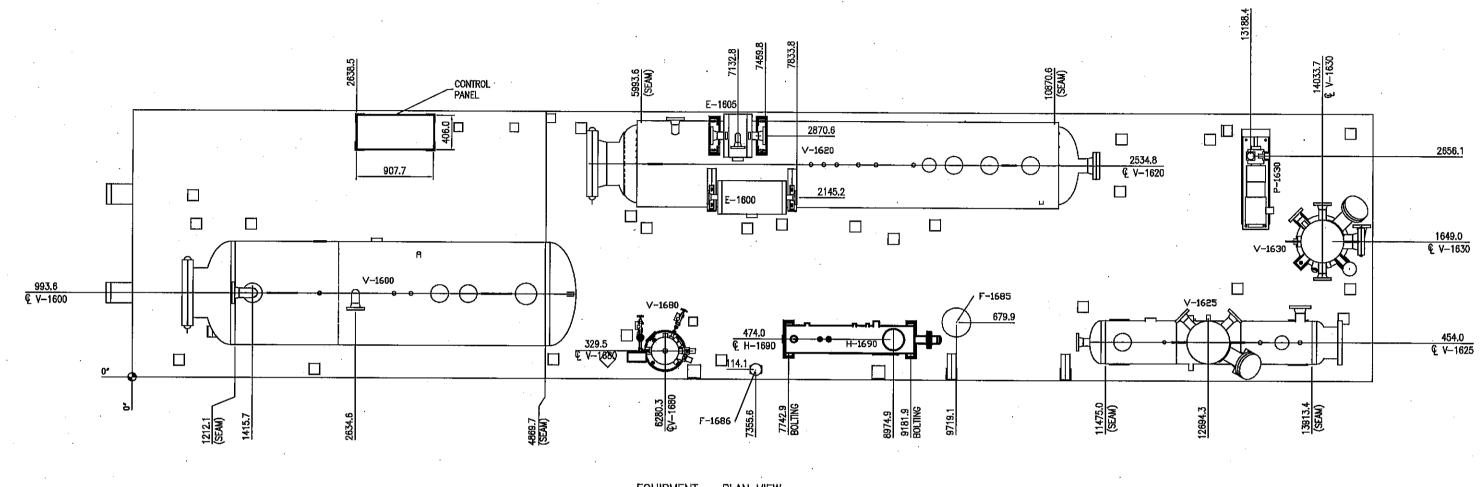


	REFERENC	<u>E</u> DRAWIN	GS			-		RE	VISIO	1S			and the second	
DWG, NO.	DESCRIPTION	DWG, NO.	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	NO.	DATE	BY	AP'D	DESCRIPTION	Shipping weigh
				A	1009-1	3 DD	LB	ISSUED FOR APPROVAL						
<u></u>				В	10-11-1	5 DD	LB	ISSUED FOR APPROVAL		• •				SANDBLAST
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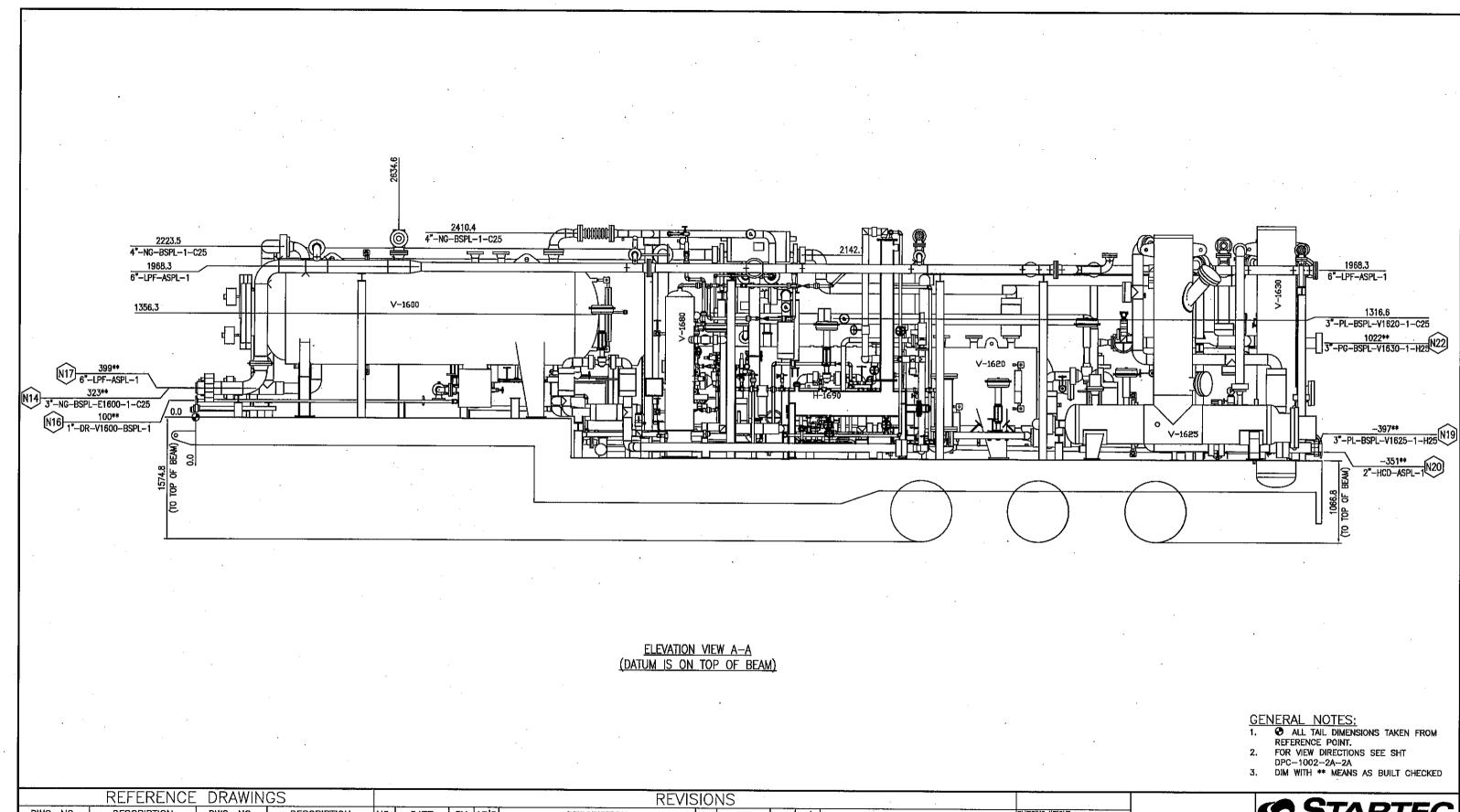
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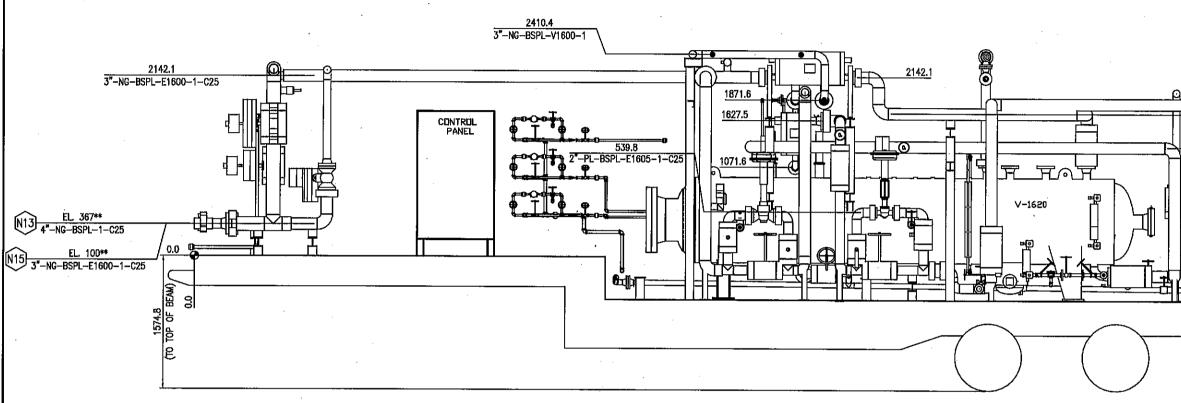
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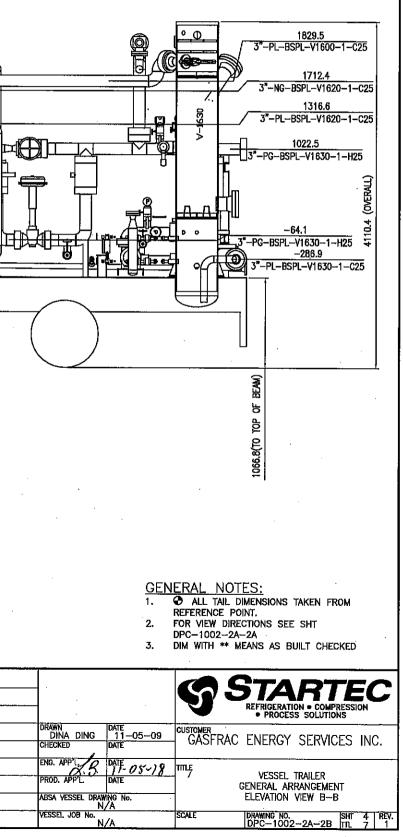
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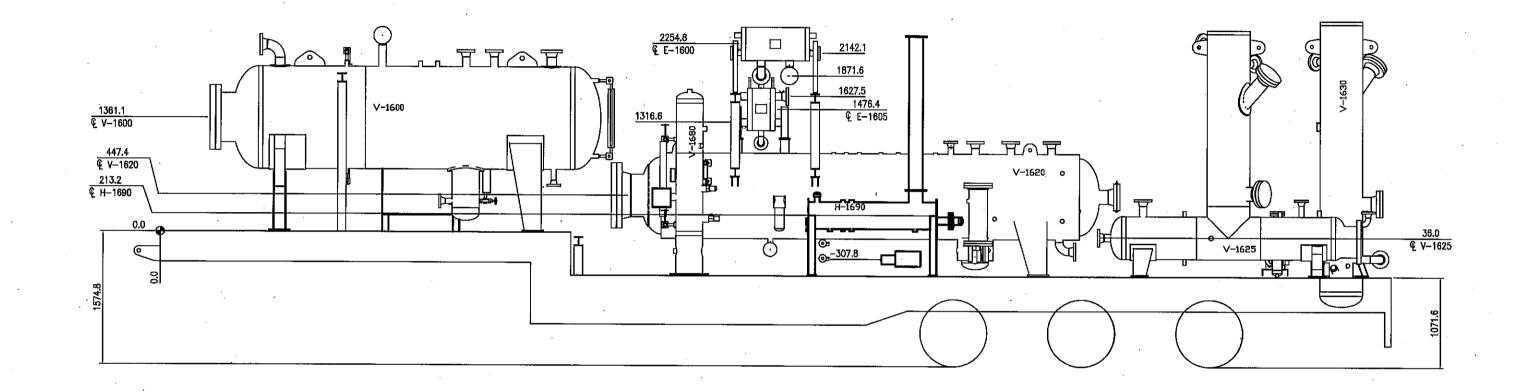
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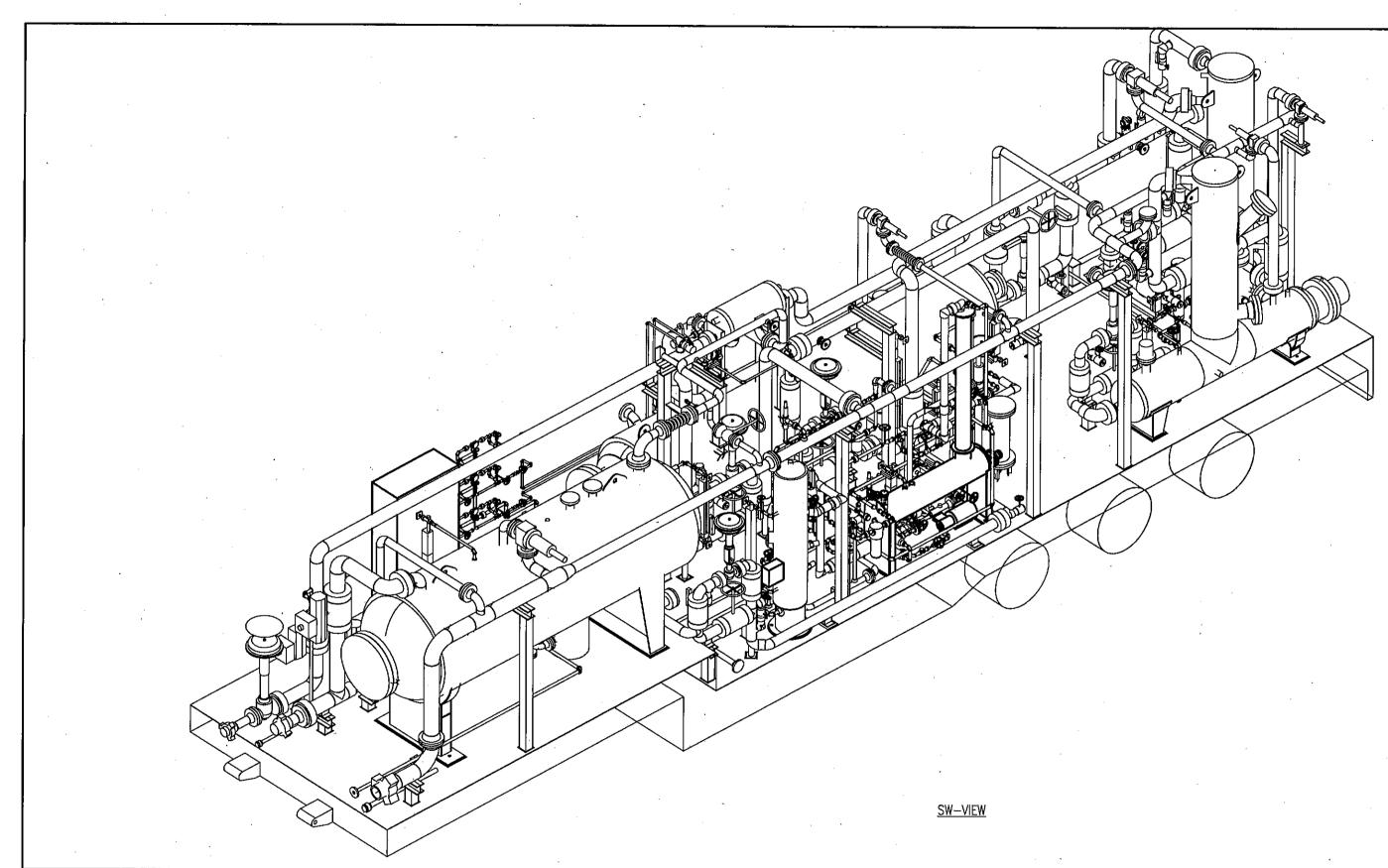




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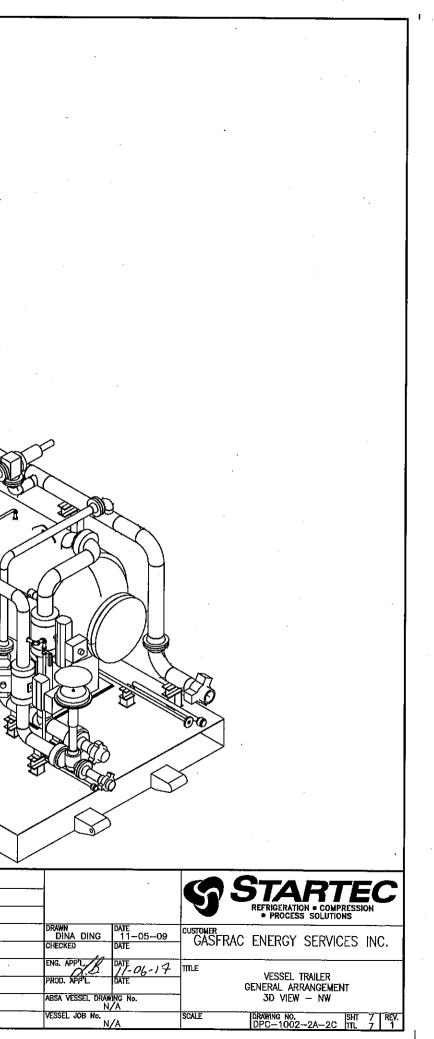


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STARTEC COMPRESSION & PROCESS SOLUTIONS for GASFRAC ENERGY SERVICES Inc.

4.0 mmscfd Propane Recovery Plant

(Startec job DPC-1002)

Process, Operation, and Control Description

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1. INTRODUCTION

This Manual provides a description of the equipment and its operation and control. The process is described together with the suggested start and stop sequences. The individual control loops are also described. Lists of alarms, trips and PSVs are provided as Appendices.

This propane recovery plant is designed and built by Startec Compression & Process Solutions, Calgary, Canada, for GASFRAC Energy Services Inc. (Calgary). They are also the end user and will use the plant throughout the western provinces of Canada and in the United States in their well stimulation business.

The propane recovery plant is designed to treat up to 4.0 mmscfd of Flow Back well stimulation fluid, producing dry gas and the recovered propane liquid as products.

The package consists of two trailered units being a propane refrigeration plant and a gas process unit with interconnecting hose and facilities for quick connection of the required utilities.

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2. PROCESS OVERVIEW

2.1 DESIGN CASES, FEEDS AND PRODUCTS

The gas and liquid feed stream for the propane recovery plant are fracture fluids that are flowed back from a fractured well to complete the well fracturing process.

The flow back process flow composition is not constant. Higher proportions of the propane fracturing fluid are seen at the start of the flow back and the proportion of the propane fracturing fluid declines as the well flow gradually lifts out the fracturing fluid from the well. The process simulation for the recovery process covered a range of propane compositions from 90% down to 10% and the equipment has been provided to meet the worst case sizing requirement for the 4.0 mmscfd design flow.

The gas feed enters the plant at the inlet separator V-1600 and the propane rich off gas goes on to a typical Dew Point control system of heat exchangers and a propane refrigerate chiller to remove additional LPG liquids from the gas stream. These liquids are then combined with the free hydrocarbon liquid separated initially in the inlet separator and this hydrocarbon liquid feed goes to the deethanizer unit V-1625 / V-1630 to fractionate to meet the required HD5 propane specification of the bottoms product.

Note: throughout this Manual the design controller setpoints, design alarm and trip setpoints, design pressures, temperatures and flows are used. These will vary during commissioning and operation and should be used as an initial set of values for starting the plant. The final operating values for alarms, trips and controller setpoints will be determined during commissioning and the first few months of operation. Some setpoints related to the compressor lube oil system are manufacturer specified and should not be changed without approval of Startec.

The feed and product conditions are noted in the following tables:

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2.2 SIMPLIFIED PROCESS DESCRIPTION

2.2.1 Normal Case

Fracturing Fluids and well effluent from the client's targeted wellbore are first filtered of any suspended frac sand or propant prior to a choked well flow control manifold. This flow is vaporized using an indirect fired line heater. The proprietary chemicals used to gel the propane are removed and the vapour stream is sent to the propane recovery plant. This fluid stream enters the inlet separator where any free liquids are retained and separation of any hydrocarbon liquids from formation water can take place in this 3 phase separator. The gas stream off the top of the inlet separator then goes to the dew-point control equipment. The gas stream is then cooled by passing through the shell side of the gas-to-gas exchanger E-1600, further cooled passing through the shell side of gas-to-liquids exchanger E-1605 and is then chilled in Gas Chiller E-1610. A propane (R290) refrigeration system provides cooling for the gas chiller E-1610.

A glycol / water mix is injected at each shell side exchanger inlet mentioned above to prevent hydrate formation. The three-phase flow from E-1610 is separated in a 3-phase low temperature separator (LTS) V-1620. The cold vapour from V-1620 passes to the plate side of the gas-to-gas exchanger E-1600 and is warmed by the incoming gas stream and leaves the dew-point plant as product gas for sale or disposal.

The cold hydrocarbon liquids from the LTS pass to the plate side of the gas-liquids exchanger E-1605 and is warmed by the incoming gas stream and flows through LV-1620. This hydrocarbon liquid stream combines with the hydrocarbon liquid stream accumulated in the inlet separator V-1600 and flows through LV-1600 to the inlet of deethanizer tops tower V-1625. Because of transport height limitations the deethaizer tower has been split into two shorter towers. The tops tower previously mentioned V-1625 and the bottoms tower V-1630 that has the reboiler heating element HTR-1630 that provides the heat to drive off the light ends in the liquid feed stream.

V-1625 is a non-refluxed distillation column designed to remove most of the ethane from the bottoms product. The ethane-rich deethanizer overheads are recycled (compressed) to the plant inlet, sold or disposed of at the flare-stack. The deethaniser bottoms flows to the propane product storage tank ????? to be located elsewhere on the wellsite.

The rich glycol from LTS V-1620 boot flows to a regenerator package H-1690. A 12 KW electric heated reboiler / still unit provide lean glycol for injection. A flash tank, glycol filter, carbon filter and injection pump are also provided.

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3. EQUIPMENT LIST AND PLANT ARRANGEMENT

3.1 MAJOR EQUIPMENT LISTING

Please refer to general arrangement drawings DPC-1002-2 (Compressor Trailer) and DPC-1002-2A (Vessel Trailer).

The propane recovery plant is supplied on two 10' 4" wide x 48 ft long trailers as follows:

3.1.1 Compressor Trailer

Please refer to P&ID drawing DPC-1002-01 sheets 1A-1D & 1G-1L.

Compressor Trailer (Trailer #1)					
Description: Propane (R290) Refrigerant System, Process Chiller Purpose: Provide refrigerant to chill feed gas					
Tag #	Description	Purpose			
K-1660	R290 compressor Howden XRV-	Compress R290 vapour			
	204-193-50 oil flooded screw				
	compressor				
KM-1660	R290 Compressor Driver 250hp,	Drive R290 Compressor			
	3/60/230/460VAC				
V-1670	R290 Compressor Oil Separator 24"	Separate R290 and compressor oil			
	OD x 120" s/s				
HTR-1670/1671	2 kW immersion heater (each)	Maintain oil temperature when the compressor			
		is not running			
AC-1655	R290 Condenser, 1222 kW, fin-fan,	Condense compressed R290 vapour			
	12 x 3.7 kW 3/60/460VAC fan				
	motors				

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Compressor Trailer	r (Trailer #1)				
Description: Propane (R290) Refrigerant System, Process Chiller					
Purpose: Provide r	efrigerant to chill feed gas				
Tag #	Description	Purpose			
K-1660	R290 compressor Howden XRV-	Compress R290 vapour			
	204-193-50 oil flooded screw				
	compressor				
ACM-1655 A to F	Condenser Fan Driver 3.7 kW,1200	Provide airflow for aerial condenser			
	rpm, CL 1 Div 2				
ACM-1656 A to F	Condenser Fan Driver 3.7 kW,1200	Provide airflow for aerial condenser			
	rpm, CL 1 Div 2				
PCV-1650	Hot gas bypass valve for receiver V-	Maintain pressure in receiver during low			
	1650	ambient conditions			
V-1650	R290 Receiver 30" ID x 96" s/s	Storage / buffer volume for liquid R290			
F-1646	R290 filter-drier	Remove free water from refrigerant			
P-1655	Propane Coolant Pump	Circulate liquid propane to E-1670 oil cooler			
PM-1655	Propane Coolant Pump Driver 1.5	Drive Propane Coolant pump			
	hp, 3/60/230/460VAC				
E-1670	R290 Compressor Oil Cooler	Cool compressor oil			
F-1675A/B	R290 Compressor Oil Filter	Filter compressor oil			
DPCV-1670	Compressor Discharge differential	Maintain pressure in oil separator V-1670			
	pressure control valve	during low ambient temperatures			
TCV-1668	Temperature control valve for	Bypass oil to oil cooler			
	compressor oil				
PCV-1610	Propane Hot gas bypass valve	Provide hot R290 to chiller (false load)			
E-1610	Gas chiller, Plate & Shell with surge,	Chill and partially condense cooled feed gas			
	Duty 169 kW				
E-1615	Gas chiller surge drum, 670mm OD	Separate liquid from refrigerant vapour,			
	x 1200mm s/s	provide surge volume for startup and upsets			

Septimus 40 mmscfd Dewpoint Control Plant - Process, Control and Operations Description

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Compressor Traile	r (Trailer #1)			
Description: Propane (R290) Refrigerant System, Process Chiller Purpose: Provide refrigerant to chill feed gas				
				Tag # Description Purpose
K-1660	R290 compressor Howden XRV- 204-193-50 oil flooded screw compressor	Compress R290 vapour		
LV-1610	Level control valve for Propane R290 Chiller E-1610	Control refrigerant level in chiller		
Glycol Metering FI-1615	Glycol injection for hydrate control (manual)	Meter and inject EG/water into exchanger inlets for hydrate control		
RIO #1	Remote IO Junction Box, Class 1 Div 2 Terminal Box	Control and monitor propane refrigeration plant		
UH-100	Building Heater, 10 kW, 460/3/60	Electric heater for compressor room		

3.1.2 Vessel Trailer

Please refer to P&ID drawing DPC-1002-01 sheets 1A-1D & 1G-1L.

Vessel Trailer (Trailer #2)
Description: Gas Cooling, Gas-Liquids Separation, EG Regeneration, RIO
Purpose: Produce and separate NGL from feed gas, Produce HD5 spec Deethanizer bottoms product

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Tag #	Description	Purpose	
V-1600	Inlet Separator,48" OD x 144" S/S	3 phase separation of liquids from the inlet gas	
	w/ 12.75" OD Boot x 18" LG	stream	
E-1600	Gas-to-gas exchanger, Plate &	Cool feed gas, warm sales gas	
	Shell, 26" Duty 97 kW		
E-1605	Gas-to-liquids exchanger, Plate &	Cool feed gas, warm NGL	
	Shell, Duty 70 kW		
LV-1600	Level control valve for inlet	Control level of hydrocarbon level in the inlet	
	separator HC phase	separator	
LV-1601	Level control valve for inlet	Control level of produced water in the inlet	
	separator H2O phase	separator	
V-1620	Low temperature separator, 36" ID	Separate natural gas, NGL and rich glycol	
	x 192" s/s, 12" OD x 10" glycol boot		
LV-1620	Level control valve for LTS NGL	Control level of hydrocarbon liquids in LTS	
	phase		
LV-1624	Level control valve for LTS rich	Control level of rich glycol in LTS	
	glycol phase		
HTR-1620	LTS Boot heater, 1.0 kW, 460/3/60	LTS boot heater to aid in the glycol separation	
USD-1600	Pneumatically Actuated Ball valve	Closes the inlet flow to the unit on ESD	
USD-1601	Pneumatically Actuated Ball valve	Closes the outlet flow from the unit on ESD	
FLR-1603	Pneumatically Actuated Ball valve	Opens a path to Flare bypassing the recovery	
		plant	
Glycol Metering	Glycol injection for hydrate control	Meter and inject EG/water into exchanger	
FI-1600, FI-1605	(manual)	inlets for hydrate control	
H-1690	Glycol regeneration package	Regenerate rich glycol from LTS V-1620	
	(reboiler, surge, packed still), 12"		
	OD x 60" s/f		
HTR-1691	12 kW electric heater for glycol	Heat rich glycol in reboiler	
	reboiler		
P-1695	Glycol injection Pump, 2.0 usgpm,	Pump lean glycol into high pressure gas	

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Vessel Trailer (Tr	railer #2)		
	Cooling, Gas-Liquids Separation, EG Reg		
Purpose: Produce and separate NGL from feed gas, Produce HD5 spec Deethanizer bottoms product			
Tag #	Description	Purpose	
V-1600	Inlet Separator,48" OD x 144" S/S w/ 12.75" OD Boot x 18" LG	3 phase separation of liquids from the inlet gas stream	
	triplex piston type	exchangers	
PM-1695	Driver for glycol pump, 1.0 hp, 3/60/460VAC	Drive glycol pump	
E-1690 A/B	Lean/Rich Glycol Exchanger	Cools the Lean Glycol for pumping	
F-1686	Glycol bag filter	Filter larger particulates	
F-1685	Glycol carbon filter	Polishing filter – removes hydrocarbons	
LV-1680	Level control value for glycol flashControl EG level in flash tanktank V-1680		
V-1680	Glycol flash tank, 12" OD x 60" s/s	Separate hydrocarbons from rich glycol stream	
LV-1680	Level control valve for glycol flash tank V-1680	Control EG level in flash tank	
BPCV-1681	Backpressure control valve for glycol flash tank V-1680	Maintain pressure in flash tank	
V-1625	Deethanizer Bottoms, packed, 20" OD x 80" vertical c/w reboiler section	Add heat to concentrate ethane in overheads and produce spec liquid product	
HTR-1630	Deethanizer Reboiler heater, 173 kW, 5 stage, 480/3/60	Provides heat to boil off the ethane and lighter vapours	
LV-1625	Level control valve for deethanizer V-1625 bottoms	Control level of NGL in deethanizer bottoms and deliver propane product	
V-1630	Deethanizer Top, packed, 20" OD x 120" S/S	Concentrate ethane in overheads	
P-1630	Propane Transfer Pump, 80.0	Pumps liquids from the bottom V-1630 to the	

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Vessel Trailer (T	railer #2)				
Description: Gas Cooling, Gas-Liquids Separation, EG Regeneration, RIO					
Purpose: Produc	Purpose: Produce and separate NGL from feed gas, Produce HD5 spec Deethanizer bottoms product				
Tag #	Tag # Description Purpose				
V-1600	Inlet Separator,48" OD x 144" S/S w/ 12.75" OD Boot x 18" LG	3 phase separation of liquids from the inlet gas stream			
	usgpm, Blackmer LGLD2E	top of V-1625			
PM-1630	Driver for propane transfer pump, 5.0 hp, 3/60/460VAC	Drive propane transfer pump			
PV-1638	Deethanizer pressure control valve (future)	Maintain pressure in deethanizer V-1630			
PV-1639	Deethanizer to Flare control valve	Maintain pressure in deethanizer V-1630 by venting overheads to flare			
RIO #2	Remote IO Junction Box, Class 1 Div 2 Terminal Box	Control and monitor gas process plant			

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3.2 EQUIPMENT ARRANGEMENT

The equipment in Startec's scope of work is mounted on two mobile trailer (TARE 80,000 lbs each) units that are moved from location to location as required by GASFRAC and their clients.

The trailers are designed to be situated on the lease in a side-by-side configuration so as to facilitate the connection of the interconnecting low temperature pressure hoses as required by the process.

All interconnecting hose between the two trailers is provided by Startec. Piping from the trailer units to other site equipment is provided by others.

All control system cabling on the two trailers is provided by Startec and are wired back to the RIO panel boxes located at the front end of both trailers.

All control system cabling from the skids to the plant PLC located in the utility trailer is provided by others.

Power cabling is by others.

The propane recovery plant is tied into the wellsite fracturing equipment via the high pressure hoses at the appropriate customer connections as defined in the P&ID. On site hook-up of the propane recovery plant and final site installation configuration is the responsibility of others.

The compressor building is provided by Startec. The compressor building electrical (ie. Lighting and power outlets etc.) is provided and installed by others.

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4. CONTROL AND ELECTRICAL OVERVIEW

4.1 GENERAL

The propane recovery plant is designed for a Class 1 Division 2 hazardous area. All electrical equipment is CSA approved for Class 1 Division 2; all wiring is CSA cable and conduit for Class 1 Div 2. The RIO skid edge terminal boxes are NEMA 4.

The plant requires power to be supplied at 3/60/460 VAC for motors, heaters etc.. The control system requires a 24 VDC supply with the end devices (supplied by Startec) operating on 24 VDC. The control system is provided by Kilowatts as part of the Utility and power generation and distribution requirement contracted to them.

4.2 CONTROL SYSTEM

The control system will be based on a control philosophy and shutdown key provided by Startec.

The PLC (by Kilowatts) provides control logic for the various PID loops in the propane recovery plant and also provides machinery and plant protection. Transmitters and switches are provided for level, pressure, temperature etc. and used by the PLC to provide control, alarms and shutdowns. All setpoints are operator-configurable from the HMI.

There are skid-edge terminal boxes on each trailer to allow connection of the devices on the trailers to the PLC. The cabling (multi-core flex for CSA Class 1 Division 2) is run from the terminal boxes across the lease to the PLC on the utility trailer.

Note that motor control is directed and executed by Kilowatt's PLC – please see the P&IDs for the signal flow.

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5. DETAILED PROCESS AND EQUIPMENT DESCRIPTION

5.1 INLET SEPARATION

In the following sections, values are provided for process variables and setpoints. The values given are the design values. These values will change or need to be adjusted during commissioning and as the feed conditions or composition change.

On completion of the well fracturing process the well is but on flow back. This begins the propane recovery process and cleans the well in preparation for production. The fluid from the wellbore are heated and its pressure is controlled and directed to the Propane Recovery Plant.

The Propane recovery Plant can be isolated from the upstream facilities in the event of an ESD event. The plant is equipped with solenoid actuated inlet (USD-1600) ball valve and outlet (USD-1601) ball valve to isolate and an on unit ball valve to flare (FLR-1603).

The hydrocarbon feed is a water-saturated mixture of hydrocarbons, containing a range of hydrocarbons from methane & Ethane, to propane and small amounts of heavier hydrocarbons. The feed is predominantly propane (90%) as the flow back starts and will gradually reduce to 10 -20% propane and a point where the flow back is deemed complete. The recovery of the propane reduces significantly the recurring expense of replenishing the propane requirement for each fracturing operation.

The propane recovery process plant provides the required liquid separation and subsequent dewpoint control of the gas by cooling the feed gas stream, condensing the heavier hydrocarbons (predominantly propane) and physically separating them in a fractionating tower.

The inlet separator is a 48" OD x 144" S/S 3 phase horizontal separator that is equipped with a boot to collect the separated heaviest component in the inlet stream, usually produced water. The vessel is also equipped with an additional liquid / liquid coalescing element to enhance the separation of the water and hydrocarbon in the separator. The gas stream has a second separation enhancement at the outlet of the separator with the addition of a vane pack and mesh pad.

The hydrocarbon being lighter than the water phase collects on top of the water and spills over an internal weir plate into the hydrocarbon collection compartment of the separator. The level of the hydrocarbon in the compartment is monitored by LIT-1600 (guided wave radar level transmitter) and the level is controlled through LV-1600 by LIC-1600. This hydrocarbon goes to the deethanizer top tower V-1630 for further processing.

The produced water level that is collected in the boot of the separator has the interface level of the water in the boot monitored by LIT-1601 (guided wave radar level

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transmitter) and the level is controlled through LV-1601 by LIC-1601. The produced water is taken from the propane recovery plant and collected in a storage tank elsewhere on the lease for intermittent disposal as required.

The inlet separator has been provided with MeOH connection points as a means of hydrate control in the separator in the event of its occurrence.

The gas stream from the inlet separator now goes on for further gas conditioning and additional liquid separation in the LTS (V-1620).

V-1600 Inlet Separator - Instruments			
Instrument	Tag	Location	
Pressure Gauge	PI-1600	Separator shell	
Control Valves	LV-1600	Hydrocarbon out	
	LV-1601	Water Boot out	
Thermocouple	TE-1600	Separator shell	
Temperature Gauge	TI-1600	Separator shell	
Inlet Shut-off	USD-1600	Separator Inlet line	
Level Gauge	LG-1600	Separator shell (Hydrocarbon level)	
Level Gauge	LG-1601	Separator shell (Vessel level)	
Level Gauge	LG-1602	Separator shell (Boot level	
Level Transmitter	LIT-1600	Separator shell (HC level)	
Level Transmitter	LIT-1601	Separator shell (Boot level)	

5.2 GAS CONDITIONING PORTION OF THE DEWPOINT PLANT

The following detailed description of the gas conditioning portion (HP side) of the dewpoint plant process should be read in conjunction with the Process and Instrumentation Drawings (P&ID) DPC-1001-A,B, G, H-K.

High pressure gas from the customer's inlet separator and recycle gas from the customer's deethaniser overheads recycle compressor are combined to form the feedstream to the Dewpoint Control Plant.

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5.2.1 Gas-Gas Exchanger E-1600A/B and Gas-Liquids Exchanger E-1605

The high pressure gas feedstream at 4930 kPag and 45 °C enters the tubesides of heat exchangers E-1600A and E-1600B. Cold gas at -24 °C from Low Temperature Separator (LTS) V-1620 on the shell sides of E-1600A/B cools the rich inlet gas. The tube side gas exits E-1600A/B at 4895 kPag and -5 °C and enters the tubeside of gas-liquids exchanger E-1605 where it is cooled further by heat exchange with the LTS liquids at -24 °C on the shellside. E-1600A/B and E-1605 are provided with spray nozzles in the tube side bonnets to facilitate the continuous injection of lean glycol to prevent the formation of hydrates.

These exchangers are TEMA type NEN with fixed tubesheets. The following instrumentation is provided:

E-1600A/B Gas-Gas Exchanger - Instruments			
Instrument	Тад	Location	
Pressure Gauge	PI-1600	Tubeside inlet (Feed)	
	PI-1601	Shellside outlet (Sales Gas)	
	PI-1603	Tubeside outlet (to G-L)	
Pressure Transmitter	PT-1600	Tubeside inlet (Feed)	
	PT-1602	Shellside outlet (Sales Gas)	
Temperature Gauge	TI-1600	Tubeside inlet	
	TI-1602	Tubeside outlet	
	TI-1601	Shellside outlet (Sales Gas)	
Glycol Flowmeter	FI-1600A	Tubeside of shell A	
	FI-1600B	Tubeside of shell B	

E-1605 Gas-Liquids Exchanger - Instruments			
Instrument	Тад	Location	
Temperature Gauge	TI-1611	Tubeside outlet	
	TI-1606	Shellside outlet	
	TI-1605	Shellside inlet	
Pressure Gauge	PI-1613	Tubeside outlet	
	PI-1605	Shellside outlet	

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E-1605 Gas-Liquids Exchanger - Instruments			
Instrument Tag Location			
Glycol Flowmeter	FI-1605	Tubeside	

5.2.2 Gas Chiller E-1610

Gas from the tube side of E-1605 leaves at 4861 kPag and -7 °C. To provide suitable LPG products from the fractionation plant and meet sales gas HC dewpoint, the feed gas must be finally cooled to -24 °C in chiller E-1610. Liquid propane refrigerant (R290) at -29 °C is evaporated to provide the chilling duty. This exchanger is TEMA BEU type with removable tube bundle with a surge vessel. A separate manually-drained oil collection pot is provided. Hot gas from the discharge of the refrigeration compressor can be injected into the chiller via valve PV-1610 to maintain operation at low process duty.

The liquid refrigerant level is maintained close to or just over the top of the tube bundle by guided wave level transmitter LT-1611 and level controller LIC-1611 and level control valve LV-1611. The top row of tubes may be exposed if superheat is required for the vapour. The BEU shell is not designed for any vapour / liquid separation, which is achieved in the surge drum.

Note: the oil-flooded screw compressors used in the refrigeration plant allow oil to pass into the refrigerant stream. This oil will collect in the colder parts of the system, usually the chiller. At this point, the oil is denser than the propane refrigerant and will, over time, collect in the chiller shell. The lower portion of the oil pot shell is uninsulated – if no oil is present this portion will be covered in ice; if oil is present the portion of the boot below the oil-propane interface will be free of ice. When sufficient oil is present the oil pot may be manually drained (note that R290 vapour will flash off the oil).

To prevent the formation of hydrates lean glycol is continuously injected into the tube side bonnet of E-1610.

The following instrumentation is provided on the gas chiller:

E-1610 / E-1615 Gas Chiller / Surge Vessel - Instruments			
Instrument	Tag	Location	
Pressure Gauge	PI-1611	Shellside outlet (propane)	
Pressure Transmitter	PT-1601	Shellside outlet (propane)	
Temperature Gauge	TI-1612	Tubeside outlet (gas)	
	TI-1610	Shellside outlet (propane)	
PSV	PSV-1612	Shellside (tube rupture)	

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E-1610 / E-1615 Gas Chiller / Surge Vessel - Instruments			
Instrument	Тад	Location	
Glycol Flowmeter	FI-1610	Tubeside	
Level Gauge	LG-1611	Shellside (propane)	
Level Transmitter	LT-1611	Shellside	
Level Switch	LSHH-1610	Shellside	

5.2.3 Low Temperature Separator V-1620 (LTS)

The process side discharge from E-1610, which comprises three phases (hydrocarbon vapour, condensed hydrocarbon liquid and rich glycol), is then directed to the Low Temperature Separator V-1620 which under normal operating conditions operates at -27.4 °C.

The fluid enters the Low Temperature Separator and is separated into the three phases by gravity over time; both the hydrocarbon liquids and glycol phases have a design retention time of 30 minutes. An inlet diverter and two full diameter premium coalescing elements aid initial separation of vapour and liquids and mist in the separated vapour stream is removed by a meshpad in the LTS vapour outlet. A weir separates the liquid-liquid separation section and boot from the LTS HC Liquid section – the product overflows the weir into the product section where it leaves the LTS. A vortex breaker is provided for the hydrocarbon liquid outlet and an internal siphon for the rich glycol.

The hydrocarbon liquid level in the LTS is measured by guided wave level transmitter LT-1620 on the product section, which is used by LIC-1620 to control level control valve LV-1620. Note that there is a significant pressure drop across this valve: upstream is LTS pressure of 2100 kPag, downstream is deethanizer pressure of 1100 kPag. The fluid is liquid upstream of LV-1620, two-phase downstream.

The rich glycol collects in the boot section of the LTS; the interface level in the boot is measured by guided wave radar level transmitter LT-1624 and is controlled by LIC-1624 acting on level control valve LV-1624. Note that the rich glycol level is set high in the boot compartment.

Rich glycol passes through LV-1624 to the glycol regeneration skid H-1690 where the absorbed water is removed and the glycol is regenerated to a 85 wt% EG/15 wt% water mixture. The glycol boot contains an electric heater to aid in the glycol separation. Note that there is a significant pressure drop across valve LV-1620: upstream is LTS pressure of 2100 kPag, downstream is glycol flash tank V-1680 pressure of 345 kPag. The fluid is liquid upstream of LV-1624, two-phase downstream.

The following instrumentation is provided on the LTS:

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V-1620 LTS - Instruments			
Instrument	Tag	Location	
Pressure Gauge	PI-1621	LTS shell	
Pressure Transmitter	PT-1622	LTS shell	
Temperature Gauge	TI-1621	LTS shell	
Thermocouple	TE-1620	LTS shell	
PSV	PSV-1620	LTS shell (fire)	
Level Gauge	LG-1620	LTS HC liq compartment	
	LG-1621	LTS shell / Glycol boot	
	LG-1622	LTS shell	
Level Transmitter	LT-1620	LTS HC liq bridle	
	LT-1624	LTS shell / Glycol boot bridle	

5.2.4 Sales Gas from LTS to Skid Edge

The cold, dry vapour from LTS V-1620 is directed back to the plate side of gas-gas heat exchangers E-1600, where it cools the feed stream and is warmed prior to leaving the propane recovery plant for the customer's dispersal or disposal.

5.2.5 Hydrocarbon Liquids from LTS V-1620 to Gas/Liquids Exchanger E-1605

The condensed hydrocarbon liquid collects in the hydrocarbon liquid compartment of the LTS and flows out to the plate side of the gas-liquids heat exchanger E-1605 where it warmed against the gas feed. As it is possible to form hydrates at the inlet of the deethanizer. The liquid flow is controlled by control valve LV-1620. The liquid at -11 °C from the plate side of E-1605 flows to the V-1630 deethanizer top vessel. The LTS hydrocarbon liquid level control valve LV-1620 is installed downstream of the Gas/Liquids exchanger E-1605 to ensure that exchanger remains flooded.

5.2.6 High Pressure Side Blowdown

Blowdown valve BDV-1600 and orifice RO-1600 allow the high pressure gas / liquid portion of the dewpoint plant to be depressurised. This valve is controlled from the PLC and is operated via solenoid BYV-1600.

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Orifice plate RO-1600 is sized to blow down the LTS skid to 690 kPag within 15 minutes

Note: the dewpoint plant PLC does not control process isolation valves or ESD valves, which are all off-skid, provided by others. Start, Stop and Blowdown of the dewpoint plant is dependent upon cooperation between the customer's DCS and the dewpoint plant PLC.

During blowdown, the material stresses will be within allowable limits at the corresponding pressures and temperatures.

During re-start and re-pressurisation, the DCS should prevent pressure from rising until the LTS low temperature alarm (TAL-1620) has cleared. The MDMT of the LTS is -45 °C, and the Low temperature alarm is set at -40 °C.

5.3 FRACTIONATION PORTION OF THE PROPANE RECOVERY PLANT

The following detailed description of the fractionation portion (LP side) of the propane recovery plant process should be read in conjunction with the Process and Instrumentation Drawings (P&ID) DPC-1002-01 sheets C &D.

5.3.1 Deethanizer Top V-1630 & Deethanizer Bottom V-1625

Because of the mobility requirement for the Propane Recovery Plant the deethanizer needs to be split to provide the design requirement for a 11 foot long packed section to meet the bottoms product specification while the overall travelling height is below the 13.5' maximum.

The deethanizer is designed to split its feed stream into two product streams, one vapour and one liquid. The overhead vapour stream is relatively free of heavier components suitable for liquid products and the liquid stream contains only trace amounts of components too light for liquid product.

This deethanizer is designed to provide a bottoms product with an ethane to propane mole ratio of 0.15; this ensures the majority of the ethane in the feed streams is sent to the overheads.

The deethanizer top V-1630 is fed the combined stream of liquid hydrocarbon from the LTS (V-1620) and the Inlet Separator (V-1600). The liquid enters this vessel just below the meshpad near the top of the tower. This nozzle has an internal inlet distributer to distribute the flow across the diameter of the bed. The deethanizer top tower V-1630 contains a 5.5' section of random packing. The liquid trickles down through the tower packing and is cross flowing with the vapours from V-1625 that

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have entered the bottom of V-1630 and provides the heat required to strip the liquid stream of its light ends (methane & ethane). The accumulated liquid level at the bottom of the tower is monitored by LIT-1635 (Guided wave Level transmitter) and then pumped by the Liquid Transfer Pump P-1630 on a control signal from LIC-1635 to the top liquid connection on the V-1625 deethanizer bottom tower.

The deethanizer bottom V-1625 is a reboiled fractionating tower with a 5.5' packed bed and has a single liquid feed near the top of the column that receives the liquid collected in the bottom of the Tops tower V-1630. The liquid entering the tower is again distributed across the tower diameter. The column is 20" OD x 120". Both tower beds consist of 0.5 m³ of IMPT #25 carbon steel random packing.

The deethanizer is controlled by maintaining the overhead design pressure at 1100 kPag and the bottoms design temperature at 35 °C. The overheads pressure is measured by PT-1638 and used by PIC-1639 to control pressure control valve PV-1639. This valve controls the deethaizer pressure by controlling vapour produced and releasing it to the flare system. In the future if a market or requirement for this gas is determined an additional valve (PV-1638) can be installed to control the pressure and deliver the vapour to this use. The existing PT-1638 can be use to control both valves in the future.

The heat input for V-1625 is provided by a 5 stage electric immersion heater HTR-1630. Liquid from the tower section of V-1625 (the deethanizer bottom tower) drops by gravity and is gathered in the reboiler section of this vessel surrounding the immersionheater elements where it is heated. The vapour generated in the reboiler section flows up through the packing as stripping the liquid flow. The liquid in the reboiler section is the deethanized product. The liquid level in the reboiler section is maintained above the immersion heater element by a weir. The liquid product over flows the weir and is collected in the storage compartment at the end opposite the heater element. This level is monitored by guided wave radar level transmitter LT-1625 which is used by LIC-1625 to control level control valve LV-1625. The warm liquid at 35 °C and 1100 kPag flows through LV-1625 to be delivered off skid as the propane product.

Vent valve PV-1629 also allows the deethanizer and reboiler to be depressurised. In this case PV-1629 is operated via solenoid EYV-1629 and controlled by the plant DCS.

Blanket gas is provided from the plant fuel gas system to allow purging prior to maintenance and to maintain pressure as the deethanizer and its reboiler cool. The gas is provided by regulator PCV-1630 set at 345 kpag.

The following instrumentation is provided on the deethanizer bottom V-1625 and deethanizer top V-1630:

V-1625 Deethanizer Bottom - Instruments		
Instrument	Тад	Location

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V-1625 Deethanizer Bottom - Instruments			
Instrument	Tag	Location	
Pressure Gauge	PI-1627	Overheads line	
	PI-1630	Reboiler Bottom	
Pressure Transmitter	PT-1628	Overheads line	
Differential Pressure Transmitter	DPIT-1626	Overheads to Bottoms section	
Temperature Gauge	TI-162?	Bottom section	
	TI-1626	Overheads line	
Thermo couple	TE-1626	Bottom section	
	TE-1625	Overheads	
PSV	PSV-1624	Reboiler section (fire)	
Level Gauge	LG-1625	Bottoms section	
Level Valve	LV-1625	Liquid Outlet line	
Level Transmitter	LT-1625	Bottoms Storage compartment	
Level Switch	LSLL-1630	Reboiler section	

	V-1630 Deethanizer Top - Instruments			
Instrument	Тад	Location		
Pressure Gauge	PI-1637	Overheads		
	PI-1634	Tower Pressure		
	PI-1625	Transfer Pump Discharge		
	PI-1635	Liquid Feed line		
Temperature Gauge	TI-1625	Transfer Pump Discharge		
	TI-1635	Liquid Feed line		
	TI-1636	Overheads line		
Thermocouple	TE-1635	Hot oil supply line		
Pressure Transmitter	PT-1638	Overheads line		
PSV	PSV-1635	Overheads line (failure of LV-1620)		

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V-1630 Deethanizer Top - Instruments			
Instrument Tag Location			
	PSV-1634	Tower Bottom(fire)	
Pressure Valve	PV-1639	Overheads line	
Differential Pressure Transmitter	DPIT-1636	Overheads to Bottoms section	
Level Transmitter	LT-1635	Tower Bottoms (Bridle)	
Flow Transmitter	FT-1630 / FE-1630	Hot oil return line	

5.4 GLYCOL INJECTION AND REGENERATION SYSTEM

5.4.1 Glycol Regenerator H-1690, Flash Tank V-1680, Glycol Filters F-1685/1686

As the gas stream is cooled in the gas exchangers water is condensed from the gas. At the design pressures and temperatures it is possible to form hydrates in the exchanger tubes which will reduce or stop gas flow. To prevent hydrate formation ethylene glycol is used as a hydrate inhibitor in the plant. In the lean / regenerated form it exists as a mixture of 85% by weight ethylene glycol and 15% by weight water.

The lean glycol is injected into the gas stream at the gas-gas exchangers E-1600, gas-liquids exchanger E-1605 and gas chiller E-1610. As the injected lean glycol passes through the gas exchangers it is diluted by the condensed water down to a rich 80/20 mixture of glycol and water.

The rich glycol stream is recovered from the Dew Point Control Plant in the boot of the Low Temperature Separator V-1620. The boot is level controlled by LT-1624 and LIC-1624 acting on level control valve LV-1624. The LTS boot contains an electric coil and the rich glycol in the boot is warmed slightly. The warming aids the separation of glycol and hydrocarbons in the boot.

The rich glycol from the LTS boot via LV-1624 is returned to the glycol regeneration package H-1690 which consists of

- o a 12" OD x 60" regenerator H-1690 with an electric heater HTR-1691 and packed still section
- two small rich/lean heat exchangers in series to cool the glycol pump flow

Note there is a large pressure drop across LV-1624. This valve will need to be tuned along with LV-1680 to avoid LAHH in flash tank V-1680.

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The rich glycol passes through the still coil, condensing vapour in the still to minimise glycol vapour loss and being warmed in the process. From the still coil the warming rich glycol passes through the two lean/rich heat exchangerswhere it is warmed further. As mentioned this helps to cool lean glycol returning to the Dew Point Control Plant.

After the rich glycol is warmed, it enters the glycol flash tank V-1680 where gas and heavier hydrocarbons (absorbed at the high pressure and low temperature in the Dew Point Control Plant) are separated and removed from the system. The glycol flash tank is fitted with a manual hydrocarbon liquid skimmer to provide for the removal of any hydrocarbon liquid carried through from the Low Temperature Separator V-1620.

The glycol flash tank has a pneumatic level controller LC-1680 which acts on level control valve LV-1680 to maintain a constant level in V-1680. A blanket gas supply is provided via regulator PCV-1682 to maintain the flash tank pressure at 345 kPag and the flash tank also has an overheads pressure regulator BPCV-1681 set at 517 kPag. If the pressure generated by the separated vapour is greater than 517 kPag then BPCV-1681 will control the flash tank pressure. If the pressure cannot be maintained above 345 kPag then PV-1682 will open and allow blanket gas to maintain the vessel pressure and circulate glycol to the reboiler. The flash tank has a blowdown valve BDV-1680 and also a meshpad to remove any mist in the vapour.

From V-1680 the rich glycol is filtered to remove particulates in bag filter F-1686 and dissolved hydrocarbons in activated carbon filter F-1685 before it enters the packed section of the glycol still at the top, where it is counter current contacted with reboiler vapours to effectively strip the water from it. The glycol drains down through the glycol still ending up in the reboiler H-1690, which is on temperature control by TIC-1692 at 130 °C, to yield regenerated glycol. The reboiler overflows a weir to the surge compartment of the H-1695 regenerator vessel.

The atmospheric regenerator section is heated by a stab-in etectric immersion heater HTR-1691 capable of 12 kW of duty. The temperature in the regenerator is measured by TE-1692 and used by TIC-1692 to control HTR-1691. The glycol regenerator is maintained at 130 °C. The heater HTR-1691 has an internal thermocouple that monitors the heating element temperature and will shut down the heater if this temperature exceeds its design limit.

Water stripped from the glycol exits the still column at atmospheric pressure and is and is collected in a local container for intermittent disposal.

H-1690 Glycol Regenerator - Instruments			
Instrument Tag Location			
Temperature Gauge	TI-1692	Regenerator shell	
	TI-1695	Glycol Pump suction	
	TI-1694	E-1690A tubeside out to V-1680	

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H-1690 Glycol Regenerator - Instruments			
Instrument	Тад	Location	
Thermocouple	TE-1692	Regenerator shell	
Cone Relief Device	PRV	Regenerator shell (thermal)	
Level Gauge	LG-1690	Surge shell	
Level Switch	LSLL-1690	Regenerator reboiler shell	
	LSLL-1691	Surge shell	

V-1680 Glycol Flash Tank -Instruments			
Instrument	Тад	Location	
Pressure Gauge	PI-1681	Blanket gas inlet	
	PI-1680	Glycol outlet	
Temperature Gauge	TI-1680	Flash tank shell	
PSV	PSV-1683	Flash tank shell (fire)	
Level Gauge	LG-1682	Flash tank shell (hydrocarbons)	
	LG-1680	Flash tank shell (glycol)	
Level Controller (pneumatic)	LC-1680	Flash tank shell	
Level Switch	LSH1681	Flash tank shell	
	LSLL-1683	Flash tank shell	

F-1685 / 1686 Glycol Filter - Instruments			
Instrument Tag Location			
Differential Pressure Gauge	DPI-1686	F-1686	
	DPI-1685	F-1685	
PSV	PSV-1686	F-1686 (fire)	
	PSV-1685	F-1685 (fire)	

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5.4.2 Glycol Pump P-1695

Lean glycol from the shell side of the Lean/Rich glycol exhangers passes to the injection pump P-1695 where the pressure is raised for injection into the gas exchangers at around 2100 kPag. The pump is a triplex plunger pump with pulsation damper in the discharge line.

The maximum flow from the pump is 2 usgpm which provides significantly more than the theoretical quantity required for hydrate control. This allows for losses and for incomplete coverage by the spray nozzles in each exchanger.

Glycol from the surge compartment passes through a Y-strainer with 60 gauge mesh screen to the pumps.

A 70 psi differential must be maintained across each spray nozzle; this is controlled by the ³/₄" globe valves in each supply line and by varying pump speed (if available).

As described here, the control scheme is for fixed speed operation.

The driver PM-1695 has an O/O (On -Off) switch HS-1695 which allows the following:

- in Off, the pump is not running and will not start automatically
- in On, the pump is under PLC control and may stop or start automatically without warning

In normal operation, the switches should be set to "On".

Note that selecting "Off" for HS-1695A/B will only stop PM-1695A/B, not the dewpoint plant.

P-1695 Glycol Injection Pumps - Instruments			
Instrument Tag Location			
Pulsation Dampener	PD-1695A	Pump discharge line	
Pressure Gauge	PI-1696	Pump discharge line	
Temperature Gauge	TI-1695	Pump common suction line	
PSV	PSV-1695	Pump discharge line (blocked flow)	

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5.5 PROPANE (R290) REFRIGERATION SYSTEM

The Dew Point Control Plant relies on cooling the gas to condense heavier hydrocarbons and water. The cooling is provided by the propane refrigeration system. The refrigeration system is a closed loop, using propane (R290) as the refrigerant. The principal of operation is to compress low-pressure refrigerant vapour from the shellside of chiller E-1610, allowing the refrigerant to condense at high pressure using the atmosphere as the heat sink.

The refrigerant plant comprises 1 x 100% duty electric motor driven oil-flooded screw compressor complete with chiller surge drum, oil separator, propane coolant pump, oil cooler, oil filter, fin-fan condenser, accumulator and propane filter-driers.

The sections below describe the operation of the R290 loop, starting at the gas chiller E-1610.

5.5.1 Propane / Process Portion

5.5.1.1 Gas Chiller E-1610 (see also section 5.2.2 above)

The chiller E-1610 is a plate & shell flooded-type evaporator, 169 kW of duty and 18.8 sq.m transfer surface. Warm process gas in the tubes at 2100 kPag and -7 °C boils off liquid propane refrigerant at 117 kPaa and -38 °C in the chiller shell.

Refrigerant liquid from the accumulator V-1650 at 1310 kPag and 20 °C flows to the gas chiller E-1610 via level control valve LV-1610. The evaporating temperature in the chiller sets the pressure in the chiller (117kPaa) and thus the refrigerant compressor's suction pressure. The chiller is thus at low pressure and there is a pressure drop across LV-1611, resulting in cold liquid refrigerant and some flash vapour due to the Joule-Thompson effect. The cold two-phase flow enters the chiller where the cold low pressure liquid is fully evaporated by the warm HP gas in the chiller tubes and returns to the compressor via surge drum E-1615 to start a further cycle. The refrigerant level in the chiller is controlled to maintain the top tubes covered or to have the first row uncovered if some superheat is desired. The chiller shell level is measured by LT-1610 and is used by LIC-1610 to control LV-1610. The surge drum E-1615 acts as a scrubber to ensure separation of liquid droplets and allows for the R290 level to fluctuate during start without damaging the compressor.

As the HP gas flow varies the chiller duty will vary, resulting in changes in chiller pressure. As the chiller pressure varies it is measured by pressure transmitter PT-1615 and used by PIC-1610 to control the compressor slide valve. This allows the compressor capacity to match the required chilling duty by maintaining the required evaporating temperature (saturation temperature) via the evaporating pressure (saturation pressure).

A glycol injection connection is provided at the process gas inlet of E-1610. The chiller has a drip leg provided to remove compressor oil (as described in section 5.2.2)

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and the drip leg will be heated with heat tape to facilitate the removal of this oil from the system on an intermittent basis.

E-1610 / E-1615 Gas Chiller / Surge Vessel - Instruments			
Instrument	Тад	Location	
Pressure Gauge	PI-1615	Chiller Surge vessel (propane)	
Pressure Transmitter	PT-1615	Chiller Surge vessel (propane)	
Temperature Gauge	TI-1611	Process Gas In (gas)	
	TI-1610	Process Gas Out (gas)	
PSV	PSV-1615	Chiller Surge outlet line(fire)	
Glycol Flowmeter	FI-1615	Process side (gas)	
Level Gauge	LG-1610	Chiller Bridle (propane)	
Level Transmitter	LT-1610	Chiller Bridle (propane)	
Level Valve	LV-1610	Propane inlet to chiller	

5.5.1.2 Propane Compressor K-1660

The refrigerant compressor K-1660 is a Howden XRV 204-193-5.0 oil-flooded screw compressor. This type of rotary positive displacement compressor uses two meshing helical rotors to form pockets of reducing volume allowing compression of the vapour. The male rotor is driven by the electric motor KM-1660 and in turn drives the meshed female rotor. The rotors seal against the compressor casing and the slide valve to generate pressure as the pocket volume reduces. The volumetric capacity of the compressor is steplessly variable between 10% and 100% by use of a hydraulically-actuated slide valve. The slide valve is positioned directly below the rotors and can be moved axially along part of the rotors' length. As the slide valve moves it increases or decreases the portion of the rotors' volume that is available for compression, thus increasing or decreasing the throughput.

Compressor oil is injected into the compressor casing to lubricate bearings and shaft seal, to seal the clearances between the rotors and the casing and to remove some of the heat of compression. The oil is pressure fed to the compressor. Note that there are two oil supplies to the compressor casing

- a filtered oil flow to the bearings and mechanical seal (bearing oil)
- a strained oil flow to the rotors (injection oil)

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The compressor has a fixed Vi – Vi being the ratio of volume of gas in the rotors at suction conditions to the volume of gas in the rotors at discharge conditions. For a particular Vi, a change in suction pressure results in a change in discharge pressure. Changes in either the suction or discharge conditions for the compressor may require a change in Vi to prevent over-compression or under-compression within the compressor rotors. If the customer wishes to change the operating conditions of the compressor it is recommended that Startec or other qualified screw compressor service Company review the suitability of the machine for the revised conditions.

There is a cone type strainer with 60 gauge mesh in the suction line of the compressor (immediately above the compressor suction flange).

K-1660 Propane Compressor - Instruments			
Instrument	Тад	Location	
Differential Pressure Gauge	DPI-1660	Suction line (across strainer)	
Pressure Transmitter	PT-1660	Suction line (d/s strainer)	
	PT-1615	Chiller Surge	
Temperature Gauge	TI-1664	Suction line	
Thermocouple	TE-1663	Suction line	
Vibration Switch	VSHH-1661	Compressor casing	
Position Transmitter	ZT-1660	Compressor slide valve casing	

Cold refrigerant vapour at design conditions of 114 kPaa and -35 °C is compressed to 1414 kPaa and 95 °C in K-1660.

5.5.1.3 Propane Compressors Driver KM-1660

The driver is a 3/60/460VAC TEFC induction motor, nominal speed 3600rpm, CSA approved for Class 1 Div 2. The motor delivers 250 HP and is suitable for VFD duty with a turndown of 2:1. The motor has a space heater.

The compressor is driven via a spacer type disc pack coupling (DBSE 7"); the coupling hubs are attached to the motor and compressor shafts and are removable in position.

KM-1660 Propane Compressor Driver - Instruments			
Instrument Tag Location			
Space Heater	HTR-1661 / TS-1661	Motor	

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KM-1660 Propane Compressor Driver - Instruments				
Instrument Tag Location				
Vibration Switch VSHH-1662 Motor casing				

5.5.1.4 Propane Compressor Oil Separator V-1670

The hot compressed refrigerant / oil mixture is separated in oil separator V-1670. The separator is a vertical vessel (24" OD x 120" s/s).

The oil is separated by change in direction, gravity and finally by coalescing elements within the oil separator shell. The discharged propane vapour will contain no more than 10ppm (by weight) of compressor oil. The coalescing elements are replaceable, accessed via the man-way.

The separator contains immersion heaters HTR-1670 & HTR-1671 to maintain the oil at a minimum temperature when the compressors are not running. Ensure these heaters are energised when the compressors are off, de-energised when the compressors are running. The heaters have a built-in adjustable thermostat to control the oil temperature. TE-1672 is provided to measure oil temperature and provide a startup permissive and setpoint for the temperature control.

The retention allowed in the oil separator provides discharge oil with minimal entrained gas. Note that the oil will absorb propane, which reduces viscosity (allowed for in the oil selection) and will froth easily when de-pressured. The oil separator is also the reservoir for the compressor oil.

Fill and drain valves are provided. The drain allows the oil to be dumped to the drain header or to be collected for re-use.

V-1670 Oil Separator - Instruments			
Instrument	Тад	Location	
Pressure Gauge	PI-1671	Oil separator shell	
Pressure Transmitter	PT-1675	Oil separator shell	
Temperature Gauge	TI-1671	Oil separator shell	
Thermocouple	TE-1670	Oil separator shell, vapour	
	TE-1672	Oil separator shell, oil	
PSV	PSV-1672	Oil separator shell (blocked flow)	
Sight Glass	SG-1670	Oil separator shell	

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V-1670 Oil Separator - Instruments			
Instrument	Тад	Location	
Sight Glass	SG-1671	Oil separator shell	
Level Switch	LSL-1671	Oil separator shell	
Heaters	HTR-1670	Oil separator shell	
	HTR-1671	Oil separator shell	
Flow Indicator	FI-1670	Secondary oil return	

5.5.1.5 Propane Condenser AC-1655

From the compressors the hot refrigerant vapour goes to differential pressure control valve DPCV-1670 then to the condenser AC-1655 which is a fin-fan type with twelve (12) fan motors ACM-1655A/B/C/D/E/F and ACM-1656A/B/C/D/E/F that are staged in pairs to come on and off as the condensing load changes. The outlet temperature can also be controlled by an adjustment to the air flow by opening and closing the auto-louvres situated on top of the condenser. The condenser cools the hot refrigerant vapour against ambient air – firstly de-superheating the vapour and then totally condensing the vapour. The condensing (saturation) temperature sets the (saturation) pressure in the condenser and thus the compressors' discharge pressure. The condensing temperature is measured by TE-1655 and used by TIC-1655 to control the fan motors ACM-1655/1670 and the louvres TV-1655 to maintain 46 °C. At times of low ambient this system will not be able to control the condensing conditions and a winter pressure control system is provided to compensate (see section 5.5.1.9 below for description).

AC-1655 Propane Condenser - Instruments			
Instrument Tag Location			
Thermocouple	TE-1655	Discharge line	
PSV	PSV-1655	Inlet line (fire)	
Vibration Switch	VSHH-1655A/B	Fan motors	
Vibration Switch	VSHH-1656A/B	Fan motors	

5.5.1.6 Propane Accumulator V-1650

This pressure vessel has a TCRN registration provided by the transport authorities that allows for the transport of the propane which is considered a hazardous material. The condensed liquid refrigerant from AC-1655 flows by gravity to the accumulator V-1650 (30" OD x 96" s/s). This vessel is designed to hold the entire refrigerant charge when the propane recovery plant needs to be transported to a new location or when the system requires maintenance. It also provides a buffer

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volume to accommodate process changes, process upsets and the reduced circulation rate required in winter. Normally the vessel will run around 20% full and will hold the entire charge when 80% full.

Note that the accumulator can also be described as "receiver".

V-1650 Propane Accumulator - Instruments			
Instrument Tag Location		Location	
Temperature Gauge	TI-1657	Accumulator shell	
PSV	PSV-1652	Accumulator shell (fire)	
Level Gauge	LG-1650	Accumulator shell (float gauge)	
Level Transmitter	LT-1650	Accumulator shell	

5.5.1.7 Propane Filter-Driers F-1646

The propane may contain water; water in the refrigeration system is not desirable as it may freeze. The filter-driers F-1646 contain absorbent cores which will remove water and maintain the system's dryness. This design uses one filter-drier vessel with the entire propane flow passing continually through the three.

The filter can also be used in a slipstream mode. The amount of flow that bypasses the filter is controlled by the manual 2" globe valve between the filter inlet and outlet connections. The bypass flow is typically 10% of the total flow. During startup the drier cores will have to be changed frequently as any water in the propane charge is removed. After startup the charge should be clean and dry and, unless propane is added to the system, it will not be necessary to change cores often. Inspection/replacement frequency can be advised by the Startec startup mechanic after he has assessed the system.

F-1646 Propane Filter-Drier - Instruments			
Instrument Tag Location			
Differential Pressure Gauge	DPI-1646	Filter shell	

5.5.1.8 Hot Gas Bypass

The propane refrigeration system has a hot gas bypass valve (HGBP) PCV-1610. This allows hot gas from the compressor discharge to flow into the propane side of gas chiller E-1610. The hot gas is de-superheated and evaporates some of the liquid in the chiller shell and is used to maintain flow to the compressor when the process

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load is below the turndown of the compressor (<10% capacity). Also known as a phantom load, the HGBP can be used to run the R290 system during commissioning or after maintenance when process gas may not be available. The HGBP value is a regulator-type control value and is controlled by sensing pressure from the compressor suction line.

5.5.1.9 Low Ambient Pressure Control

The propane refrigeration system has winter pressure control for low ambient operation. When the ambient temperature is low it is possible for the condensing pressure to drop below that needed to circulate refrigerant from the accumulator to the chiller. To compensate for this and ensure that sufficient pressure is available to circulate refrigerant, the following controls are installed:

- a discharge differential pressure control valve DPCV-1670. This valve maintains a minimum compressor discharge pressure of 1034 kPag. This prevents
 oil carry over which may occur at low oil separator pressure and provides a minimum pressure to maintain refrigerant circulation. Note this valve is
 usually fully open.
- accumulator pressure maintenance control valve PCV-1650, set at 900 kPag. This valve allows hot gas from the compressor discharge to enter the cold accumulator. This maintains pressure in the accumulator to circulate refrigerant.
- check valve in the line from the condenser AC1655 to the accumulator V-1650. This valve allows liquid to back up into the condenser, flooding some of the tubes and reducing the effective capacity. This allows the condensing temperature to rise and hence the condensing pressure. When the condensing pressure becomes greater than the accumulator pressure, the check valve allows liquid to flow to the accumulator. The accumulator pressure is now above the setpoint of PCV-1650 and this valve closes. With liquid flowing from the condenser the flooded tube volume decreases, the condensing pressure drops, PCV-1650 opens and the condenser starts to flood again. This cycle repeats for as long as low ambient conditions exist

5.5.2 Compressor Oil and Oil Cooling Portion

5.5.2.1 General

The screw compressor requires a continuous supply of oil to lubricate and seal the machine. Oil that is injected into the compressor is mixed with the refrigerant vapour and discharged to the oil separator

V-1670. The oil is separated from the refrigerant vapour by gravity settling and the majority of the remaining oil mist is removed in the coalescing section of the oil separator. The discharged refrigerant stream will contain no more than 10ppm by weight of oil when properly maintained and operated.

5.5.2.2 Positive Compressor Oil Delivery

The separated oil flows by source pressure delivery from the oil separator V-1670 to the oil cooler E-1670. Positive delivery of the oil to the compressor is ensured by

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monitoring the lube oil delivery header pressure (PT-1677) to compressor suction pressure (PT-1615) and the lube oil delivery header pressure (PT-1677) to the oil separator/compressor discharge pressure (PT-1675). a differential of 207 kPa between the oil separator and the oil supply header. ??????? more information on XRV control.

5.5.2.3 Compressor Oil Cooler E-1670 and Oil Filters F-1675A/B

Oil from V-1670 flows to the oil cooler E-1670 to be cooled prior to its delivery to the compressor.

The oil is cooled against propane to 66 °C. From E-1670 the oil stream splits:

- One stream is strained and flows to the rotor injection port. This oil is injected into the rotor flutes to cool, lubricate and seal the rotor / casing clearance. A manual globe control valve is provided for flow control this will be used to match the oil flow to the desired discharge temperature during commissioning. Improper adjustment of this valve can lead to compressor performance problems or failure Startec's Mechanic will adjust this valve and advise on its operation.
- The remainder flows to oil filters F-1675A/B. These 10 micron elements filter the oil that is provided to the compressor bearings and shaft seal. There are 2 x 100% filters; the elements are replaceable in operation. Note: each filter body has two isolation valves during operation three of the four valves must be open to prevent damage to the off-line filter body by liquid expansion. A differential pressure gauge DPI-1675 is also provided across the elements providing a measure of performance.

Oil from the filters flows to the oil supply header for distribution into the compressor bearings and seal. The oil supply temperature is monitored by TE-1675 to prevent either low or high oil temperatures.

Compressor Oil Cooler E-1670 and Oil Filter F-1675A/B - Instruments			
Instrument	Тад	Location	
Pressure Gauge	PI-1669	Oil pump discharge line	
	PI-1676	Oil cooler oil outlet	
	PI-1678	Oil header	
Differential Pressure Gauge	DPI-1675	Across oil filters	

The oil injected via the rotor port and the bearing / seal ports is discharged to the oil separator to start another cycle.

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Compressor Oil Cooler E-1670 and Oil Filter F-1675A/B - Instruments				
Instrument	Тад	Location		
Pressure Transmitter	PT-1675	Oil Separator		
	PT-1677	Oil header		
Temperature Gauge	TI-1672	Oil from Oil Separator		
	TI-1677	Oil cooler outlet (oil)		
Thermocouple	TE-1675	Oil header		
Temperature Control Valve	TCV-1668	Oil cooler (oil side)		

5.5.2.4 Propane Oil Coolant Pump P--1655

The oil is cooled from compressor discharge temperature to the required supply temperature of 66°C. The coolant is liquid propane. The propane coolant is cooled as an additional load added to the propane condenser where it is cooled against ambient air. Propane coolant pump P-1655 circulates the propane liquid to the oil cooler E-1670 and is flashed and develops enough pressure to enter the AC-1655 propane condenser inlet stream.

There are no controls on this circuit other than manual globe flow control valve at P-1655 discharge. This valve should be set to maintain the pump's desired operating point on its curve while delivering the propane flow required to cool the compressor oil.

The driver PM-1655 has an HOA (Hand-Off-Auto) switch HS-1655 which allows the following:

- in Off, the pump is not running and will not start automatically
- in Auto, the pump is under PLC control and may stop or start automatically without warning
- in Hand, the pump is running and is under local control by the operator

In normal operation, the switch should be set to "Auto".

Note that selecting "Off" for HS-1655 will only stop PM-1665, not the propane recovery plant. The propane recovery plant may stop automatically shortly after as a result of stopping PM-1665 because some process variable has gone beyond it's safe limit.

Propane Oil Coolant Pump P-1655 - Instruments

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Instrument	Тад	Location
Pressure Gauge	PI-1655	Propane coolant pump discharge line

5.6 INSTRUMENT AIR

Each trailer has an instrument air header to supply the pneumatic devices on that skid. The header has valved off-takes, including a spare, and a drain. The air is provided from the utility trailers instrument air system – note there is no initial pressure reduction or filtering on the skids, only at the individual devices if required. Instrument air vented by various users is released to the atmosphere. The minimum air header pressure required for valve actuator operation is 80 psig.

5.7 FUEL GAS / BLANKET GAS

There is only one fuel gas requirement. On the vessel trailer fuel gas is used to blanket / pressurize the glycol flash tank V-1680. The fuel gas is regulated by self-contained Fisher outlet pressure regulator PV-1682.

Fuel gas is vented from BPCV-1681 on the flash tank to the flare header. Blanket gas for the distillation column and is discharged via the overheads to the process. Note: this may result in off-spec product from the debutaniser for a short period after restart.

During a blowdown, BDV-1681 on the flash tank will open and vent fuel gas to the flare. To avoid the loss of fuel gas, Customer should ensure that the fuel gas supply is isolated during blowdown.

5.8 DRAINS AND VENTS

The skids are provided with the following drains and vents:

	Skid #2	Discharge From
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Sweet Flare Header	Yes	Yes	PSVs, BDVs, PVs
(Common to both skids)			
Sweet Liquid Drain	Yes	Yes	hydrocarbon liquids from process
(Separate drain for each			and instruments, hot oil, glycol
skid)			
EG/Water Drain	No	Yes	EG from LTS, vent condenser,
			glycol regenerator, glycol filters.

All flare headers and drain headers are provided as skid edge connections for the customer to pipe to.