



CALHEX INDUSTRIES LTD.

9515 - 48 th. Street S.E., Calgary, Alberta, T2C 2R1

Bus: (403) 225 - 4395
Fax: (403) 261 - 2761

{ CALHEX5 }

DATA BOOK

Installation, Maintenance and Operation Manuals

SHELL AND TUBE HEAT EXCHANGERS

Customer:	EXCELSIOR ENGINEERING LTD.
For:	HUSKY OIL OPERATIONS
Drawing Description:	INLET GAS HEAT EXCHANGER
Calhex Industries Job #:	12-0779
Tag#:	E-102B
Purchase Order #:	8400547676
Vendor Document #:	12-0779
C.R.N.#:	V9688.21
Location:	Husky Oil Ansell Gas Plant
	Edson, AB

CONTENTS

DATA SHEETS

1. Equipment / Electrical Data Sheets
2. Design Calculations

DRAWINGS

3. Complete Set "CERTIFIED AS BUILT" Drawings

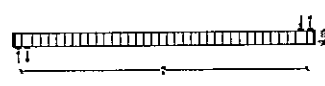
MANUALS

4. Installation, Operating & Maintenance Manuals

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LINE NO.	REV NO.		CALHEX INDUSTRIES LIMITED 9515-48th Street SE Calgary, Alberta	Rev. No.: 2 Cust. Ref. #: 3244		
SHELL and TUBE HEAT EXCHANGER SPECIFICATION SHEET - Imperial Unit						
1	0	Customer: <u>EXCELSIOR ENGINEERING</u>			Prop. No.: Q-12-2218	
2	2	Address: <u>Calgary, Alberta</u>			Date: September 14, 2012	
3	1	Plant Location: <u>Husky Oil Operations LTD.: Ansell Gas Plant</u>			Ref. No.: Q-12-2218 E-102B C2W R1	
4	0	Service of Unit: <u>Inlet Gas Heat Exchanger (Case 2 Winter)</u>			Item No.: E-102B	
5	0	TEMA type & Size (in): <u>NEN 23 x 576</u>		Connected In: <u>1-series / 1-parallel</u>		
6	0	Surface Area (ft²) → Per Unit (eff.) / Per Shell (gross) / Per Shell (eff.): <u>10570.3 / 4146.9 / 10570.3</u>				
PERFORMANCE OF ONE UNIT						
		SHELL SIDE			TUBE SIDE	
8	0	Fluid Allocation		Discharge Gas		
9	0	Fluid Name		Inlet Gas		
10	0	Fluid Quantity (Total)	lb/hr	36,880.5		
11	1	Vapor (In/Out)	lb/hr	36,880.5	36,852.9	
12	1	Liquid	lb/hr	-	27.6	
13	0	Steam	lb/hr	-	-	
14	0	Water	lb/hr	-	-	
15	0	Non-Condensables	lb/hr	-	-	
16	1	Temperature (In/Out)	°F	86.0	41.1	
17	1	Density	lb/ft³	1.1154 V/L	1.2171 V/L 41.93	
18	1	Viscosity	cP	0.0110 V/L	0.0110 V/L 0.306	
19	0	Molecular Weight, Vapor				
20	0	Molecular Weight, Non-Condensables				
21	1	Specific Heat	Btu/lb-°F	0.5271 V/L	0.5191 V/L 0.49	
22	1	Thermal Conductivity	Btu/hr-ft-°F	0.0191 V/L	0.0176 V/L 0.069	
23	0	Latent Heat	Btu/lb			
24	1	Inlet Pressure	psia	307.50		
25	1	Velocity, Average	ft/sec	9.59		
26	1	Pressure Drop, Allow./Calc.	psi	4.35	3.51	
27	0	Fouling Resistance (min)	ft²-hr-°F/Btu	0.0010		
28	1	Total Heat Exchanged:	862,314 Btu/hr	MTD (Corrected): 6.4 °F		
29	1	Transfer Rate (Btu/ft²-hr-°F) →		Service / Clean: 12.69 / 15.12		
CONSTRUCTION OF ONE SHELL						
		Shell Side			Tube Side	
32	1	Design/Vac./Test Pressure	psig	400	FV	Code
33	2	Design Temperature (Max/Min)	°F	163	/	-49
34	0	No Passes per Shell		1		
35	0	Corrosion Allowance	inches	0.0625		
36	0	Connections	Inlet: (1) 8	300#	RFWN	(1) 8 300# RFWN
37	0	Nom. Size & Rating (Inches)	Outlet: (1) 8	300#	RFWN	(1) 8 300# RFWN
38	0		Intermediate: (-) -	-	-	(-) - -
		SHELL DETAILS			BAFFLE & BUNDLE INTERNAL DETAILS	
40	2	Shell Cylinder / Head	SA-333-6	Stationary Tubesheet(s)		SA-516-70N
41	0	Shell Cyl. ID / OD (in)	23.0000	24.0000	N/A	
42	0	Kettle Cyl. ID / OD (in)	n/a	n/a	Baffle Material	
43	0	Shell Girth Flange(s)	n/a	Baffle Type / Orientation		Single-Seg. / Parallel
44	0	Aux. Shell Cyl. JOD (in)	N/A	Baffle No.		34
45	0	Expansion Jt. / Mat.	n/a	Spacing (Frt/C-C/Rear) (in)		22.562 / 16.000 / 22.562
46	2	Shell Nozz. Flg.	SA-350-LF2	Baffle Cut (% Dia.)		35.41 %
47	2	Shell Nozz. Neck	SA-333-6	Longitudinal Baffle / Seal		n/a
		EXAMINATION DETAILS			GASKET & BOLTING DETAILS	
49	2	Front Ch. Cylinder	SA-333-6	Shell Side Girth:		n/a
50	0	Frt. Ch. Cyl. ID / OD (in)	23.0000	24.0000	Tube Side Girth:	
51	2	Rear Ch. Cylinder	SA-333-6	Floating Tubesheet		Spiral Wnd T-304SS "CG"
52	0	Rr. Ch. Cyl. ID / OD (in)	23.0000	24.0000	Floating head:	
53	2	Front Ch. G.Fl./ Cvr.	SA-350-LF2	SA-350-LF2	Shell side nozzles:	
54	0	Rear Ch. G.Fl./ Cvr.	N/A	N/A	Tube side nozzles:	
55	2	Channel Nozz. Flg.	SA-350-LF2	Girth Bolting:		SA-193-B7
56	2	Channel Nozz. Neck	SA-333-6	SS Nozz. Bolting:		SA-193-B7
57	0	Impingement Protection: None - Not Required			Tube to Tubesheet Joint: Dbl. Ring Grooved - Rolled Expanded	
58	0	Est. Wgts per shell:	Wet: 32,719 lbs	Dry: 24,709 lbs	Bundle: Fixed lbs	
59	0	Rho-V-Sqd (lb/ft-sec²):	Shell Inlet/Outlet: 936 /	857	Tube Inlet/Outlet: 2477 / 2862	
60	-	Code Requirements:	ASME Sec VIII, Div.1		Registered in: AB & BC	
61	-	Remarks: Thermal Rating By Shell and Tube Software HTRI.				
62	1	1. Design includes 10.99% excess surface area.				
63	1	2. Case 2 winter datasheet for performance above, Summer case governs				
64	0	3. Sweet service both sides				
65	0	4. Anti-vibration baffles required under shell nozzles				
66	0	5. Lo-finned tubing 19 fins per inch, 16 ga (.065" thick) under the fins, 14 ga at bare ends				
67	0					
68	0					
69	0					
70	0					
71	0					

LINE NO.		REV NO.		 CALHEX INDUSTRIES LIMITED 9515-48th Street SE Calgary, Alberta		Rev. No.: 2	
				Cust. Ref. #: 3244			
SHELL and TUBE HEAT EXCHANGER SPECIFICATION SHEET - Metric Unit							
1	0	Customer: EXCELSIOR ENGINEERING				Prop. No.: Q-12-2218	
2	2	Address: Calgary, Alberta				Date: September 14, 2012	
3	1	Plant Location: Husky Oil Operations LTD.: Ansell Gas Plant				Ref. No.: Q-12-2218 E-102B C2W R1	
4	0	Service of Unit: Inlet Gas Heat Exchanger (Case 2 Winter)				Item No.: E-102B	
5	0	TEMA type & Size (mm): NEN 584 x 14630		Connected In: 1-series / 1-parallel			
6	0	Surface Area (m²) →		Per Unit (eff.) / Per Shell (gross) / Per Shell (eff.):		982 / 385.2 / 982	
PERFORMANCE OF ONE UNIT							
Fluid Allocation		SHELL SIDE			TUBE SIDE		
Fluid Name		Discharge Gas			Inlet Gas		
Fluid Quantity (Total)		16,729.0			16,128.0		
11	1	Vapor (In/Out)	kg/hr	16,729.0	16,716.5	16,128.0	16,128.0
12	1	Liquid	kg/hr	--	12.5	--	--
13	0	Steam	kg/hr	--	--	--	--
14	0	Water	kg/hr	--	--	--	--
15	0	Non-Condensables	kg/hr	--	--	--	--
16	1	Temperature (In/Out)	°C	30.0	5.0	0.0	27.4
17	1	Density	Kg/m³	17.87	19.50	6.27	5.43
18	1	Viscosity	cP	0.0110	0.0110	0.0100	0.0201
19	0	Molecular Weight, Vapor		--	--	--	--
20	0	Molecular Weight, Non-Condensables		--	--	--	--
21	1	Specific Heat	kJ/kg·°C	2.207	2.173	2.034	2.094
22	1	Thermal Conductivity	W/m·°C	0.033	0.030	0.028	0.032
23	0	Latent Heat	kJ/kg	--	--	--	--
24	1	Inlet Pressure	kPa (abs)	2120.1		696.4	
25	1	Velocity, Average	m/sec	2.92		14.08	
26	1	Pressure Drop, Allow./Calc.	kPa	30.0	24.2	70.0	18.0
27	0	Fouling Resistance (min)	m²·°C/W	0.000176		0.000176	
28	1	Total Heat Exchanged:	252.5 kW	MTD (Corrected): 3.6 °C			
29	1	Transfer Rate (W/m²·°C) →		Service / Clean: 72.05 / 85.85			
CONSTRUCTION OF ONE SHELL							
Design/Vac./Test Pressure		kPa		2,758 FV		2,758 FV	
Design Temperature (Max/Min)		°C		73 / -45		70 / -45	
No Passes per Shell				1		1	
Corrosion Allowance		mm		1.6		1.6	
Connections		Inlet: (1) 8		(1) 8		300# RFWN	
Nominal Size & Rating (Inches)		Outlet: (1) 8		(1) 8		300# RFWN	
		Intermediate: (--) --		(--) --		-- --	
SKETCH:							
							
INTERNAL DETAILS							
Shell Cylinder / Head		SA-333-6		Stationary Tubesheet(s)		SA-516-70N	
Shell Cyl. ID / OD (mm)		584.2 / 609.6		Floating Tubesheet		N/A	
Kettle Cyl. ID / OD (mm)		n/a / n/a		Baffle Material		G-44W (SA-36)	
Shell Girth Flange(s)		n/a		Baffle Type / Orientation		Single-Seg. / Parallel	
Aux. Shell Cyl. / OD (mm)		n/a / n/a		Baffle No.		34	
Expansion Jt. / Mat.		n/a		Spacing (Frt/C-C/Rear) (mm)		573 / 406 / 573	
Shell Nozz. Flg.		SA-350-LF2		Baffle Cut (% Dia.)		35.41 %	
Shell Nozz. Neck		SA-333-6		Longitudinal Baffle / Seal		n/a	
GASKET & BOLTING DETAILS							
Front Ch. Cylinder		SA-333-6		Shell Side Girth:		n/a	
Frt. Ch. Cyl. ID / OD (mm)		584.2 / 609.6		Tube Side Girth:		Spiral Wnd T-304SS "CG"	
Rear Ch. Cylinder		SA-333-6		Floating head:		n/a	
Rr. Ch. Cyl. ID / OD (mm)		584.2 / 609.6		Shell side nozzles:		Spiral Wnd T-316SS "CG"	
Front Ch. G.Fl./ Cvr.		SA-350-LF2		Tube side nozzles:		Spiral Wnd T-316SS "CG"	
Rear Ch. G.Fl./ Cvr.		N/A		Girth Bolting:		SA-193-B7	
Channel Nozz. Flg.		SA-350-LF2		SS Nozz. Bolting:		SA-193-B7	
Channel Nozz. Neck		SA-333-6		1- Bare bolt and nut, 2- Painted Bolt and nut, 3- Electro Galvanized, 4- Hot Dipped Galvanized			
IMPINGEMENT PROTECTION: None - Not Required							
Est. Wgts per shell:		Wet: 14,841 Kg		Dry: 11,208 Kg		Bundle: Fixed Kg	
Rho-V-Sqrd (kg/m·sec²):		Shell Inlet/Outlet: 1393 / 1275		Tube Inlet/Outlet: 3686 / 4259			
Code Requirements:		ASME Sec VIII, Div.1		Registered In:		AB & BC	
Remarks:		Thermal Rating By Shell and Tube Software HTRI.		TEMA Type:		'R'	
61	0	1. Design includes 10.99% excess surface area.					
62	1	2. Case 2 winter datasheet for performance above, Summer case governs					
63	1	3. Sweet service both sides					
64	0	4. Anti-vibration baffles required under shell nozzles					
65	0	5. Lo-finned tubing 19 fins per inch, 16 ga (.065"thick) under the fins, 14 ga at bare ends					
66	0						
67	0						
68	0						
69	0						
70	0						
71	0						

**CALHEX INDUSTRIES LTD.**

9515 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
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NEN CALCULATION VERSION 2.0, JAN. 26, 2011 (NOV. 26, 2001)

CALCULATION COVER SHEET

Page number: 1 of 21

DESIGN CALCULATIONS INDEX

Calculation Description	Applicable		Pages	Rev. Level
	Yes	No		
Primary Membrane Stress Calcs. (Spread sheet pgm.)	✓		2-14	0
Lifting Lug Calculations	✓		15	0
Horizontal Vessel Saddle Calculations	✓		16	0
Vertical Vessel skirt Calculations		✓		0
Other UG-22 Specified Loadings		✓		0
Vessel Impact Testing Exemption Summary	✓		1	0

REVISION LOG

REV.#: 0 Initial issue
1 Radiography

JOB INFORMATION

Job #: 12-0779 **Type:** NEN 23x576 **Size:** 10570.3 FT²
Customer: EXCELSIOR ENGINEERING **Owner:** HUSKY OIL OPERATIONS
Date: December 13, 2012 **By:** Jim Gregory
Checked: Martin Sojka
Approved: *DR* DEC 12/12

SHELL & TUBE EXCHANGER DESIGN CONDITIONS

Shell side					Tube side				
Design Pressure:	400	psi	~	2758 Kpa	400	psi	~	2758 Kpa	
Vacuum Pressure:	15	psi	~	103 Kpa	15	psi	~	103 Kpa	
Design Temperature:	163	°F	~	72.8 °C	158	°F	~	70.0 °C	
Corrosion Allowance:	0.0625	in	~	1.6 mm	0.0625	in	~	1.6 mm	
Radiography:	sopt per UW-11(a)5(b)				sopt per UW-11(a)5(b)				
Efficiency- LS / CS:	0.85	/		1.00	N/R	/		1.00	
Minimum Design Temp.:	-49				-49				
Post Weld Heat Treat:	NO				NO				

ALL MATERIAL STRESSES VALUES PER ASME SEC. II, PART D, 2010 EDITION 2011ADD.

VESSEL C.I.T. NOTES

- 1) Vessel C.I.T. exemption per UCS-66(a)(c)(d)(g), FIG UCS-66 NOTE(e), UCS-67(a)2

NOTES

- 1) NOZZLES 2" & UNDER EXEMPT PER UG-36-(c)3(a)

**CALHEX INDUSTRIES LTD.**

1515 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4385 (CALHEX3)

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CYLINDER THICKNESSES

Job number: 12-0779

Revision number: 0

Page number: 2 of 21

CODES:

Thickness of shell under internal pressure per : ASME SEC. VIII, DIV. 1 2010ED. 2011ADD. UG-27

Thickness of shell under external pressure per : ASME SEC. VIII, DIV. 1 2010ED. 2011ADD. UG-28

Shell side:

Material : SA-333-6 S or W: S Allow. Amb. Stress: 17100 psi
Pipe~ 1 / Plate~ 2 : 1 Allow. Design Stress: 17100 psi
Pipe OD: 24 in Is Corrosion Allowance applicable to material: Y
Design Pressure: 400 psi Design Temp.: 163 °F Corrosion Allowance: 0.0625 in
Efficiency: 1.00 Thickness Calculation includes 12.5% pipe tolerance

	Minimum Thickness (including CA)		Actual Thickness
$t = \frac{DP \cdot OD/2}{SE + (DP \cdot 0.4)} + CA$	0.3893	IN	0.5000 IN

MAWP ambient and uncorroded = 632.7 psi

MAWP hot and corroded = 541.1 psi

Tube side:

Material : SA-333-6 S or W: S Allow. Amb. Stress: 17100 psi
Pipe~ 1 / Plate~ 2 : 1 Allow. Design Stress: 17100 psi
Pipe OD: 24 in Is Corrosion Allowance applicable to material: Y
Design Pressure: 400 psi Design Temp.: 158 °F Corrosion Allowance: 0.0625 in
Efficiency: 1.00 Thickness Calculation includes 12.5% pipe tolerance

	Minimum Thickness (including CA)		Actual Thickness
$t = \frac{DP \cdot OD/2}{SE + (DP \cdot 0.4)} + CA$	0.3893	IN	0.5000 IN

MAWP ambient and uncorroded = 632.7 psi

MAWP hot and corroded = 541.1 psi

Tubing:

Material : SA-179 S or W: S Allow. Amb. Stress: 13400 psi
Tube OD: 0.750 in Allow. Design Stress: 13400 psi
Tube Length: 576 in Is Corrosion Allowance applicable to material: N
Design Pressure: 400 psi Design Temp.: 163 °F Corrosion Allowance: 0 in
Efficiency: 1.00

	Minimum Thickness Internal Pressure		Actual Min. Thickness
$t = \frac{DP \cdot OD/2}{SE + (DP \cdot 0.4)} + CA$	0.0111	IN	0.0830 IN

Maximum External Pressure for Tube thickness

Do / t = 9.0361 EXTERNAL PRESSURE CHART # : CS-1
L / Do = 50.000 A = 0.01414 Ext. Yield Stress: 27600
B = 13800 S : 24840

Pa = - Pa1 = 2159.9

Pa2 = 4889.5

Maximum Allowable external Pressure : 2159.9 Existing external Pressure : 415.0

**CALHEX INDUSTRIES LTD.**

9816 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4385 (CALHEX)
Fax: (403) 261 - 2761**TUBESHEET THICKNESS CALCULATION**Job number: 12-0779
Revision number: 0 | Page number: 3 of 2/**CODES:**

ASME SEC VIII, DIV. 1 2010 ED, 2011 ADD. UHX-13, & FIG UHX-13.1 (a)

DIMENSIONS & PROPERTIES

	<u> Tubes </u>	<u> Channel </u>	<u> Shell </u>	<u> Tubesheet </u>
Material :	SA-179	SA-333-6	SA-333-6	SA-516-70N
Design Pressure, P_t, P_s :	415		415	see EFF. DP.
Design Temperature T_t, T_c, T_s, T_r :	163	158	163	163
Mean Oper. Temp.'s, $T_{t,m}, T_{s,m}, T_r$:	65.24	-	66.36	83.7
Inlet / Outlet temp. at hot end, T_c, T_s :	-	81.3	86	-
Ambient Allowable Stress :	13400 *	17100	17100	20000
Design temp Allowable Stress :	13400 *	17100	17100	20000
Operating temp Allowable stress :	13400 *		17100	20000
Diameters, d_t, D_c, D_s :	0.75	23	23	-
Thicknesses, t_t, t_s, h :	0.0830	0.5000	0.5000	1.5625
Corrosion Allow., $C_t, C_s, C_{t,s}$:	-	0.0625	0.0625	0.1250
Poisson's ratio ν_t, ν_c, ν_s, ν :	0.28	0.3	0.3	0.3
Elas. Mod @ ds. Temp., E_t, E_c, E_s, E :	2.779E+07	2.879E+07	2.879E+07	2.879E+07
Elas. Mod @ op. Temp., E_t, E_s, E :	2.833E+07	2.930E+07	2.930E+07	2.920E+07
Coeff. of Thermal Exp. at op. temp, $\alpha_{t,m}, \alpha_{s,m}, \alpha'$:		6.396E-06	6.399E-06	6.451E-06
Coeff. of Thermal Exp. at In/out. temp, α_c', α_s' :		6.444E-06	6.458E-06	-

NOTE: P_t & P_s are adjusted for vacuum pressure on opposite side when noted on pg 1. If both sides have vacuum both P_s & P_t are adjusted at the same time for a single conservative calculation, rather than running 2 calcs adjusting P_s and P_t individually.

* Tube stresses are for seamless tubing per note UHX-11.3 and UHX-13.3

<u> Tube characteristics: </u>		<u> No. of Tubes, N_t :</u>	<u> 440 </u>	<u> Tube Length, L_t :</u>	<u> 576 </u>
Tube joint Expanded (Y/N):	y	No. Of Grooves(2/1/0):	2	Expansion length, l_x :	1.5625
Tube joint Welded (Y/N):	n	Weld throat length, a :	0	Tube testing (Y/N):	N
Tube Pitch, p :	0.96875	Pattern :	30	Tube Projection :	0.125
Outer tube limit, Do: 22.3902		Tube Jt., L_{max} :	1631.39	Pass plate (Y or N) :	N
Total Area of untubed lanes, $A_L = \Sigma(U_L \cdot L_{tL})$:			0		
Unsupported span TS to Baffle:	38.5625	Unsupported span Baff to Baff:			32.000
Tube layout perimeter if required, C_p :	-	Area enclosed by C_p , if required, A_p :			-

Errors:

EXPANSION JOINT DIMENSIONS AND PROPERTIESIs an Expansion Joint required ? (Y or N) : N Joint Material :
Axial Rigidity, K_j = 0 Joint Inside Diameter, D_j = 0
Is Corrosion applicable to joint Material ? (Y or N) : N**IS THE UNIT TO EXPERIENCE CYCLICAL SERVICE OR DYNAMIC LOADING (Y or N) :** N**CALCULATIONS****GEOMETRY VALUES**

μ =	0.225806452	d^* (Load cases 1 to 3) NEW =	0.6426
p_{new} =	1.0000	d^* (Load cases 4 to 7) NEW =	0.6421
p_{corr} =	1.0000	d^* (Load cases 1 to 3) CORR =	0.6426
p^* =	0.9688	d^* (Load cases 4 to 7) CORR =	0.6421
h_g =	0.0000	μ^* (Load cases 1 to 3) NEW =	0.3366
a_o =	11.1951	μ^* (Load cases 4 to 7) NEW =	0.3372
h_g' (1 to 3) new =	0.0000	μ^* (Load cases 1 to 3) CORR =	0.3366
h_g' (1 to 3) corr =	0.0000	μ^* (Load cases 4 to 7) CORR =	0.3372
h_g' (4 to 7) both =	0.0000		

**TUBE-SHEET THICKNESS CALCULATION cont.'d**Job number: 12-0779
Revision number: 0

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ps NEW =	1.0272	ps CORR =	1.0328	pc NEW =	1.0272	pc CORR =	1.0328
L NEW =	572.6250	L CORR =			572.7500		
Xs =	0.5063	Xt =			0.7007		

STIFFNESS FACTORS

K _s NEW (Case 1 to 3) =	1855597.0	K _t NEW (Case 1 to 3) =	8439.1
K _s NEW (Case 4 to 7) =	1888914.6	K _t NEW (Case 4 to 7) =	8604.4
K _s CORR (Case 1 to 3) =	1627610.3	K _t CORR (Case 1 to 3) =	8437.2
K _s CORR (Case 4 to 7) =	1656834.4	K _t CORR (Case 4 to 7) =	8602.5
K _{s,i} NEW (Case 1 to 3) =	0.4997	K _{s,i} NEW (Case 4 to 7) =	0.4989
K _{s,i} CORR (Case 1 to 3) =	0.4384	K _{s,i} CORR (Case 4 to 7) =	0.4377
J NEW (Case 1 to 3) =	1.0000	J NEW (Case 4 to 7) =	1.0000
J CORR (Case 1 to 3) =	1.0000	J CORR (Case 4 to 7) =	1.0000

SHELL COEFFICIENTS

B _s NEW =	0.5303	B _s CORR =	0.5662
k _s NEW (Case 1 to 3) =	349478.4	k _s CORR (Case 1 to 3) =	249956.1
k _s NEW (Case 4 to 7) =	355753.3	k _s CORR (Case 4 to 7) =	254444.1
λ _s NEW (Case 1 to 3) =	27459031.1	λ _s CORR (Case 1 to 3) =	25044886.0
λ _s NEW (Case 4 to 7) =	27952063.1	λ _s CORR (Case 4 to 7) =	25494571.5
δ _s NEW (Case 1 to 3) =	0.00000781	δ _s CORR (Case 1 to 3) =	0.00000902
δ _s NEW (Case 4 to 7) =	0.00000767	δ _s CORR (Case 4 to 7) =	0.00000886

CHANNEL COEFFICIENTS

B _c NEW =	0.5303	B _c CORR =	0.5662
k _c NEW (Case 1 to 3) =	349478.4	k _c CORR (Case 1 to 3) =	249956.1
k _c NEW (Case 4 to 7) =	355753.3	k _c CORR (Case 4 to 7) =	254444.1
λ _c NEW (Case 1 to 3) =	27459031.1	λ _c CORR (Case 1 to 3) =	25044886.0
λ _c NEW (Case 4 to 7) =	27952063.1	λ _c CORR (Case 4 to 7) =	25494571.5
δ _c NEW (Case 1 to 3) =	0.00000781	δ _c CORR (Case 1 to 3) =	0.00000902
δ _c NEW (Case 4 to 7) =	0.00000767	δ _c CORR (Case 4 to 7) =	0.00000886

TUBELAYOUT GEOMETRY COEFFICIENTS

h/p NEW =	1.613	E*/E NEW (Case 1 to 3) =	0.3442	E*/E CORR (Case 1 to 3) =	0.3492
h/p CORR =	1.484	E*/E NEW (Case 4 to 7) =	0.3450	E*/E CORR (Case 4 to 7) =	0.3499
		v* NEW (Case 1 to 3) =	0.3207	v* CORR (Case 1 to 3) =	0.3167
		v* NEW (Case 4 to 7) =	0.3204	v* CORR (Case 4 to 7) =	0.3165
		X _a NEW (Case 1 to 3) =	3.0309	X _a CORR (Case 1 to 3) =	3.2171
		X _a NEW (Case 4 to 7) =	3.0332	X _a CORR (Case 4 to 7) =	3.2196
Z _d NEW (1-3) =	0.0538	Z _v NEW (1-3) =	0.1063	Z _m NEW (1-3) =	0.5058
Z _d NEW (4-7) =	0.0537	Z _v NEW (4-7) =	0.1062	Z _m NEW (4-7) =	0.5055
Z _d CORR (1-3) =	0.0456	Z _v CORR (1-3) =	0.0966	Z _m CORR (1-3) =	0.4765
Z _d CORR (4-7) =	0.0455	Z _v CORR (4-7) =	0.0965	Z _m CORR (4-7) =	0.4762
Z _w NEW (1-3) =	0.1063	Z _w CORR (1-3) =	0.0966		
Z _w NEW (4-7) =	0.1062	Z _w CORR (4-7) =	0.0965		

TUBESHEET GEOMETRY COEFFICIENTS

K =	1.0719	F NEW (Case 1 to 3) =	3.9023
		F NEW (Case 4 to 7) =	3.9084
Φ NEW (Case 1 to 3) =	5.1536	F CORR (Case 1 to 3) =	3.5414
Φ NEW (Case 4 to 7) =	5.1606	F CORR (Case 4 to 7) =	3.5469
Φ CORR (Case 1 to 3) =	4.6630		
Φ CORR (Case 4 to 7) =	4.6694		

**CALHEX INDUSTRIES LTD.**

5616 - 48TH. STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX5)
Fax: (403) 261 - 2761**TUBE-SHEET THICKNESS CALCULATION cont.'d**Job number: 12-0779
Revision number: 0 | Page number: 5 of 21**TUBESHEET LOADING FACTORS**

Q ₁ NEW (Case 1 to 3) =	-0.1443	Q _{Z1} NEW (Case 1 to 3) =	1.6232
Q ₁ NEW (Case 4 to 7) =	-0.1443	Q _{Z1} NEW (Case 4 to 7) =	1.6243
Q ₁ CORR (Case 1 to 3) =	-0.1297	Q _{Z1} CORR (Case 1 to 3) =	1.7695
Q ₁ CORR (Case 4 to 7) =	-0.1296	Q _{Z1} CORR (Case 4 to 7) =	1.7708
Q _{Z2} NEW (Case 1 to 3) =	1.40446	U _{NEW} (Case 1 to 3) =	2.80892
Q _{Z2} NEW (Case 4 to 7) =	1.40664	U _{NEW} (Case 4 to 7) =	2.81328
Q _{Z2} CORR (Case 1 to 3) =	1.86646	U _{CORR} (Case 1 to 3) =	3.73292
Q _{Z2} CORR (Case 4 to 7) =	1.86930	U _{CORR} (Case 4 to 7) =	3.73860

THERMAL EXPANSION LOADING FACTORS

Y _{NEW} (Case 1 to 3) =	0	Y _b =	0
Y _{NEW} (Case 4 to 7) =	-0.004095		
Y _{CORR} (Case 1 to 3) =	0		
Y _{CORR} (Case 4 to 7) =	-0.004096		
ω _s NEW (Case 1 to 3) =	2.71913	ω _c NEW (Case 1 to 3) =	2.71913
ω _s NEW (Case 4 to 7) =	2.71913	ω _c NEW (Case 4 to 7) =	2.71913
ω _s CORR (Case 1 to 3) =	2.39239	ω _c CORR (Case 1 to 3) =	2.39239
ω _s CORR (Case 4 to 7) =	2.39239	ω _c CORR (Case 4 to 7) =	2.39239
ω* _s NEW (Case 1 to 3) =	-2.67201	ω* _c NEW (Case 1 to 3) =	-2.67201
ω* _s NEW (Case 4 to 7) =	-2.67201	ω* _c NEW (Case 4 to 7) =	-2.67201
ω* _s CORR (Case 1 to 3) =	-2.32379	ω* _c CORR (Case 1 to 3) =	-2.32379
ω* _s CORR (Case 4 to 7) =	-2.32379	ω* _c CORR (Case 4 to 7) =	-2.32379

PRESSURE LOADING DUE TO THERMAL EXPANSION UHX-13.8 (for cyclical type service only)

P _s * NEW & CORR (Case 1 to 3) =	0	P _c * NEW & CORR (Case 1 to 3) =	0
P _s * NEW (Case 4 to 7) =	0.0	P _c * NEW (Case 4 to 7) =	0.0
P _s * CORR (Case 4 to 7) =	0.0	P _c * CORR (Case 4 to 7) =	0.0
T _s * =	84.825	T _c * =	82.475

PRESSURE LOADING ON TUBESHEET

P' _s NEW (Case 1 to 3) =	804.8	P' _s CORR (Case 1 to 3) =	867.5
P' _s NEW (Case 4 to 7) =	805.6	P' _s CORR (Case 4 to 7) =	868.4
P' _i NEW (Case 1 to 3) =	1190.8	P' _i CORR (Case 1 to 3) =	1306.9
P' _i NEW (Case 4 to 7) =	1192.1	P' _i CORR (Case 4 to 7) =	1308.4
P' _γ NEW (Case 1 to 3) =	0.0	P' _γ CORR (Case 1 to 3) =	0.0
P' _γ NEW (Case 4 to 7) =	-39.4	P' _γ CORR (Case 4 to 7) =	-39.4

P _w NEW (Case 1 to 3) =	0	P _w CORR (Case 1 to 3) =	0
P _w NEW (Case 4 to 7) =	0	P _w CORR (Case 4 to 7) =	0

TUBE BUCKLING FACTORS

Tubesheet to Baffle span, l _t :	30.85		<u>NEW</u>	<u>CORR</u>
Tubesheet to Baffle span, l _t :	30.9	F _t =	129.8188	130.0292
Baffle to Baffle span, l _t :	32	F _t =	134.6581	134.6581
r _t =	0.2376	F _t (max) =	134.6581	134.6581
Tube Yield stress, S _{y,t} =	26000	C ₁ =	146.7	146.7



CALHEX INDUSTRIES LTD.

1615 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 281 - 2781

TUBE-SHEET THICKNESS CALCULATION cont.'d

Job number: 12-0779
Revision number: 0 | Page number: 6 of 2/

SUMMARY OF LOADS, CO-EFFICIENTS, & STRESSES FOR NEW TUBESHEET

Case	P_s	P_t	$\gamma \cdot$	P_{Sx}	P_{Cy}	P'_s
1	0	415.0	0	0.0	0.0	0
2	415.0	0.00	0	0.0	0.0	804.8
3	415.0	415.0	0	0.0	0.0	804.8
4	0	0	-0.0041	0.0	0.0	0.0
5	0	415.0	-0.0041	0.0	0.0	0.0
6	415.0	0	-0.0041	0.0	0.0	805.6
7	415.0	415.0	-0.0041	0.0	0.0	805.6

Case	P'_t	P_y	P_w	P_w	P_{rim}	P_e
1	1190.8	0	0.0	0.0	-24.9	-331.9
2	0.0	0	0.0	0.0	24.9	226.5
3	1190.8	0	0.0	0.0	0.0	-105.4
4	0	-39.4	0.0	0.0	0.0	-10.7
5	1192.1	-39.4	0.0	0.0	-24.9	-342.6
6	0.0	-39.4	0.0	0.0	24.9	215.7
7	1192.1	-39.4	0.0	0.0	0.0	-116.2

Case	Q_2	Q_3	F_m	$ \sigma $	$\sigma_{allowable}$
1	307.4	-0.1591	0.0795	24157.5	30000
2	-307.4	-0.1660	0.0830	17199.4	30000
3	0.0	-0.1443	0.0722	6958.2	30000
4	0.0	-0.1443	0.0721	707.5	70932
5	307.3	-0.1586	0.0793	24816.7	70932
6	-307.3	-0.1670	0.0835	16455.0	70932
7	0.0	-0.1443	0.0721	7654.2	70932

Case	$ \tau $	$\tau_{allowable}$	F_{tmin}	F_{tmax}
1	5265.8	16000	0.2224	1.5569
2	3593.7	16000	0.2457	1.5261
3	1672.1	16000	0.1724	1.6232
4	170.4	16000	0.1711	1.6243
5	5435.8	16000	0.2195	1.5600
6	3422.6	16000	0.2480	1.5222
7	1842.9	16000	0.1711	1.6243

Case	$\sigma_{t,1}$	$\sigma_{t,2}$	$\sigma_{t, allowable}$	F_s	S_{tb}
1	-1116.2567	1162.7608	13400	2.00	...
2	794.7648	-697.5403	13400	1.25	11250.8
3	-321.4919	465.2205	13400	2.00	...
4	9.4520	89.7375	26800	1.25	...
5	-1109.0706	1254.0275	26800	2.00	...
6	805.7756	-608.5018	26800	1.25	11250.8
7	-312.7471	555.7882	26800	2.00	...

Wt = 218.1

**CALHEX INDUSTRIES LTD.**

9016 - 46TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761**TUBE-SHEET THICKNESS CALCULATION cont.'d**Job number: 12-0779
Revision number: 0 | Page number: 7 of 27

Case	$\sigma_{s,m}$	$\sigma_{s,b}$	σ_s	$\sigma_{c,m}$	$\sigma_{c,b}$	σ_c
1	867.8	-20768.5	21636.3	4573.6	34723.5	39297.1
2	2605.1	25019.0	27624.0	0.0	-11990.1	11990.1
3	3472.9	4250.5	7723.4	4573.6	22733.4	27307.0
4	-112.1	-787.4	899.5	0.0	847.2	847.2
5	755.9	-21550.8	22306.7	4573.6	35565.5	40139.2
6	2492.4	24225.0	26717.5	0.0	-11136.1	11136.1
7	3360.5	3461.6	6822.0	4573.6	23582.3	28155.9

Case	σ_s , Allowable		σ_c , Allowable			
1	25650.0		25650.0	*		
2	25650.0	*	25650.0			
3	25650.0		25650.0	*		
4	65384.0		65544.0			
5	65384.0		65544.0			
6	65384.0		65544.0			
7	65384.0		65544.0			

Elastic-Plastic calculation at shell to tubesheet junction requires check

Elastic-Plastic calculation at channel to tubesheet junction requires check

ELASTIC - PLASTIC CALCULATION FOR TUBESHEET TO SHELL & / OR CHANNEL (UHX-13.7 if required)

	<u>Shell to Tubesheet</u>			<u>Channel to Tubesheet</u>		
Case:	1	2	3	1	2	3
$S_{s/c}^*$	-	25650.0	-	25650.0	-	25650.0
$Fact_{s/c}$	-	1.0000	-	0.858503235	-	1
$k_{s,c}$	-	-	-	300028.3	-	-
$\lambda_{s,c}$	-	-	-	23573667.0	-	-
F	-	-	-	3.6359	-	-
Φ	-	-	-	4.8018	-	-
Q_1	-	-	-	-0.1409	-	-
Q_{Z1}	-	-	-	1.6385	-	-
Q_{Z2}	-	-	-	1.47735	-	-
U	-	-	-	2.95470	-	-
P_w	-	-	-	0	-	-
P_w	-	-	-	0	-	-
P_{rim}	-	-	-	-26.1	-	-
P_e	-	-	-	-330.7	-	-
Q_2	-	-	-	323.4	-	-
Q_3	-	-	-	-0.1565	-	-
F_m	-	-	-	0.078249238	-	-
$ \sigma $	-	-	-	23677.4	-	-
$ \sigma $ all	-	-	-	30000	-	-

Channel to Tubesheet stress is Okay

**CALHEX INDUSTRIES LTD.**

9516 - 48TH. STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761**TUBE-SHEET THICKNESS CALCULATION cont.'d**Job number: 12-0779
Revision number: 0 | Page number: 8 of Z/**SUMMARY OF LOADS, CO-EFFICIENTS, & STRESSES FOR CORRODED TUBESHEET**

Case	P_s	P_t	γ	P_{S*}	P_{C*}	P'_s
1	0	415.0	0	0.0	0.0	0
2	415.0	0	0	0.0	0.0	867.5
3	415.0	415.0	0	0.0	0.0	867.5
4	0	0	-0.0041	0.0	0.0	0.0
5	0	415.0	-0.0041	0.0	0.0	0.0
6	415.0	0	-0.0041	0.0	0.0	868.4
7	415.0	415.0	-0.0041	0.0	0.0	868.4
Case	P'_t	P_γ	P_w	P_w	P_{rim}	P_e
1	1306.9	0	0.0	0.0	-28.7	-324.8
2	0	0	0.0	0.0	28.7	218.0
3	1306.9	0	0.0	0.0	0.0	-106.9
4	0	-39.4	0.0	0.0	0.0	-9.6
5	1308.4	-39.4	0.0	0.0	-28.8	-334.4
6	0	-39.4	0.0	0.0	28.8	208.4
7	1308.4	-39.4	0.0	0.0	0.0	-116.5
Case	Q_2	Q_3	F_m	$ \sigma $	$\sigma_{allowable}$	
1	299.3	-0.1444	0.0722	25351.2	30000	
2	-299.3	-0.1516	0.0758	17860.9	30000	
3	0.0	-0.1297	0.0648	7490.3	30000	
4	0.0	-0.1296	0.0648	669.1	70932	
5	299.2	-0.1439	0.0720	25968.7	70932	
6	-299.2	-0.1526	0.0763	17153.0	70932	
7	0.0	-0.1296	0.0648	8146.6	70932	
Case	$ \tau $	$\tau_{allowable}$		F_{tmin}	F_{tmax}	
1	5601.8	16000		0.2813	1.4072	
2	3759.0	16000		0.3175	1.3556	
3	1842.8	16000		0.2073	1.5124	
4	164.9	16000		0.0254	1.7708	
5	5766.4	16000		0.0773	1.6967	
6	3593.3	16000		0.1088	1.6519	
7	2008.2	16000		0.0254	1.7708	
Case	$\sigma_{t,1}$	$\sigma_{t,2}$	$\sigma_{t,0 allowable}$		F_s	S_{tb}
1	-1025.9799	855.8073	13400		2.00	...
2	724.9756	-439.2467	13400		1.25	11250.8
3	-301.0043	416.5606	13400		2.00	...
4	1.2489	87.1401	26800		2.00	...
5	-1363.0283	1423.1054	26800		2.00	...
6	964.4835	-689.9777	26800		1.25	11250.8
7	-399.7937	645.9876	26800		2.00	...
Wt =		247.5				

**CALHEX INDUSTRIES LTD.**

9816 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761**TUBE-SHEET THICKNESS CALCULATION cont.'d**Job number: 12-0779
Revision number: 0 Page number: 9 of 21

Case	$\sigma_{s,m}$	$\sigma_{s,b}$	σ_s	$\sigma_{c,m}$	$\sigma_{c,b}$	σ_c
1	1076.2	-25870.4	26946.6	5284.0	41907.9	47191.9
2	2932.3	29925.0	32857.3	0.0	-14879.9	14879.9
3	4008.5	4054.6	8063.0	5284.0	27028.0	32312.0
4	-114.2	-871.1	985.3	0.0	932.1	932.1
5	962.2	-26735.2	27697.4	5284.0	42833.6	48117.6
6	2817.6	29046.0	31863.7	0.0	-13939.6	13939.6
7	3894.0	3181.9	7075.9	5284.0	27961.9	33245.9

Case	σ_s , Allowable		σ_c , Allowable			
1	25650.0	*	25650.0	*		0
2	25650.0	*	25650.0			0
3	25650.0		25650.0	*		0
4	65384.0		65544.0			0
5	65384.0		65544.0			0
6	65384.0		65544.0			0
7	65384.0		65544.0			0

Elastic-Plastic calculation at shell to tubesheet junction requires check

Elastic-Plastic calculation at channel to tubesheet junction requires check

ELASTIC - PLASTIC CALCULATION FOR TUBESHEET TO SHELL & / OR CHANNEL (UHX-13.7 if required)

Case:	Shell to Tubesheet			Channel to Tubesheet		
	1	2	3	1	2	3
$S_{s/c}^*$	25650.0	25650.0	-	25650.0	-	25650.0
$Fact_{s/c}$	0.996562304	0.9333	-	0.746465934	-	0.978510805
$k_{s,c}$	249096.8	233292.3	-	186583.7	-	244584.7
$\lambda_{s,c}$	24958789.3	23375221.2	-	18695154.2	-	24506691.5
F	3.5356	3.4279	-	3.1097	-	3.5049
ϕ	4.6553	4.5135	-	4.0945	-	4.6278
Q_1	-0.1296	-0.1280	-	-0.1230	-	-0.1293
Q_{Z1}	1.7699	1.7781	-	1.8042	-	1.7715
Q_{Z2}	1.86859	1.90865	-	2.03777	-	1.87621
U	3.73718	3.81730	-	4.07554	-	3.75242
P_w	0	0	-	0	-	0
P_w	0	0	-	0	-	0
P_{rim}	-28.8	29.4	-	-31.4	-	0.0
P_e	-324.8	217.6	-	-322.3	-	-106.8
Q_2	299.7	-306.1	-	326.8	-	0.0
Q_3	-0.1443	-0.1505	-	-0.1391	-	-0.1293
F_m	0.072158408	0.075235219	-	0.06957245	-	0.064648099
$ \sigma $	25337.3	17699.0	-	24241.9	-	7464.1
$ \sigma $ all	30000	30000	-	30000	-	30000

**CALHEX INDUSTRIES LTD.**

9415 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761**TUBESHEET WELD SIZING**

Job number: 12-0779

Revision number: 0

Page number: 10 of 27

CODES:

ASME SEC. VIII, DIV. 1 2010 ED. 2011ADD.:

FIG. UW-13.2 (d)

	<u>Tube Side</u>	<u>Shell Side</u>
Channel and Shell Outside Diameters:	24	24
Channel and Shell Thicknesses:	0.5	0.5
Tube Sheet Facing Thickness:	0.1875	0.1875
Facing Outside Diameters:	22.9375	22.9375
Channel & Shell ID's - Facing OD's:	0.0625	0.0625
Corrosion Allowances:	0.0625	0.0625
Is the tubesheet Supported or Unsupported :	S	
Tube Sheet weld groove angle (°) :		30

CALCULATIONS

	<u>Tube Side</u>	<u>Shell Side</u>
Actual corroded thicknesses, t :	0.4375	0.4375
Facing Edge to Channel & Shell OD, a :	0.53125	0.53125
Minimum dimension b for supported Tubesheet [2t _s -a]:	0.34375	0.34375
Minimum dimension b for unsupported Tubesheet [3t _s -a]:	0.78125	0.78125
Flat Land dimension of groove weld (1/16" of RF in Shell):	0.1250	0.1250
Minimum TS Groove angle, supported Tubesheet (°):	22.4	22.4
Minimum TS Groove angle, unsupported Tubesheet (°):	51.009	51.00901
Actual b dimension :	0.4317	0.4317
Minimum T _p dimension :	0.25	0.25

ACTUAL MINIMUM TUBESHEET THICKNESS

$$T = 0.4317 + 0.4317 + 0.25 = \underline{1.1134}$$

ACTUAL MINIMUM TUBESHEET THICKNESS INCLUDING CORROSION ALLOWANCE

$$T_c = 1.1134 + 0.125 = \underline{1.2384}$$



CALHEX INDUSTRIES LTD.

9515 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761

SHELL ALLOWABLE COMPRESSIVE STRESS

Job number: 12-0779
Revision number: 0 Page number: 11 of 2/

CODES:

ASME SEC. VIII, DIV. 1 2010 ED., per UG-23 (b)

Shell

Material :	SA-333-6	S or W:	S	Allow. Amb. Stress:	17100	psi
Pipe~ 1 / Plate~ 2 :		1		Allow. Design Stress:	17100	psi
Shell OD :	24		in	Corrosion Allowance :	0.0625	in
Design Pressure :	400		psi	Design Temperature :	163	°F

CALCULATIONS

New uncorroded thickness : 0.5 in
Thickness reduced for pipe tolerance of 12.5%
Minimum thickness, t : 0.3750 in
Outside radius, Ro : 12 in

EXTERNAL PRESSURE CHART # : CS-2

$$\text{Factor A} = \frac{0.125}{(Ro / t)} = 0.0039063$$

Maximum Shell Compressive Stress, B ($S_{B,S}$) = 16744 psi

**CALHEX INDUSTRIES LTD.**

9815 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225-4395 (CALHEX)
Fax: (403) 261-2761

NOZZLE REINFORCEMENT IN SHELL CALC. VERSION 3.0, JAN 08, 2007, (Dec. 21, 2002)

NOZZLE REINFORCEMENT CALCULATION

Job number: 12-0779

Revision number: 0

Page number: 12 of 21

CODES:

ASME SEC. VIII, DIV. I, 2010 ED., 2011 ADD.

UG-36,37,40,41,45 ; UW-15,16; Appedix 1-7

DIMENSIONS & PROPERTIES

<u>Operating Conditions</u>			<u>Shell</u>	<u>Nozzle</u>
Design Pressure :	400	Material :	SA-333-6	SA-106-B
Design Temperature :	163	Seamless or Welded :	S	S
Corrosion Allowance :	0.0625	Ambient Allowable Stress :	17100	17100
Nozzle nom. Size :	8	Operating Allowable Stress :	17100	17100
Nozzle Rating :	300 #	Pipe or Plate :	PI	PI
Shell or Tube side :	s	Efficiency, E :	1.000	1.000
<u>Repad</u>		Outside Diameter :	24.0000	8.625
Material :	sa-516-70n	Thickness :	0.500	0.500
Ambient Allow. Stress :	20000	Radial Reinforcement Limit, D [*] :	0.0000	-
Operating Allow. Stress :	20000	Hillside Offset, L :	-	0.0000
Outside Diameter :	12.6250	Inward Nozz. Projection :	-	0.0000
Thickness :	0.2500	Nozz. Fillet Weld size, L ₁ / L ₃ :	0.3750	0.0000
Weld size, L ₂ :	0.2500			
Is the Nozzle Saddled on (Y or N):		N		

CALCULATIONS (corroded condition)

t _r :	0.27580	f _{r1} :	1.000	Parall. :	15.5000		
t :	0.37500	f _{r2} :	1.000	Norm. :	0.9375	<u>Min. Weld leg sizes</u>	<u>Per</u>
t _m :	0.09193	f _{r3} :	1.000	D _p :	12.6250	L ₁ :	0.3571 UW-16
t _n :	0.43750	f _{r4} :	1.000		12.6250	L ₂ :	0.1786 UW-16
t _e :	0.25000	F :	1.000	d :	7.7500	L ₃ :	0.3571 UW-16
t _i :	0.00000		0.500	d [*] :	7.7500	<u>Minimum Nozz. thickness (UG-45)</u>	
				d (circ.) :	7.7500	t _n min =	0.3383

$$\text{AREA REQUIRED, } A = d t_r F + 2 t_n t_r F (1 - f_{r1}) =$$

Area Available in Shell, A₁ (use larger value of) :

$$d^* (E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) = 0.7688$$

$$2 (t + t_n) (E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) = 0.1612$$

Area Available in Nozzle Outward, A₂ (use smaller value of) :

$$5^* (t_n - t_m) f_{r2} t = 0.6479$$

$$\text{<no-repad>} \quad 5^* (t_n - t_m) f_{r2} t_n = 0.7559$$

$$\text{<with repad>} \quad 2^* (t_n - t_m) (2.5 t_n + t_e) f_{r2} = 0.9287$$

Area Available in Nozzle Inward, A₃ (use smaller value of) :

$$5 t t_r f_{r2} = 0 \quad 5 t t_r f_{r2} = 0$$

$$5 h t_r f_{r2} = 0$$

$$\text{Area Available in outward nozzle weld, } A_{41} =$$

$$\text{Area Available in repad weld, } A_{42} =$$

$$\text{Area Available in inward nozzle weld, } A_{43} =$$

$$\text{Area Available in repad, } A_5 = (D_p - d - 2 t_n) t_e f_{r4} =$$

$$\text{TOTAL AVAILABLE AREA} =$$

Opening is adequately reinforced by :

Longitudinal Rein

$$2.1375$$

$$0.7688$$

$$0.6479$$

$$0.0000$$

$$0.1406$$

$$0.0625$$

$$0.0000$$

$$1.0000$$

$$2.6199$$

$$0.4824$$

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NOZZLE REINFORCEMENT IN SHELL CALC. VERSION 3.0, JAN 08, 2007, (Dec. 21, 2002)

NOZZLE REINFORCEMENT CALCULATIONJob number: 12-0779
Revision number: 0 Page number: 13 of 21**CODES:**

ASME SEC. VIII, DIV. I, 2010 ED., 2011 ADD.

UG-36,37,40,41,45 ; UW-15,16; Appedix 1-7

DIMENSIONS & PROPERTIES

<u>Operating Conditions</u>			<u>Shell</u>	<u>Nozzle</u>
Design Pressure :	400	Material :	SA-333-6	SA-106-B
Design Temperature :	158	Seamless or Welded :	S	S
Corrosion Allowance :	0.0625	Ambient Allowable Stress :	17100	17100
Nozzle nom. Size :	8	Operating Allowable Stress :	17100	17100
Nozzle Rating :	300 #	Pipe or Plate :	PI	PI
Shell or Tube side :	T	Efficiency, E :	1.000	1.000
<u>Repad</u>		Outside Diameter :	24.0000	8.625
Material :	sa-516-70n	Thickness :	0.500	0.500
Ambient Allow. Stress :	20000	Radial Reinforcement Limit, D' :	0.0000	-
Operating Allow. Stress :	20000	Hillside Offset, L :	-	0.0000
Outside Diameter :	12.6250	Inward Nozz. Projection :	-	0.0000
Thickness :	0.2500	Nozz. Fillet Weld size, L ₁ / L ₃ :	0.3750	0.0000
Weld size, L ₂ :	0.2500			
Is the Nozzle Saddled on (Y or N):		N		

CALCULATIONS (corroded condition)

t _r :	0.27580	f _{r1} :	1.000	Parall. :	15.5000		
t :	0.37500	f _{r2} :	1.000	Norm. :	0.9375	<u>Min. Weld leg sizes</u>	<u>Per</u>
t _m :	0.09193	f _{r3} :	1.000	D _p :	12.6250	L ₁ :	0.3571 UW-16
t _n :	0.43750	f _{r4} :	1.000		12.6250	L ₂ :	0.1786 UW-16
t _o :	0.25000	F :	1.000	d :	7.7500	L ₃ :	0.3571 UW-16
t _i :	0.00000		0.500	d' :	7.7500	<u>Minimum Nozz. thickness (UG-45)</u>	
				d (circ.) :	7.7500	t _n min =	0.3383

$$\text{AREA REQUIRED, } A = d t F + 2 t_n t_r F (1 - f_{r1}) =$$

$$2.1375$$

Area Available in Shell, A₁ (use larger value of) :Long.

$$d^* (E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) = 0.7688$$

$$2 (t + t_n) (E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) = 0.1612$$

$$0.7688$$

Area Available in Nozzle Outward, A₂ (use smaller value of) :

$$5^* (t_n - t_m) f_{r2} t = 0.6479$$

$$<\text{no-repad}> 5^* (t_n - t_m) f_{r2} t_n = 0.7559$$

$$<\text{with repad}> 2^* (t_n - t_m) (2.5 t_n + t_o) f_{r2} = 0.9287$$

$$0.6479$$

Area Available in Nozzle Inward, A₃ (use smaller value of) :

$$5 t t_{f_{r2}} = 0 \quad 5 t t_{f_{r2}} = 0$$

$$5 h t_{f_{r2}} = 0$$

$$0.0000$$

$$\text{Area Available in outward nozzle weld, } A_{41} =$$

$$0.1406$$

$$\text{Area Available in repad weld, } A_{42} =$$

$$0.0625$$

$$\text{Area Available in inward nozzle weld, } A_{43} =$$

$$0.0000$$

$$\text{Area Available in repad, } A_5 = (D_p - d - 2 t_n) t_o f_{r4} =$$

$$1.0000$$

$$\text{TOTAL AVAILABLE AREA} =$$

$$2.6199$$

Opening is adequately reinforced by :

$$0.4824$$

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8515 - 46TH STREET S.E., CALGARY, ALBERTA, T2C 2R1

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EXTERNAL PRESSURE ON CYLINDER STRESS CALCULATION

Job number: 12-0779

Revision number: 0

Page number: 14 of 21

CODES:

ASME SEC. VIII, DIV. 1 2010 ED., 2011ADD. per UG-23 (b)

SHELL-CHANNEL-NOZZLE CYLINDER

Material :	SA-333-6	S or W:	S	Allow. Ambient Stress:	17100	psi
Pipe~ 1 / Plate~ 2 :		1		Allow. Design Stress:	17100	psi
Description:	SHELL			Corrosion Allowance :	0.0625	in
External Design Press. :	15	psi		Design Temperature :	163	°F
Cylinder OD, Do:	24	in				
Cylinder thickness:	0.5	in				
Cylinder Length:	572.75	in				

CALCULATIONS

Do / t: 64.0000

L / Do: 23.8646

EXTERNAL PRESSURE CHART #: CS-2

Shell Compressive Stress Factor, B = 4060

Maximum Allowable External Pressure, Pa: 84.58 PSI

Minimum thickness at 15 PSI = 0.2413 in
(Excluding C/A)

**CALHEX INDUSTRIES LTD.**

5515 - 45TH. STREET S.E., CALGARY, ALBERTA, T2C 2R1

Bus: (403) 225 - 4395 (CALHEX)
Fax: (403) 261 - 2761**EXTERNAL PRESSURE ON CYLINDER STRESS CALCULATION**Job number: 12-0799
Revision number: 0 | Page number: 15 of 21**CODES:**

ASME SEC. VIII, DIV. 1 2010 ED., 2011ADD. per UG-23 (b)

SHELL-CHANNEL-NOZZLE CYLINDER

Material :	SA-333-6	S or W:	S	Allow. Ambient Stress:	17100	psi
Pipe~ 1 / Plate~ 2 :			1	Allow. Design Stress:	17100	psi
Description:	CHANNEL			Corrosion Allowance :	0.0625	in
External Design Press. :	15	psi		Design Temperature :	158	°F
Cylinder OD, Do:	24	in				
Cylinder thickness:	0.5	in				
Cylinder Length:	17	in				

CALCULATIONS

Do / t :	64.0000	EXTERNAL PRESSURE CHART # :	CS-2
L / Do :	0.7083		

Shell Compressive Stress Factor, B = 16815

Maximum Allowable External Pressure, Pa: 350.31 PSI

Minimum thickness at 15 PSI = 0.0750 in
(Excluding C/A)

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EXTERNAL PRESSURE ON CYLINDER STRESS CALCULATION

Job number: 12-0799

Revision number: 0

Page number: 16 of 21

CODES:

ASME SEC. VIII, DIV. 1 2010 ED., 2011ADD. per UG-23 (b)

SHELL-CHANNEL-NOZZLE CYLINDER

Material :	SA-333-6	S or W:	S	Allow. Ambient Stress:	17100	psi
Pipe~ 1 / Plate~ 2 :			1	Allow. Design Stress:	17100	psi
Description:	8" NOZZLE SHELL			Corrosion Allowance :	0.0625	in
External Design Press. :	15	psi		Design Temperature :	163	°F
Cylinder OD, Do:	8.625	in				
Cylinder thickness:	0.5	in				
Cylinder Length:	12	in				

CALCULATIONS

Do / t : 23.0000

EXTERNAL PRESSURE CHART # : CS-2

L / Do : 1.3913

Shell Compressive Stress Factor, B = 17288

Maximum Allowable External Pressure, Pa: 1002.20 PSI

Minimum thickness at 15 PSI = 0.0346 in
(Excluding C/A)

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EXTERNAL PRESSURE ON CYLINDER STRESS CALCULATION

Job number: 12-0799

Revision number: 0

Page number: 17 of 21

CODES:

ASME SEC. VIII, DIV. 1 2010 ED., 2011ADD. per UG-23 (b)

SHELL-CHANNEL-NOZZLE CYLINDER

Material :	SA-333-6	S or W:	S	Allow. Ambient Stress:	17100	psi
Pipe~ 1 / Plate~ 2 :			1	Allow. Design Stress:	17100	psi
Description:	8" NOZZLE channel			Corrosion Allowance :	0.0625	in
External Design Press. :	15	psi		Design Temperature :	158	°F
Cylinder OD, Do:	8.625	in				
Cylinder thickness:	0.5	in				
Cylinder Length:	12	in				

CALCULATIONS

Do / t: 23.0000

L / Do: 1.3913

EXTERNAL PRESSURE CHART #: CS-2

Shell Compressive Stress Factor, B = 17288

Maximum Allowable External Pressure, Pa: 1002.20 PSI

Minimum thickness at 15 PSI = 0.0306 in
(Excluding C/A)

**CALHEX INDUSTRIES LTD.**

9516 - 48TH STREET S.E., CALGARY, ALBERTA, T2C 3P1

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EXT PRESS NOZZLE REINFORCEMENT IN SHELL CALC. VERSION 1.1, Jan 06,2006 (Sept.30, 2002)

EXTERNAL PRESSURE NOZZLE REINFORCEMENT CALCULATIONJob number: 12-0799
Revision number: 0 | Page number: 18 of 21**CODES:**

ASME SEC. VIII, DIV. I, 2010ed., 2011ADD.

UG-28,36,37,40,41,45 ; UW-15,16

DIMENSIONS & PROPERTIES

Operating Conditions		Shell		Nozzle	
Design Pressure :	15	Material :	SA-333-6		SA-333-6
Design Temperature :	163	Seamless or Welded :	S		S
Corrosion Allowance :	0.0625	Ambient Allowable Stress :	17100		17100
Nozzle nom. Size :	8	Operating Allowable Stress :	17100		17100
Nozzle Rating :	300 #	Pipe or Plate :	PI		PI
Shell or Tube side :	S	Efficiency, E :	1.000		1.000
Repad		Outside Diameter :	24.0000		8.625
Material :	SA-516-70N	Thickness :	0.500		0.500
Ambient Allow. Stress :	20000	Radial Reinforcement Limit, d' :	0.0000		-
Operating Allow. Stress :	20000	Hillside Offset, L :	-		0.0000
Outside Diameter :	12.6250	Inward Nozz. Projection :	-		0.0000
Thickness :	0.2500	Nozz. Fillet Weld size, L ₁ / L ₃ :	0.3750		0.0000
Weld size, L ₂ :	0.2500				
Is the Nozzle Saddled on (Y or N):					

CALCULATIONS (corroded condition)

t _r :	0.24130	f _{r1} :	1.000	Parall. :	15.5000		
t :	0.37500	f _{r2} :	1.000	Norm. :	0.9375		
t _m :	0.03460	f _{r3} :	1.000	D _p :	12.6250		
t _n :	0.43750	f _{r4} :	1.000		12.6250		
t _e :	0.25000	F :	1.000	d :	7.7500		
t _i :	0.00000		0.500	d' :	7.7500		
				d (circ.) :	7.7500		
						Min. Weld leg sizes	
						L ₁ :	0.3571
						L ₂ :	0.1786
						L ₃ :	0.3571
						Minimum Nozz. thickness (UG-45)	
						t _n min =	0.3038
						Longitudinal Rein	
						0.9350	
AREA REQUIRED, A = 0.5 * (d * F + 2 * t_n * F * (1 - f_{r4})) =							
Area Available in Shell, A₁ (use larger value of) :						Long.	
d * (E ₁ t - F t _r) - 2 t _n (E ₁ t - F t _r) (1 - f _{r1}) =						1.0362	
2 (t + t _n) (E ₁ t - F t _r) - 2 t _n (E ₁ t - F t _r) (1 - f _{r1}) =						0.2173	
Area Available in Nozzle Outward, A₂ (use smaller value of) :							
5 * (t _n - t _m) f _{r2} t =						0.7554	
<no-repad> 5 * (t _n - t _m) f _{r2} t _n =						0.8813	
<with repad> 2 * (t _n - t _m) (2.5 t _n + t _e) f _{r2} =						1.0828	
Area Available in Nozzle Inward, A₃ (use smaller value of) :							
5 t t _i f _{r2} =						0	
5 t t _i f _{r2} =						0	
5 h t _i f _{r2} =						0	
Area Available in outward nozzle weld, A ₄₁ =						0.1406	
Area Available in repad weld, A ₄₂ =						0.0625	
Area Available in inward nozzle weld, A ₄₃ =						0.0000	
Area Available in repad, A ₅ = (D _p - d - 2 t _n) t _e f _{r4} =						1.0000	
TOTAL AVAILABLE AREA =						2.9947	
Opening is adequately reinforced by :						2.0597	

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EXT PRESS NOZZLE REINFORCEMENT IN SHELL CALC. VERSION 1.1, Jan 06,2006 (Sept.30, 2002)

EXTERNAL PRESSURE NOZZLE REINFORCEMENT CALCULATION

Job number: 12-0799

Revision number: 0

Page number: 19 of 21

CODES:

ASME SEC. VIII, DIV. I, 2010ed., 2011ADD.

UG-28,36,37,40,41,45 ; UW-15,16

DIMENSIONS & PROPERTIES

<u>Operating Conditions</u>		<u>Shell</u>		<u>Nozzle</u>
Design Pressure :	15	Material :	SA-333-6	SA-333-6
Design Temperature :	158	Seamless or Welded :	S	S
Corrosion Allowance :	0.0625	Ambient Allowable Stress :	17100	17100
Nozzle nom. Size :	8	Operating Allowable Stress :	17100	17100
Nozzle Rating :	300 #	Pipe or Plate :	PI	PI
Shell or Tube side :	T	Efficiency, E :	1.000	1.000
<u>Repad</u>		Outside Diameter :	24.0000	8.625
Material :	SA-516-70N	Thickness :	0.500	0.500
Ambient Allow. Stress :	20000	Radial Reinforcement Limit, d' :	0.0000	-
Operating Allow. Stress :	20000	Hillside Offset, L :	-	0.0000
Outside Diameter :	12.6250	Inward Nozz. Projection :	-	0.0000
Thickness :	0.2500	Nozz. Fillet Weld size, L ₁ / L ₃ :	0.5000	0.0000
Weld size, L ₂ :	0.2500			
Is the Nozzle Saddled on (Y or N):				
N				

CALCULATIONS (corroded condition)

t _r :	0.07500	f _{r1} :	1.000	Parall. :	15.5000		
t :	0.37500	f _{r2} :	1.000	Norm. :	0.9375	<u>Min. Weld leg sizes</u>	<u>Per</u>
t _m :	0.03460	f _{r3} :	1.000	D _p :	12.6250	L ₁ :	0.3571 UW-16
t _n :	0.43750	f _{r4} :	1.000		12.6250	L ₂ :	0.1786 UW-16
t _e :	0.25000	F :	1.000	d :	7.7500	L ₃ :	0.3571 UW-16
t _i :	0.00000		0.500	d' :	7.7500	<u>Minimum Nozz. thickness (UG-45)</u>	
				d (circ.) :	7.7500	t _n min =	0.1375
						<u>Longitudinal Rein</u>	
AREA REQUIRED, A = 0.5*(d t F + 2 t _n t F(1-f _{r1})) =						0.2906	
Area Available in Shell, A ₁ (use larger value of) :						<u>Long.</u>	
d*(E ₁ t - F t _r) - 2 t _n (E ₁ t - F t _r)(1-f _{r1}) =						2.3250	
2(t + t _n)(E ₁ t - F t _r) - 2 t _n (E ₁ t - F t _r)(1-f _{r1}) =						0.4875	
Area Available in Nozzle Outward, A ₂ (use smaller value of) :						2.3250	
5*(t _n - t _m) f _{r2} t =						0.7554	
<no-repad> 5*(t _n - t _m) f _{r2} t _n =						0.8813	
<with repad> 2*(t _n - t _m)(2.5 t _n + t _e) f _{r2} =						1.0828	
Area Available in Nozzle Inward, A ₃ (use smaller value of) :						0.7554	
5 t t _i f _{r2} =						0	
5 t t _i f _{r2} =						0	
5 h t _i f _{r2} =						0.0000	
Area Available in outward nozzle weld, A ₄₁ =						0.2500	
Area Available in repad weld, A ₄₂ =						0.0625	
Area Available in inward nozzle weld, A ₄₃ =						0.0000	
Area Available in repad, A ₅ = (D _p - d - 2 t _n) t _e f _{r4} =						1.0000	
TOTAL AVAILABLE AREA =						4.3929	
Opening is adequately reinforced by :						4.1023	

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LIFTING LUG CALCULATION VERSION 2.0 May 27, 2008

LIFTING LUG CALCULATION

Job number: 12-0799
Revision number: 0 Page number: 20 of 21

CODES:

ASME SEC. VIII, DIV. I, 2010 ed., 2011ADD.: UG-22
TEMA Ninth Edition, 2007: RGP-G-7.24
Pressure Vessel Design Manual: Pg. 171 - 189

LIFTING-LUG GEOMETRY

Lug Material SA-516-70N
Allowable Stress 20000 psi

Design Load 19125 lbs/lug
Shackle Pin 1.625 in
Actual Hole 1.75 in
Lug Base Length 10 in
Lug Thickness 1.5 in
Fillet Weld Leg 0.5 in
Insulation Thk. 2 in
Lug Height 7 in
Pin offset 4.5 in

SHELL GEOMETRY:

Shell Material SA-333-6
Allowable Stress 17100 psi

Shell Type 0 Pipe
Shell Thickness 0.5 in
Corrosion 0.0625 in
Inside Diameter 23 in
Repad Thickness 0.375 in
Mill Tolerance 0.875
Effective Shell Thickness 0.5557 in

Shackle clearance 0.43 in

Maximum Load / Lug:

Vertical Load = 19125 lb
Longitudinal Load = 14312 lb
Cross Load = 4130 lb

Shell Stress:**Shell Actual Stresses:****Code Allowable Stresses:**

Radial stress = 13995 psi 17100 psi (Sa)
Longitudinal stress = 9348 psi 25650 psi combined (1.5 x Sa)

Lifting Details:

Minimum Sling or Chain Rating: 24000 lbs (12.0 ton)

Maximum Off Vertical Angle for L 36.8 deg (for each lifting-lug)

NOTE: If this angle is less than 30 degree, two crane or a spreader bar shall be used for the lift.

**CALHEX INDUSTRIES LTD.**

6615 - 48TH. STREET S.E., CALGARY, ALBERTA, T2C 3R1

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HORIZONTAL SUPPORT SADDLE CALCULATION VERSION 3.0, JAN. 03, 2005 (JAN. 08, 2002)

HORIZONTAL SUPPORT SADDLE STRESSES

Job number: 12-0779

Revision number:

Page number: 2 / of 2 /

CODES:

Recommended Good practice : L.P. Zick analysis- Pressure Vessel Handbook latest

DIMENSIONS & PROPERTIES

Tema type unit (ie. NEN):	NEN	Length between shell seams, (L):	575.75
Total Dry Weight:	25500 Lbs	Maximum Seam to Ctr. Of Saddle, (A):	36
Total Wet Weight:	33200 Lbs	Saddle Support Width (SSW):	22
Design Pressure	400 psi	Saddle Gusset Width (SGW):	4
Shell Material:	SA-333-6	Support and Gusset thickness (tsg):	0.5000
Allow. Stress in Tension:	17100 psi	Is a Wear Plate used (Y or N):	Y
Allow. Stress in Comp.:	16744 psi	Wear Plate Thickness (twp):	0.2500
Shell P ipe or P L ate:	PI	Wear Plate Width (WPW):	8
Shell OD:	24.000 IN		
Shell Thickness:	0.5000 IN		
Corrosion Allowance:	0.0625 IN		
Efficiency:	1.0000		

Tube Sheet Thickness : 1.5625

CALCULATIONS

Weight of unit full of water:	33200.0 Lbs	Contact Angle, θ :	127.8
Load per Saddle, Q:	11066.66667 IN	K_1 :	0.3749
Minimum Shell thickness, t_s :	0.3750	K_2 :	1.0530
Shell Outside Radius, R:	12	K_3 :	0.3190
Head or TS Length, H:	1.5625	K_4 :	0.7543
Min. Equiv. Head Thickness, t_h :	0.375	K_5 :	0.3699
		K_6 :	0.0468
		K_7 :	0.7328
		K_8 :	0.6670

LONGITUDINAL BENDING STRESSES:

	<u>ALLOWABLE</u>	<u>ACTUAL</u>
Tension (at the saddles):	17100	7630.0
Compression (at the saddles):	16744	5708.7
Tension (at midspan):	17100	13415.3
Compression (at the midspan):	16744	615.3

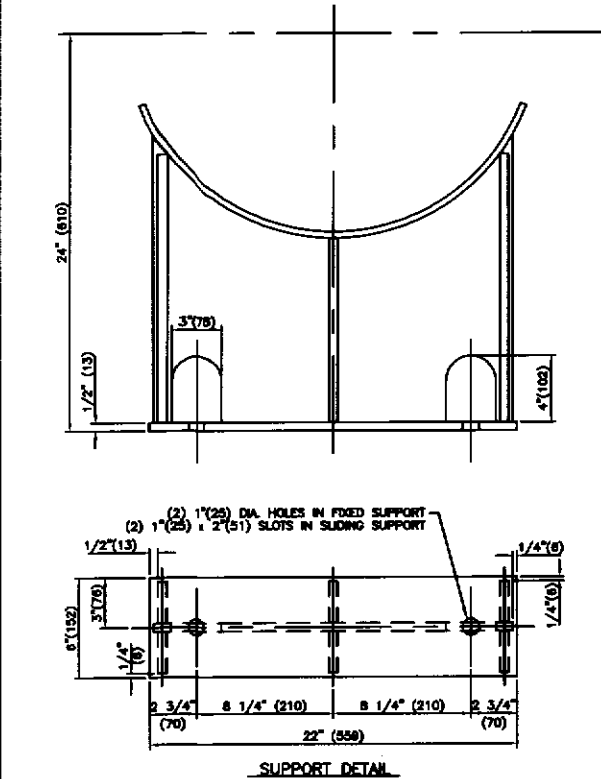
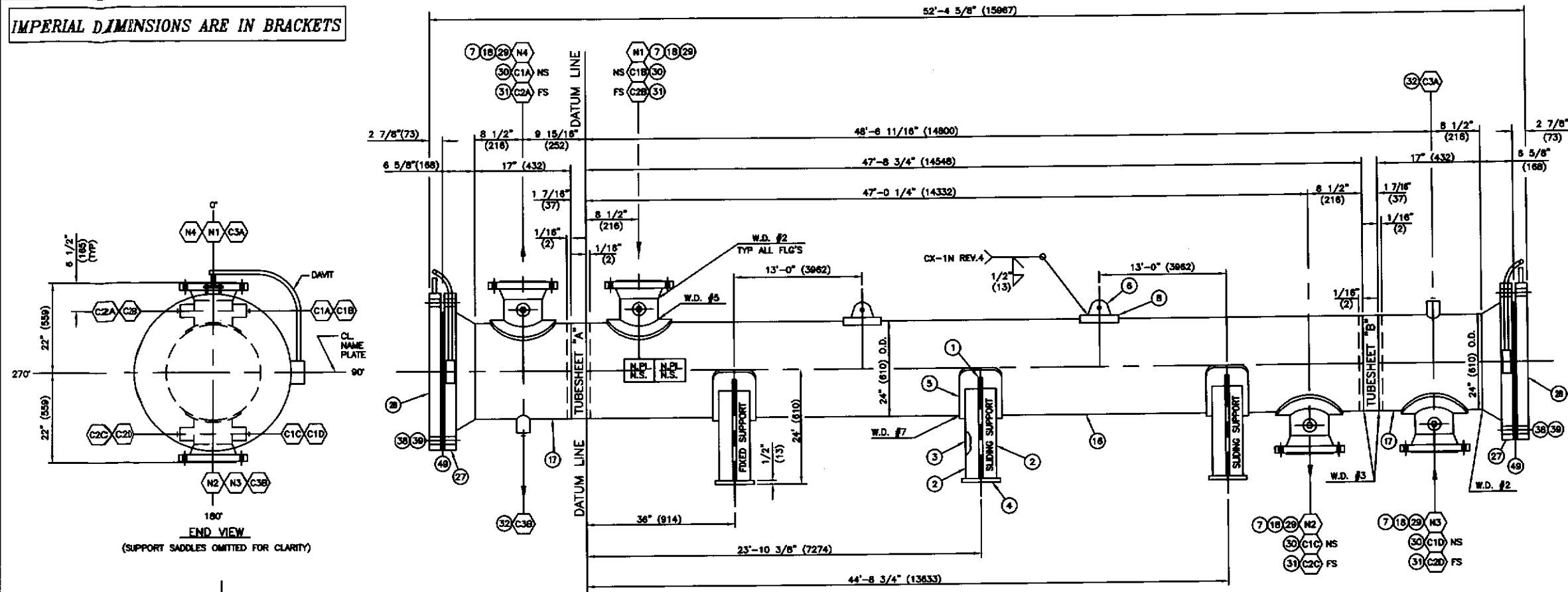
TANGENTIAL SHEAR STRESSES

Shell:	13680	1354.6
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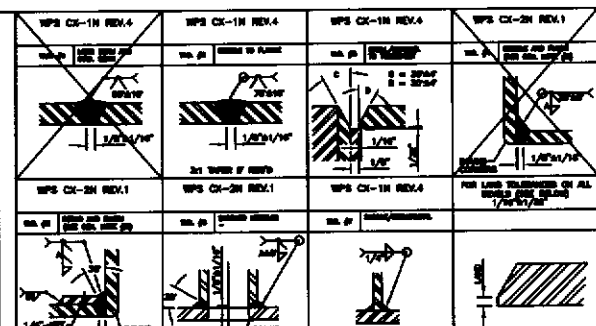
CIRCUMFERENTIAL STRESS

At Horn of Saddle:	25650	6530.8
At Bottom of Shell	8372	1568.5

IMPERIAL DIMENSIONS ARE IN BRACKETS



CONSTRUCTION / GENERAL NOTES					
NO.	DESCRIPTION	REV.	DATE	BY	APP.
1	SURFACE PREP: SEPO-SPS (COMMERCIAL BLAST) PRIMER: ONE COAT OF EPOXY PRIMER (1.5-2.0 mils DFT) PAINT: ONE COAT OF INDUSTRIAL HIGH GLOSS ENAMEL (1.5-2.0 mils DFT) COLOR: WHITE GREY				
2	EXTERNAL DIMENSIONS, NOZZLE, SUPPORT LOCATIONS AND FINISHING TOLERANCES SEE TSD 2007 EDITION, SECTION 2, FIGURES F-1 AND F-2				
1	20	1	YES	MS	DEC.14/12
0	20	0	NO	MS	SEP.12/12
REV.	BY	DESCRIPTION	REV. LEVEL	REQUIRED	APPROVAL



NOZZLE / CONNECTION SCHEDULE									
REF.	QTY.	SIZE	WGT.	TYPE	SERVICE	WELD SIZE A	WELD SIZE B	WELD DETAIL	REMARKS
N1	1	8"	300	SPWN	SHELL SIDE INLET	3/8"	1/4"	2.5	10"
N2	1	8"	300	SPWN	SHELL SIDE OUTLET	3/8"	1/4"	2.5	10"
N3	1	8"	300	SPWN	TUBE SIDE INLET	3/8"	1/4"	2.5	10"
N4	1	8"	300	SPWN	TUBE SIDE OUTLET	3/8"	1/4"	2.5	10"
C1A-D	4	1"	6000	SCOTD	T.L.'S	3/8"	---	0	NO
C2A-D	4	3/4"	6000	SCOTD	P.L.'S	3/8"	---	0	NO
C3A/B	2	1"	6000	SCOTD	WENT / DRINK C/W PLUS	3/8"	---	0	NO

DESIGN DATA			
SHELL SIDE		TUBE SIDE	
DESIGN PRESSURE	400 PSIG + F.V. 1770 MPa + F.V.	400 PSIG + F.V. 2750 MPa + F.V.	
DESIGN TEMPERATURE	165 °F 73 °C	150 °F 70 °C	
MAX. DESIGN MEAN TEMPERATURE	-40 °F -40 °C	-40 °F -40 °C	
WELDING PROCEDURE	ASME SECTION IX, QW-11 (QW-11)	ASME SECTION IX, QW-11 (QW-11)	
STRESS RELIEF	1.5 mm	1.5 mm	
CORROSION ALLOWANCE	0.005"	0.005"	
TEST PRESSURE	600 PSIG	600 PSIG	
WELDING PROCEDURE	ASME SECTION IX, QW-11 (QW-11)	ASME SECTION IX, QW-11 (QW-11)	
MEAN DESIGN TEMP: SHELL: 60.377 °F TUBE: 60.377 °F TUBE SHEET: 74.637 °F TUBE SHEET: 74.637 °F			
WPS: CI-1N REV.4			
WPS: CI-2N REV.1			
WPS: CI-3N REV.1			
WPS: CI-4N REV.1			
WPS: CI-5N REV.1			
WPS: CI-6N REV.1			
WPS: CI-7N REV.1			
WPS: CI-8N REV.1			
WPS: CI-9N REV.1			
WPS: CI-10N REV.1			
WPS: CI-11N REV.1			
WPS: CI-12N REV.1			
WPS: CI-13N REV.1			
WPS: CI-14N REV.1			
WPS: CI-15N REV.1			
WPS: CI-16N REV.1			
WPS: CI-17N REV.1			
WPS: CI-18N REV.1			
WPS: CI-19N REV.1			
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WPS: CI-95N REV.1			
WPS: CI-96N REV.1			
WPS: CI-97N REV.1			
WPS: CI-98N REV.1			
WPS: CI-99N REV.1			
WPS: CI-100N REV.1			

BILL OF MATERIAL			
ITEM	QTY.	DESCRIPTION	P.O.#
PLATE / STRUCTURAL			
1	2	1/2" PL. x 21 1/2" x 17 3/8" LB. - SUPPORT WEB	0-448
2	12	1/2" PL. x 2 1/2" x 16 1/4" - OUTER SUPPORT GUSSETS	0-448
3	6	1/2" PL. x 2 1/2" x 11 1/8" - MIDDLE SUPPORT GUSSETS	0-448
4	3	1/2" PL. x 8" x 22" - SHE PLATES	0-448
5	3	3/8" PL. x 8" x 30" LB. ROLLED TO 24" LB. - SUPPORT WEAR PLATE	SA-510-70H
6	2	1 1/2" THK. PLATE x 7" x 16" - SHELL LIFTING LUGS	SA-510-70H
7	4	1/4" PL. x 12 5/8" O.D. x 8 5/8" LB. ROLLED TO 24" LB. - N1-N4 REPAIRS	SA-510-70H
8	2	3/8" PL. x 8" x 14" LB. ROLLED HARDWAY TO 24" LB. - LIFT LUG REPAIR	SA-510-70H
PIPE / FITTINGS			
16	1	24" - SCH. 40 (0.300") SEAMLESS PIPE x 47'-6 3/4" LB. - SHELL	SA-333-6
17	2	24" - SCH. 40 (0.300") SEAMLESS PIPE x 17" LB. - CHANNELS	SA-333-6
18	4	8" - SCH. 40 (0.300") SEAMLESS PIPE x 7 1/2" LB. - N1, N2, N3, N4	SA-333-6
FORGINGS			
ANSI FLANGES / CPLG'S			
27	2	24" - CLASS 300 RFWN (SCH. 40 BORE) - CHANNEL FLANGES	CLASS 1 SA-350-LF2
28	2	24" - CLASS 300 RF BLED FLANGE - CHANNEL COVER	CLASS 1 SA-350-LF2
29	4	8" - CLASS 300 RFWN (SCH. 40 BORE) - N1, N2, N3, N4	CLASS 1 SA-350-LF2
30	4	1" - CLASS 6000 SCOTD FULL CPLG - C1A-D	CLASS 1 SA-350-LF2
31	4	3/4" - CLASS 6000 SCOTD FULL CPLG - C2A-D	CLASS 1 SA-350-LF2
32	2	1" - CLASS 6000 SCOTD FULL CPLG C/W PLUG - C3A/B	CLASS 1 SA-350-LF2
STUD BOLTS & NUTS			
35	48	1 1/2" DIA. x 8 1/4" LB. STUD BOLTS	SA-193-B7
36	48	1 1/2" DIA. H. HEX NUTS	SA-194-2H
GASKETS			
46	4	24" - CLASS 300 RF. FLUOROC. STYLE G.A. GASKET (SEE DETAIL)	T-3168.S.
NAME PLATES			
58	1	12" LB. x 6" T-BAR STYLE NAME PLATE BRACKETS C/W S.S. NAMEPLATE PLATE (SEE DETAIL)	SA-510-70H
QUANTITIES			
QUANTITIES LISTED ARE FOR ONE UNIT, ONE UNIT REQ'D			
SPECIAL CHEMISTRY			
CERTIFIED AS BUILT			

CALHEX INDUSTRIES LTD.
9515 - 48th STREET S.E.
CALGARY, ALBERTA T2C 2R1

CUSTOMER: EXCELSIOR ENGINEERING
FOR
HUSKY OIL OPERATIONS

PROJECT: INLET GAS HEAT EXCHANGER
(1) NEW 23 x 576
P.O. #: 8400547576
HUSKY OIL ANSELL GAS PLANT

ENGINEERING RECORDS

DESIGNED BY: J. JORDON
CHECKED BY: D. JORDON
APPROVED BY: M. JORDON

DATE: OCT.12/12
DATE: OCT.12/12

SCALE: L.S.D. NO.:
N.T.S.

12-0779-S

Technical drawing of a tubeshheet detail, showing front and side views with dimensions and annotations.

Dimensions:

- Overall length: 1' 9/16"
- Top flange thickness: 3/16" (5)
- Tube side thickness: 22 15/16" (563) DIA
- Shell side thickness: 22 15/16" (563) DIA
- Overall diameter: 24" (610) O.D.
- Bottom flange thickness: 30" (TYP)

Annotations:

- DRILL AND TAP 1/2"(13) DEEP FOR 5/8"(10) DIA TIE RODS SEE T.L.C. FOR LOCATION REQ'D IN TUBESHEET "A" ONLY
- TUBESHEET INSPECTION PER UG-83(d)3

Views:

- Front view (left): Shows the circular cross-section with a central vertical axis and horizontal axis, and a 270° mark.
- Side view (right): Shows the longitudinal section with a central vertical axis and horizontal axis, and a 270° mark.

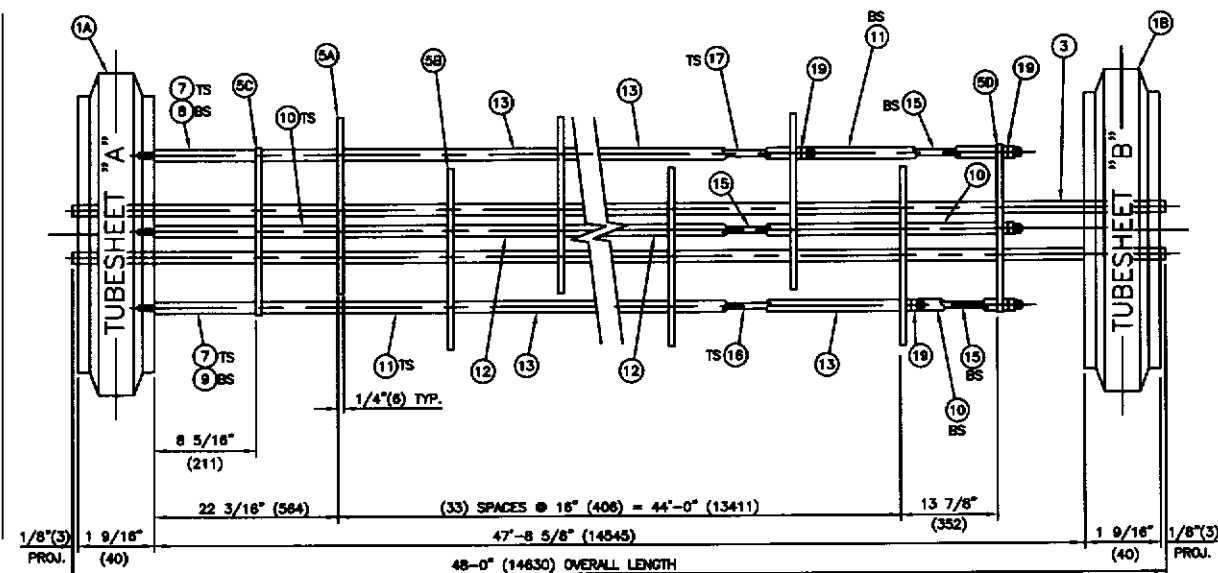
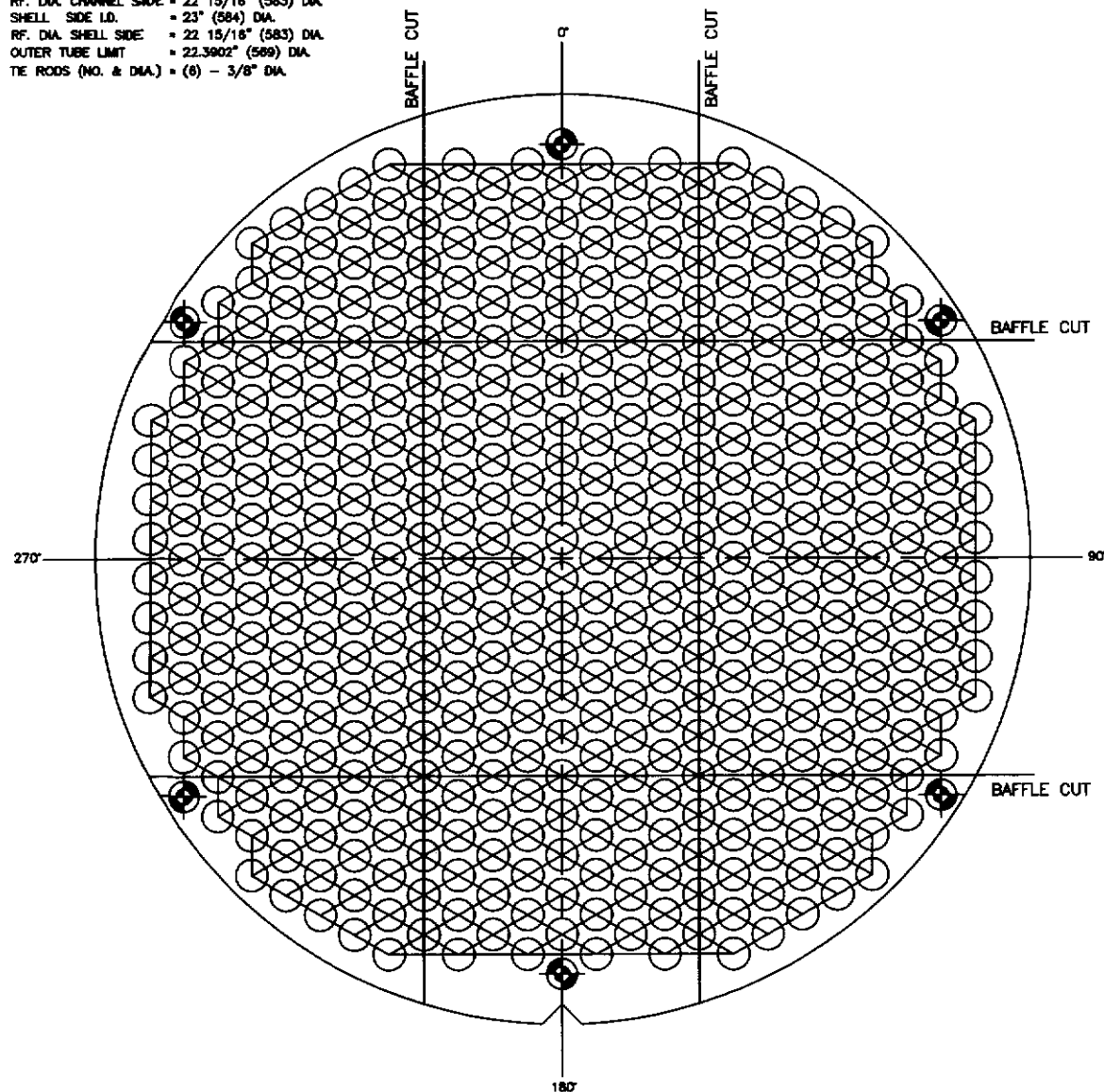
Labels:

- TUBE SIDE
- SHELL SIDE

Section Line:

1-1

(440) 3/4"(19) O.D. x 1/4 BWG x 48'-0" (14830) LG.
ON A 31/32"(24.8) 30° TRI. PITCH
CHANNEL SIDE I.D. = 23" (584) DIA.
RF. DIA. CHANNEL SIDE = 22 15/16" (583) DIA.
SHELL SIDE I.D. = 23" (584) DIA.
RF. DIA. SHELL SIDE = 22 15/16" (583) DIA.
OUTER TUBE LIMIT = 22.3902" (569) DIA.
TIE RODS (NO. & DIA.) = (8) - 3/8" DIA.



5C BAFFLE DETAIL
(1 REQ'D)

5D BAFFLE DETAIL
(1 REQ'D)

5A BAFFLE DETAIL
(17 REQ'D)

5B BAFFLE DETAIL
(17 REQ'D)

[illegible]

CONSTRUCTION / GENERAL NOTES									
NO.									
1									
2									
3									
4									
5									
6									
7									
0	JO	ISSUED FOR APPROVAL	SEE "3" CML	SEE "3" CML	WE	SEPS/1			
REV.	BY	DESCRIPTION	CHG. PACKAGE REV. LEVEL	REQUIRED CHG. REQUIRED	APPROVAL	DATE			
REVISION RECORD									

BILL OF MATERIAL				
ITEM	QTY.	DESCRIPTION	MATERIAL	P.O.#
PLATE				
1	2	1 5/16" PL. x 24" DIA. TUBENET	SA-516-70R	
2				
TUBES				
3	440	3/4" DIA. x #14 BWG (3/16) SDRS ENDS (18 FR 16 GA. UNDER FWD) x 48'-0" SEAMLESS TUBES	SA-178	
4				
BAFFLES				
5	36	1/4" PL. x 22 13/16" O.D. BAFFLES	SA-409	
6				
SPACERS				
7	3	3/4" DIA. x #14 BWG x 8 5/16" L.G. SPACER	SA-178/SA-214	
8	2	3/4" DIA. x #14 BWG x 22 3/16" L.G. SPACER	SA-178/SA-214	
9	1	3/4" DIA. x #14 BWG x 38 3/16" L.G. SPACER	SA-178/SA-214	
10	4	3/4" DIA. x #14 BWG x 13 5/8" L.G. SPACER	SA-178/SA-214	
11	2	3/4" DIA. x #14 BWG x 28 5/8" L.G. SPACER	SA-178/SA-214	
12	66	3/4" DIA. x #14 BWG x 15 3/4" L.G. SPACER	SA-178/SA-214	
13	64	3/4" DIA. x #14 BWG x 31 3/4" L.G. SPACER	SA-178/SA-214	
14				
TIE RODS				
15	3	3/8" DIA. R.R. x 47'-5" L.G. TIE ROD	R.R. SRL	
16	1	3/8" DIA. R.R. x 46'-1" L.G. TIE ROD	R.R. SRL	
17	2	3/8" DIA. R.R. x 44'-8" L.G. TIE ROD	R.R. SRL	
18				
NUTS				
19	12	3/8" DIA. HEX NUTS	SA-320	
20				
IMPACT PLATE				
21				
22				
QUANTITIES				
MATERIAL LISTED IS FOR ONE BUNDLE, ONE BUNDLE REQUIRED				
SPECIAL CHEMISTRY NOTES				

**CERTIFIED
AS BUILT**



CALHEX INDUSTRIES LTD.
9515 - 48th STREET S.E.
CALGARY, ALBERTA T2C 2R1

CUSTOMER: DEXELSOR ENGINEERING
FOR
HUSKY OIL OPERATIONS

PROJECT: INLET GAS HEAT EXCHANGER (1) NEM 23 x 576 P.O. #: 8400547678 HUSKY OIL ANSELL GAS PLANT	ITEM#: E-102B
---	---------------

ENGINEERING RECORD	
2	NAME
DRAWING BY:	J.GREGORY
CHECKED BY:	B.JACKIE
APPROVED BY:	

SCALE	L.S.D. NO.:	-
	DWG. NO.:	
N.T.S.	12-0779-T	

INSTALLATION, OPERATION AND MAINTENANCE

SECTION 4

E-1 PERFORMANCE OF HEAT EXCHANGERS

Satisfactory operation of heat exchangers can be obtained only from units which are properly designed and have built-in quality. Correct installation and preventive maintenance are user responsibilities.

E-1.1 PERFORMANCE FAILURES

The failure of heat exchanger equipment to perform satisfactorily may be caused by one or more factors, such as:

- (1) Excessive fouling.
- (2) Air or gas binding resulting from improper piping installation or lack of suitable vents.
- (3) Operating conditions differing from design conditions.
- (4) Maldistribution of flow in the unit.
- (5) Excessive clearances between the baffles and shell and/or tubes, due to corrosion.
- (6) Improper thermal design.

The user's best assurance of satisfactory performance lies in dependence upon manufacturers competent in the design and fabrication of heat transfer equipment.

E-2 INSTALLATION OF HEAT EXCHANGERS

E-2.1 HEAT EXCHANGER SETTINGS

E-2.11 CLEARANCE FOR DISMANTLING

For straight tube exchangers fitted with removable bundles, provide sufficient clearance at the stationary head end to permit removal of the bundle from the shell and provide adequate space beyond the rear head to permit removal of the shell cover and/or floating head cover.

For fixed tubesheet exchangers, provide sufficient clearance at one end to permit withdrawal and replacement of the tubes, and enough space beyond the head at the opposite end to permit removal of the bonnet or channel cover.

For U-tube heat exchangers, provide sufficient clearance at the stationary head end to permit withdrawal of the tube bundle, or at the opposite end to permit removal of the shell.

E-2.12 FOUNDATIONS

Foundations must be adequate so that exchangers will not settle and impose excessive strains on the exchanger. Foundation bolts should be set to allow for setting inaccuracies. In concrete footings, pipe sleeves at least one size larger than bolt diameter slipped over the bolt and cast in place are best for this purpose, as they allow the bolt center to be adjusted after the foundation has set.

E-2.13 FOUNDATION BOLTS

Foundation bolts should be loosened at one end of the unit to allow free expansion of shells. Slotted holes in supports are provided for this purpose.

E-2.14 LEVELING

Exchangers must be set level and square so that pipe connections may be made without forcing.

E-2.2 CLEANLINESS PROVISIONS

E-2.21 CONNECTION PROTECTORS

All exchanger openings should be inspected for foreign material. Protective plugs and covers should not be removed until just prior to installation.

E-2.22 DIRT REMOVAL

The entire system should be clean before starting operation. Under some conditions, the use of strainers in the piping may be required.

SECTION 4 INSTALLATION, OPERATION AND MAINTENANCE

E-2.23 CLEANING FACILITIES

Convenient means should be provided for cleaning the unit as suggested under "Maintenance of Heat Exchangers," Paragraph E-4.

E-2.3 FITTINGS AND PIPING

E-2.31 BY-PASS VALVES

It may be desirable for purchaser to provide valves and by-passes in the piping system to permit inspection and repairs.

E-2.32 TEST CONNECTIONS

When not integral with the exchanger nozzles, thermometer well and pressure gage connections should be installed close to the exchanger in the inlet and outlet piping.

E-2.33 VENTS

Vent valves should be provided by purchaser so units can be purged to prevent vapor or gas binding. Special consideration must be given to discharge of hazardous or toxic fluids.

E-2.34 DRAINS

Drains may discharge to atmosphere, if permissible, or into a vessel at lower pressure. They should not be piped to a common closed manifold.

E-2.35 PULSATION AND VIBRATION

In all installations, care should be taken to eliminate or minimize transmission of fluid pulsations and mechanical vibrations to the heat exchangers.

E-2.36 SAFETY RELIEF DEVICES

The ASME Code defines the requirements for safety relief devices. When specified by the purchaser, the manufacturer will provide the necessary connections for the safety relief devices. The size and type of the required connections will be specified by the purchaser. The purchaser will provide and install the required relief devices.

E-3 OPERATION OF HEAT EXCHANGERS

E-3.1 DESIGN AND OPERATING CONDITIONS

Equipment must not be operated at conditions which exceed those specified on the name plate(s).

E-3.2 OPERATING PROCEDURES

Before placing any exchanger in operation, reference should be made to the exchanger drawings, specification sheet(s) and name plate(s) for any special instructions. Local safety and health regulations must be considered. Improper start-up or shut-down sequences, particularly of fixed tubesheet units, may cause leaking of tube-to-tubesheet and/or bolted flanged joints.

E-3.21 START-UP OPERATION

Most exchangers with removable tube bundles may be placed in service by first establishing circulation of the cold medium, followed by the gradual introduction of the hot medium. During start-up all vent valves should be opened and left open until all passages have been purged of air and are completely filled with fluid. For fixed tubesheet exchangers, fluids must be introduced in a manner to minimize differential expansion between the shell and tubes.

E-3.22 SHUT-DOWN OPERATION

For exchangers with removable bundles, the units may be shut down by first gradually stopping the flow of the hot medium and then stopping the flow of the cold medium. If it is necessary to stop the flow of cold medium, the circulation of hot medium through the exchanger should also be stopped. For fixed tubesheet exchangers, the unit must be shut down in a manner to minimize differential expansion between shell and tubes. When shutting down the system, all units should be drained completely when there is the possibility of freezing or corrosion damage. To guard against water hammer, condensate should be

INSTALLATION, OPERATION AND MAINTENANCE

SECTION 4

drained from steam heaters and similar apparatus during start-up or shut-down. To reduce water retention after drainage, the tube side of water cooled exchangers should be blown out with air.

E-3.23 TEMPERATURE SHOCKS

Exchangers normally should not be subjected to abrupt temperature fluctuations. Hot fluid must not be suddenly introduced when the unit is cold, nor cold fluid suddenly introduced when the unit is hot.

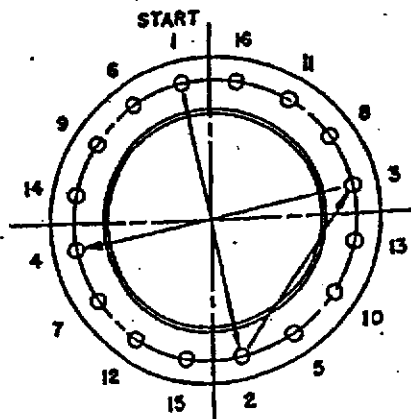
E-3.24 BOLTED JOINTS

Heat exchangers are pressure tested before leaving the manufacturer's shop in accordance with ASME Code requirements. However, normal relaxing of the gasketed joints may occur in the interval between testing in the manufacturer's shop and installation at the jobsite. Therefore, all external bolted joints may require retightening after installation and, if necessary, after the exchanger has reached operating temperature.

E-3.25 RECOMMENDED BOLT TIGHTENING PROCEDURE

It is important that all bolted joints be tightened uniformly and in a diametrically staggered pattern, as illustrated in Figure E-3.25, except for special high pressure closures when the instructions of the manufacturer should be followed.

FIGURE E-3.25



E-4 MAINTENANCE OF HEAT EXCHANGERS

E-4.1 INSPECTION OF UNIT

At regular intervals and as frequently as experience indicates, an examination should be made of the interior and exterior condition of the unit. Neglect in keeping all tubes clean may result in complete stoppage of flow through some tubes which could cause severe thermal strains, leaking tube joints, or structural damage to other components. Sacrificial anodes, when provided, should be inspected to determine whether they should be cleaned or replaced.

E-4.11 INDICATIONS OF FOULING

Exchangers subject to fouling or scaling should be cleaned periodically. A light sludge or scale coating on the tube greatly reduces its efficiency. A marked increase in pressure drop and/or reduction in performance usually indicates cleaning is necessary. The unit should first be checked for air or vapor binding to confirm that this is not the cause for the reduction in performance. Since the difficulty of cleaning increases rapidly as the scale thickness or deposit increases, the intervals between cleanings should not be excessive.

SECTION 4 INSTALLATION, OPERATION AND MAINTENANCE

E-4.12 DISASSEMBLY FOR INSPECTION OR CLEANING

Before disassembly, the user must assure himself that the unit has been depressurized, vented and drained, neutralized and/or purged of hazardous material.

To inspect the inside of the tubes and also make them accessible for cleaning, the following procedures should be used:

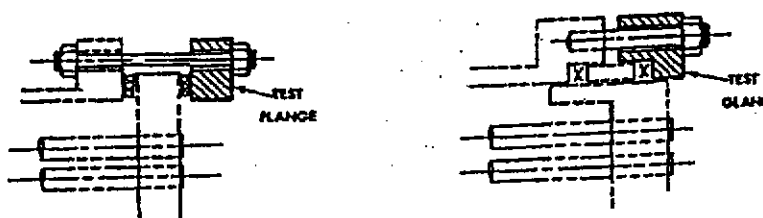
- (1) Stationary Head End
 - (a) Type A, C, D & N, remove cover only
 - (b) Type B, remove bonnet
- (2) Rear Head End
 - (a) Type L, N & P, remove cover only
 - (b) Type M, remove bonnet
 - (c) Type S & T, remove shell cover and floating head cover
 - (d) Type W, remove channel cover or bonnet

E-4.13 LOCATING TUBE LEAKS

The following procedures may be used to locate perforated or split tubes and leaking joints between tubes and tubesheets. In most cases, the entire front face of each tubesheet will be accessible for inspection. The point where water escapes indicates a defective tube or tube-to-tubesheet joint.

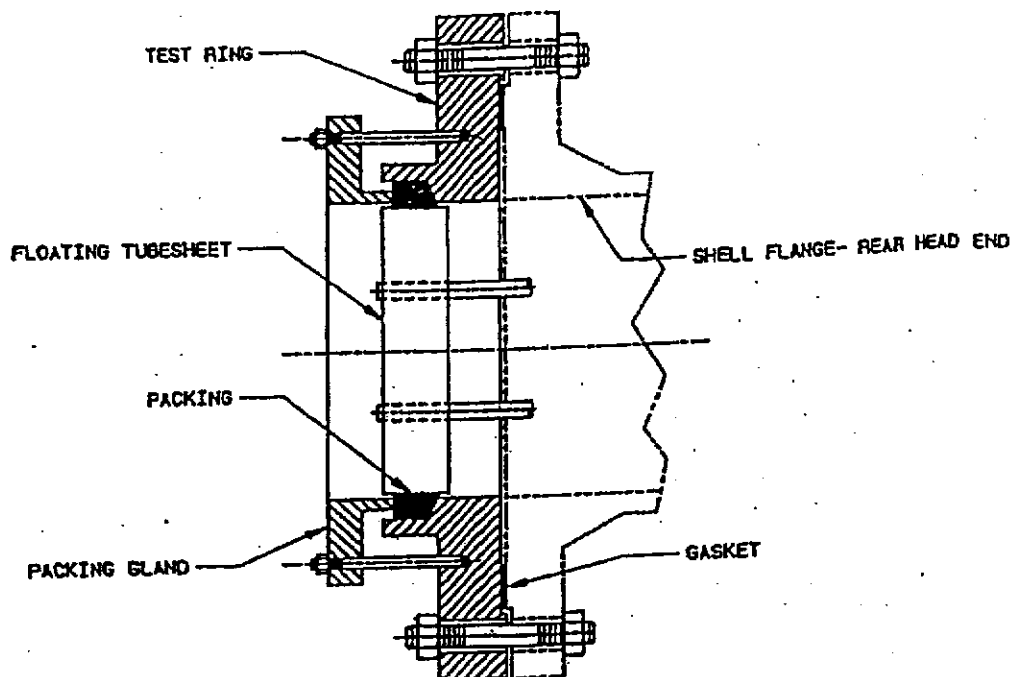
- (1) Units with removable channel cover: Remove channel cover and apply hydraulic pressure in the shell.
- (2) Units with bonnet type head: For fixed tubesheet units where tubesheets are an integral part of the shell, remove bonnet and apply hydraulic pressure in the shell. For fixed tubesheet units where tubesheets are not an integral part of the shell and for units with removable bundles, remove bonnet, re-bolt tubesheet to shell or install test flange or gland, whichever is applicable, and apply hydraulic pressure in the shell. See Figure E-4.13-1 for typical test flange and test gland.

FIGURE E-4.13-1



- (3) Units with Type S or T floating head: Remove channel cover or bonnet, shell cover and floating head cover. Install test ring and bolt in place with gasket and packing. Apply hydraulic pressure in the shell. A typical test ring is shown in Figure E-4.13-2. When a test ring is not available it is possible to locate leaks in the floating head end by removing the shell cover and applying hydraulic pressure in the tubes. Leaking tube joints may then be located by sighting through the tube lanes. Care must be exercised when testing partially assembled exchangers to prevent over extension of expansion joints or overloading of tubes and/or tube-to-tubesheet joints.
- (4) Hydrostatic test should be performed so that the temperature of the metal is over 60° F (16° C) unless the materials of construction have a lower nil-ductility transition temperature.

FIGURE E-4.13-2



E-4.2 TUBE BUNDLE REMOVAL AND HANDLING

To avoid possible damage during removal of a tube bundle from a shell, a pulling device should be attached to eyebolts screwed into the tubesheet. If the tubesheet does not have tapped holes for eyebolts, steel rods or cables inserted through tubes and attached to bearing plates may be used. The bundle should be supported on the tube baffles, supports or tubesheets to prevent damage to the tubes.

Gasket and packing contact surfaces should be protected.

E-4.3 CLEANING TUBE BUNDLES

E-4.3.1 CLEANING METHODS

The heat transfer surfaces of heat exchangers should be kept reasonably clean to assure satisfactory performance. Convenient means for cleaning should be made available.

Heat exchangers may be cleaned by either chemical or mechanical methods. The method selected must be the choice of the operator of the plant and will depend on the type of deposit and the facilities available in the plant. Following are several cleaning procedures that may be considered:

- (1) Circulating hot wash oil or light distillate through tubes or shell at high velocity may effectively remove sludge or similar soft deposits.
- (2) Some salt deposits may be washed out by circulating hot fresh water.
- (3) Commercial cleaning compounds are available for removing sludge or scale provided hot wash oil or water is not available or does not give satisfactory results.
- (4) High pressure water jet cleaning.
- (5) Scrapers, rotating wire brushes, and other mechanical means for removing hard scale, coke, or other deposits.

SECTION 4

INSTALLATION, OPERATION AND MAINTENANCE

- (6) Employ services of a qualified organization that provides cleaning services. These organizations will check the nature of the deposits to be removed, furnish proper solvents and/or acid solutions containing inhibitors, and provide equipment and personnel for a complete cleaning job.

E-4.32 CLEANING PRECAUTIONS

- (1) Tubes should not be cleaned by blowing steam through individual tubes since this heats the tube and may result in severe expansion strain, deformation of the tube, or loosening of the tube-to-tubesheet joint.
- (2) When mechanically cleaning a tube bundle, care should be exercised to avoid damaging the tubes.
- (3) Cleaning compounds must be compatible with the metallurgy of the exchanger.

E-4.4 TUBE EXPANDING

A suitable tube expander should be used to tighten a leaking tube joint. Care should be taken to ensure that tubes are not over expanded.

E-4.5 GASKET REPLACEMENT

Gaskets and gasket surfaces should be thoroughly cleaned and should be free of scratches and other defects. Gaskets should be properly positioned before attempting to retighten bolts. It is recommended that when a heat exchanger is dismantled for any cause, it be reassembled with new gaskets. This will tend to prevent future leaks and/or damage to the gasket seating surfaces of the heat exchanger. Composition gaskets become dried out and brittle so that they do not always provide an effective seal when reused. Metal or metal jacketed gaskets, when compressed initially, flow to match their contact surfaces. In so doing they are work hardened and, if reused, may provide an imperfect seal or result in deformation and damage to the gasket contact surfaces of the exchanger.

Bolted joints and flanges are designed for use with the particular type of gasket specified. Substitution of a gasket of different construction or improper dimensions may result in leakage and damage to gasket surfaces. Therefore, any gasket substitutions should be of compatible design.

Any leakage at a gasketed joint should be rectified and not permitted to persist as it may result in damage to the gasket surfaces.

Metal jacketed type gaskets are widely used. When these are used with a tongue and groove joint without a nubbin, the gasket should be installed so that the tongue bears on the seamless side of the gasket jacket. When a nubbin is used, the nubbin should bear on the seamless side.

E-4.6 SPARE AND REPLACEMENT PARTS

The procurement of spare or replacement parts from the manufacturer will be facilitated if the correct name for the part, as shown in Section 1, Table N-2, of these Standards is given, together with the serial number, type, size, and other information from the name plate. Replacement parts should be purchased from the original manufacturer.

E-4.7 PLUGGING OF TUBES

In U-tube heat exchangers, and other exchangers of special design, it may not be feasible to remove and replace defective tubes. Defective tubes may be plugged using commercially available tapered plugs with ferrules or tapered only plugs which may or may not be seal welded. Excessive tube plugging may result in reduced thermal performance, higher pressure drop, and/or mechanical damage. It is the user's responsibility to remove plugs and neutralize the bundle prior to sending it to a shop for repairs.

U

W

—

—

RT2-T

RT2-S

TS MAEWP 15 PSI AT 158°F
SS MAEWP 15 PSI AT 163°F

CRN

V9688.21

PROV. REG.

(A)

6260

TAG NO.

E-102 B

CERTIFIED BY

CALHEX INDUSTRIES LTD.

CALGARY, ALBERTA, CANADA



MAWP

400

PSIG

AT

158

°F

TEMP. SIDE

MDMT

-49

°F

AT

400

PSIG

MAWP

400

PSIG

AT

163

°F

TEMP. SIDE

MDMT

-49

°F

AT

PSIG

SERIAL NO.

12-0779

YEAR BUILT

**CALHEX INDUSTRIES LTD.**9515 - 48th Street S.E., Calgary, Alberta, T2C 2R1

Bus: (403) 225 - 4395

{CALHEX5}

Fax: (403) 261 - 2761

MATERIAL CONTROL SHEETJob #: 12-0779Item #: E-102B

Part Description	Material Specification	Material Tracking # / Heat # - Plate Identifier	Part Description	Material Specification	Material Tracking # / Heat # - Plate Identifier
TUBES	SA179	193106	NOZZLE REWN	SA333-LF2 CL.1	12/30011
"	"	213254			
			NOZZLE PIPE	SA333-L	8368 (268216)
TUBESHEETS	SA516-70N	8663 (344655-30841)			
			NOZZLE REPADS	SA516-70N	8998 (W2H905-D01)
SHELL CYLINDERS	SA333-L	8959 (MA3971)			
CHANNEL REWN	SA333-LF2 CL.1	H6742/3			
CHANNEL CYLINDERS	SA333-L	8959 (MA3971)			
CHANNEL COVERS	SA333-LF2 CL.1	198658			
SUPPORT WEAR PADS	SA516-70N	8947 (S699M-01115)			
LIFT LUG REPADS	SA516-70N	8947 (S699M-01115)			

Above materials meet the requirements of ASME Section II Part A

Quality Control Signature: Date: DEC 12 2012

**RONCONI SpA****COLD DRAWN STEEL TUBES**20090 OPERA (MI) - Via Lambro, 9-ITALY
www.ronconi.com - quality@ronconi.com

CERTIFICATO PROVE MATERIALI

Mod. MDCQ01 B7

Test Certificate - Abnahmeprüfzeugnis

EN 10204 3.1REPARTO
COLLAUDO C.Inspezione Dept. -
Abnahmeabteilungum. Cert. **11893**Data **05/06/2012**

Date - Datum

Foglio 1/1
Sheet - BlattCliente **HEAT TRANSFER TUBULAR PRODUCTS LLC**

Customer - Kunde

Ordine num. PST 221

Order - Bestellung

Descrizione **COLD DRAWN SEAMLESS TUBES**

Description - Beschreibung

Norma e Acciaio **ASME SA179**

Norm and Steel Grade - Norm und Stahlgüte

Pezzi **200+500+520**

Quantity - Anzahl

Peso kg. **18865**

Weight - Gewicht

Dimensioni **19,05 x 2,11MW x 12217/13437/14656 mm**

Sizes - Abmessungen

Data **23/04/2012**

Date - Datum

Ns. Commessa **32 13 12 405/2**

Our order - Unsere Bestellung

Trattamento termico **Normalized**

Heat treatment - Wärmebehandlung

In accordo a **YOUR REF. ST221**

Acc.to - Gemäss

Data **21/05/2012**

Date - Datum

Valori richiesti Requirements Anforderungen			Rs min	Rm min max		A _{2"} min	A _{p5} min	HRB min max 72		min	med	min			
Provino Specimen Probekörper			Snervamento Yield point Streckgrenze	Rottura Tensile strength Zugfestigkeit		Allungamento Elongation Bruchdehnung		Durezza Hardness Härte		Resilienza Notch impact Kerbschlagarbeit		Prova a caldo Hot test Wärmeproofung			
N	Sez mm ²	Lo mm	Risultati ottenuti (Results - Ergebnisse)												
			N/mm2	N/mm2	%	%		J	J	N/mm2					
1								65 ✓							
2								66 ✓							
3								66 ✓							
4								67 ✓							
5	Prova di Schiacciamento eseguita con esito positivo - Flattening test satisfactory - Aufweitversuch zufriedenstellend durchgeführt												OK		
6	Prova di Allargamento eseguita con esito positivo - Flaring test satisfactory - Ringfaltversuch zufriedenstellend durchgeführt													OK	
7															
8															
9															
10															
11															
12															
13															
14															
15															
16															
17															
18															

MATERIAL CHECKED TO
ASME SECTION II BY
CAL HEX INDUSTRIES LTD.

CONFORMS TO 2010 EDITION: 2011 ADDENDA

DATE: DEC 11/12

SIGNATURE:

MIN. TEK.:

Si certifica che è stato eseguito con esito positivo il: ☒ Controllo (100%) Eddy current secondo norma **ASME SA450 24.8.2.1**
Eddy current test (100%) acc.to - Wirbelstromprüfung (100%) gemäss
☐ Controllo (100%) Ultrasuoni secondo norma
Ultrasonic test (100%) acc.to - Ultraschallprüfung (100%) gemäss
☐ Controllo PMI (100%)
PMI test (100%) - PMI (100%)

Il controllo visivo e dimensionale dei tubi è stato eseguito con esito positivo
The visual and dimensional test has been performed with satisfactory result - Die visuellen und dimensional Kontrollen wurden mit zufriedenstellenden Ergebnissen durchgeführt

Analisi chimica Chemical analysis - Chemische Analyse										Acciaio calmato ed elaborato al forno elettrico, degasato a vuoto Steel elaborated in electric furnace, fully killed and vacuum degassed - Beruhigter Elektro Vakuum entgast Stahl									
Colata N. Heat No - Schmelze Nr	C %	Si %	Mn %	P %	S %	Cr %	Mo %	Ni %	Cu %	V %	Nb %	Al %	N %	Sn %	Ti %	As %	Sb %		
193106	0,100		0,46	0,009	0,003														
213254	0,095		0,46	0,007	0,002														

Marcatura (Marking - Markierung) **RONCONI/ITALY/SA179/HEATNO/19,05X2,11/MW**

Note Notes - Anmerkungen

ORIGIN OF RAW MATERIAL: GERMANY
MANUFACTURER: RONCONI SPA - ITALY
Tests n° 1-2-5-6 heat n° 193106: 1020 tubes
Tests n° 3-4-5-6 heat n° 213254: 500 tubes

Il Capo reparto

Chief of Dept. - Abteilungschef
CND II Lev. ET-UT Cert. n. FG1746**RONCONI SpA**
CONTROLLO QUALITÀ
QUALITY CONTROL

Ente collaudatore

Inspected by - Abnahmebeamter



edmonton exchanger
& manufacturing ltd.

CERTIFICATE OF COMPLIANCE

5545-89 Street Edmonton, Alberta Canada T6E 5W9

www.edmontonexchanger.com

tel 780.468.6722 • QC fax 780.466.4668 • sales fax 780.466.5155

Customer CALHEX INDUSTRIES LTD.

PO CX-07737

Work Order C89057 Date 2011/04/18 ColCa 24156 Page 1 of 1

Item#	Description	Qty	Heat#
P89057-1	PLATE(S) - 2.0000" NOM X 121" X 72" (Material Spec: SA 516-70 Normalized) Conforms to NACE MR0175 / ISO 15156-2 2009 Annex A	1	350925-23140
P89057-2	PLATE(S) - 1.7500" NOM X 121" X 72" (Material Spec: SA 516-70 Normalized) Conforms to NACE MR0175 / ISO 15156-2 2009 Annex A	1	344655-30841 B663
P89057-3	PLATE(S) - 1.5000" NOM X 121" X 72" (Material Spec: SA 516-70 Normalized) Conforms to NACE MR0175 / ISO 15156-2 2009 Annex A	1	350924-23519
P89057-4	PLATE(S) - 1.0000" NOM X 121" X 60" (Material Spec: SA 516-70 Normalized) Conforms to NACE MR0175 / ISO 15156-2 2009 Annex A	1	G7492-879270448

Brinell Equipment: Newage Calibrated Pin
Brinell Hardness Tester

Material being supplied conforms to the latest ASME Code Section II, Part A, 2010 Edition. All welders and procedures are qualified to ASME Code Section IX.

Supplementary Examination - Items

CE=0.39
NACE-OK
-SD-OK
S≤0.006





DILLINGER HÜTTE

Erläuterungen siehe Rückseite/Explications voir au verso/See revers for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch	A08 Manufacturer's order/ A03 Certificate No.	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10	354135-003	1/9
MATERIAL TEST REPORT (MTR)				
A05 Established inspecting body	A06 Purchaser	A07.1 No.	901 Product	
DH	EDMONTON STEEL, EDMON	ED10548-J1010-ER	HOT ROLLED PLATES	
Final receiver		A07.2 No.		
		EDMONTON STEEL, EDMON		
SA20-S5				
B02 Steel design	SA516-70			
B03 Any suppl. requirements	ASME-III-A:07+A09			
DIL-HUR-3:R29-2010-01-31				

A01-A99 Further commercial information - Concession requests

B14 Item No.	B07.1 Heat No.	B16 Concession request no.	Date
03	344653	30842-01 1-CK2WP	06.04.10
03	344653	30843-01 1-CJVK2	06.04.10

B01-B99 Description of the product

B14 Item No.	B08 Number of pieces	B09 Thickness	B10 Width	B11 Length	B12 Theoretical mass	B04 Predicted delivery condition	B07.2 Heat No.	B07.1 Rolled plate No. Test No.
01	1	1,5000	121,00000	480,00000	11207	N	344653	32210-01
01	1	1,5000	121,00000	480,00000	11207	N	344653	32210-02
02	1	1,6250	97,00000	480,00000	9733	N	344653	30848-01
02	1	1,6250	97,00000	480,00000	9733	N	344653	30848-02
03	1	1,7500	121,00000	480,00000	13075	N	344652	32216-01
03	1	1,7500	121,00000	480,00000	13075	N	344653	30842-01
03	1	1,7500	121,00000	480,00000	13075	N	344653	30843-01
03	1	1,7500	121,00000	480,00000	13075	N	344655	28436-01
03	1	1,7500	121,00000	480,00000	13075	N	344655	30836-01
03	1	1,7500	121,00000	480,00000	13075	N	344655	30837-01
03	1	1,7500	121,00000	480,00000	13075	N	344655	30841-01
05	1	2,0000	121,00000	480,00000	14943	N	344657	28426-01
05	1	2,0000	121,00000	480,00000	14943	N	344657	28428-01
05	1	2,0000	121,00000	480,00000	14943	N	344657	28429-01
05	1	2,0000	121,00000	480,00000	14943	N	344657	28430-01

201/202/203 We, hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.

QM-System: Certification as per ISO 9001

AG der Dillinger Hüttenwerke
Postfach 1880, D-66748 Dillingen/Saar
Inspection department

Inspector's stamp
Date 14.05.10
BM 1

Test House Manager
B. MUELLER



CONFORMS TO 2010 EDITION: 2011 ADDENDA

MATERIAL CHECKED TO
ASME SECTION II BY
CALHEX INDUSTRIES LTD.
DATE: MAY 15, 2011
SIGNATURE: JPK
MIN. THK.: 1.772"

CONFORMS TO 2010 EDITION: 2011 ADDENDA

JOB # STOCK
HEAT CODE #344653
(344655-30841)



DILLINGER HÜTTE

Erläuterungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificates)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch	A09 Manufacturer's order/ A03 Certificate No.	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991-A1:1995 + AS PER ISO 10474:1991		360093-14.05.10	354135-003	2/...
MATERIAL TEST REPORT (MTR)				
A05 Established inspecting body	A06 Purchaser	B01 Product		
DH	Final receiver	HOT ROLLED PLATES		
B02 Steel design.				
SA516-70				
B03 Any suppl. requirements				
ASME-II-A:07+A09				
DIL-HUB-3:R29-2010-01-31				
		SA20-S5		

B01-B99 Description of the product

B14 Item No.	B08 Number of pieces	B10 Thickness	B10 Width	B11 Length	B12 Theoretical mass	B04 Product delivery condition	B07.2 Heat No.	B07.1 Rolled plate No./ Test No.	A09 Purchaser article number
05	1	2,0000 x	121,00000 x	480,00000	14943	N	344657	28431-01	
05	1	2,0000 x	121,00000 x	480,00000	14943	N	344657	28432-01	
05	1	2,0000 x	121,00000 x	480,00000	14943	N	344657	28433-01	
**	7				104601				
06	1	2,2500 x	121,00000 x	480,00000	16810	N	344659	22452-01	
06	1	2,2500 x	121,00000 x	480,00000	16810	N	344659	23550-01	
**	2				33620				
***	20				271626				

B04 Product delivery condition

ITEM NO.: 01-06
N: HT: 1670 GR.F +36 -27 GR.F
SOAKING TIME TO ATTAIN THE TARGET TEMPERATURE OVER THE WHOLE SECTION: 1-1,75 MIN/MM (25-45 MIN/INCH)
COOLING IN STILL AIR

B06 Marking of the product

ITEM NO.: 01-06
STEEL DESIGNATION SA516 70 MLTV SA516 60 MLTV
HEAT NO. / TRADEMARK / ROLLED PLATE NO.-TEST NO. / INSPECTOR'S STAMP

B07-B99 Further information about the product

ITEM NO.: 01-06
THICKNESS REDUCTION RATIO $\geq 3,0$ IS FULFILLED (CF. A/SA20 PAR. 5.3)

A04		20/10/2023 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.	AG der Dillinger Hüttenwerke Postfach 1580, D-66748 Dillingen/Saar Inspection department	Inspector's stamp Date 14.05.10	BM 1
QM-System: Certification as per ISO 9001					
B. MUELLER Test House Manager					



DILLINGER HÜTTE

Erläuterungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch	A08/ Manufacturer's order/ A03 Certificate No.	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10	354135-003	3/...
MATERIAL TEST REPORT (MTR)				
A05 Established inspecting body	A06 Purchaser	B01 Product		
DH	Final receiver	HOT ROLLED PLATES		
EDMONTON STEEL, EDMON		EDMONTON STEEL, EDMON		
A07.1 No. ED10548-J1010-ER				
A07.2 No.				
SA20-S5				
B02/ Steel design. SA516-70				
B03 Any suppl. ASME-II-A:07+A09				
requirements DIL-HUE-3:R29-2010-01-31				

C10-C29 Tensile test

914 B07.2 Item Heat No. No.	B07.1 Rolled/ Test No.	B05 Reference (heat) treatment	C01 C02 C03 C10 C11 Temp. ORF	C12 RM	C13 A % L0-ZIN	C14-C15
01 344653 32210			K1 QV RT 48,1	75,0	41	
02 344653 30848			K1 QV RT 48,1	74,5	36	
03 344652 32216			K1 QV RT 47,9	74,7	37	
03 344653 30842			K1 QV RT 48,3	74,1	40	
03 344653 30843			K1 QV RT 48,0	74,4	38	
03 344655 28436			K1 QV RT 45,8	73,1	40	
03 344655 30836			K1 QV RT 47,9	74,0	39	
03 344655 30837			K1 QV RT 47,4	73,8	37	
03 344655 30841			K1 QV RT 48,0	73,5	39	
05 344657 28426			K1 QV RT 47,0	73,4	40	
05 344657 28428			K1 QV RT 48,9	74,1	38	
05 344657 28429			K1 QV RT 47,7	74,0	39	
05 344657 28430			K1 QV RT 47,1	72,8	41	
05 344657 28431			K1 QV RT 46,7	73,7	40	
05 344657 28432			K1 QV RT 47,7	73,7	42	
05 344657 28433			K1 QV RT 48,3	73,7	39	
06 344659 22452			K1 QV RT 44,7	74,5	39	
06 344659 23550			K1 QV RT 44,4	73,7	37	

201202203 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.

QM-System: Certification as per ISO 9001

AG der Dillinger Hüttenwerke
Postfach 1580, D-66748 Dillingen/Saar
Inspection department



B. NOELLER
Test House Manager

Inspector's stamp

Date 14.05.10

BM





DILLINGER HÜTTE

Erfüllungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificates)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10	4/...
MATERIAL TEST REPORT (MTR)			

A05 Established inspecting body	A06 Purchaser	A07.1 No.	A07.2 No.
DH	EDMONTON STEEL, EDMONTON	ED10548-J1010-ER	
	Final receiver		
	EDMONTON STEEL, EDMONTON		

S02 Steel design	SA516-70	SA20-S5
S03 Any suppl. requirements	ASME-II-A:07+A09	
	DIL-HUE-3:R29-2010-01-31	

C30-C39 Hardness test									
B14 Item No.	B07.2 Heat No.	B07.1 Roll plate/ Test No.	B05 Reference (heat) treatment	C01	C02/C01	C03 Temp. °C/°F	C33 Testing method	C35 Individual values	C32 Mean value
01	344653	32210		K1	O	RT HBW 10/3000		HB 143	142
02	344653	30848		K1	O	RT HBW 10/3000		HB 146	142
03	344652	32216		K1	O	RT HBW 10/3000		HB 139	138
03	344653	30842		K1	O	RT HBW 10/3000		HB 141	142
03	344653	30843		K1	O	RT HBW 10/3000		HB 140	141
03	344655	28436		K1	O	RT HBW 10/3000		HB 138	136
03	344655	30836		K1	O	RT HBW 10/3000		HB 138	137
03	344655	30837		K1	O	RT HBW 10/3000		HB 140	142
03	344655	30841		K1	O	RT HBW 10/3000		HB 139	138
05	344657	28426		K1	O	RT HBW 10/3000		HB 138	138
05	344657	28428		K1	O	RT HBW 10/3000		HB 142	140
05	344657	28429		K1	O	RT HBW 10/3000		HB 138	138
05	344657	28430		K1	O	RT HBW 10/3000		HB 141	141
05	344657	28431		K1	O	RT HBW 10/3000		HB 135	136
05	344657	28432		K1	O	RT HBW 10/3000		HB 139	138
05	344657	28433		K1	O	RT HBW 10/3000		HB 142	140
06	344659	22452		K1	O	RT HBW 10/3000		HB 144	143
06	344659	23550		K1	O	RT HBW 10/3000		HB 138	138

A04	Z01/Z02/Z03 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.	AG der Dillinger Hüttenwerke Postfach 1580, D-66748 Dillingen/Saar Inspection department	AG der Dillinger Hüttenwerke Postfach 1580, D-66748 Dillingen/Saar Inspection department
	DM-System: Certification as per ISO 9001		
		B. MUELLER Test House Manager	Inspector's stamp Date 14.05.10
			BM 1



DILLINGER HÜTTE

Erklärungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch		A08/ Manufacturer's order/ A03 Certificate No.		Sheet	
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10		354135-003		5/...	
MATERIAL TEST REPORT (MTR)				B01 Product			
A05 Established inspecting body DIL		Final receiver		HOT ROLLED PLATES			
EDMONTON STEEL, EDMONTON		EDMONTON STEEL, EDMONTON					
A07.1 No. ED10548-J1010-ER		A07.2 No.					
B02/ Steel design. SA516-70							
B03 Any suppl. requirements		DIL-HUE-3:R29-2010-01-31					

C40-C48 Impact test												
B14 Item No.	B07.2 Heat No.	B07.1 Red plate/ Test No.	B05 Reference (heat) treatment	C01	C02/ C01	C03 Temp. QRT	C41 Width of test piece	C46 Type of test piece	C44 Testing method	C48 Energy	C45 C42 Individual values AV-FT LBF	C43 Mean value
01	344653	32210		K1	LV	-51		CHP-V			82	96
02	344653	30848		K1	LV	-51		CHP-V			111	97
03	344652	32216		K1	LV	-51		CHP-V			103	128
03	344653	30842		K1	LV	-51		CHP-V			97	72
03	344653	30843		K1	LV	-51		CHP-V			108	96
03	344655	28436		K1	LV	-51		CHP-V			55	104
03	344655	30836		K1	LV	-51		CHP-V			102	83
03	344655	30837		K1	LV	-51		CHP-V			72	117
03	344655	30841		K1	LV	-51		CHP-V			75	116
05	344657	28426		K1	LV	-51		CHP-V			101	97
05	344657	28428		K1	LV	-51		CHP-V			82	91
05	344657	28429		K1	LV	-51		CHP-V			119	81
05	344657	28430		K1	LV	-51		CHP-V			82	120
05	344657	28431		K1	LV	-51		CHP-V			109	94
05	344657	28432		K1	LV	-51		CHP-V			17	21
05	344657	28433		K1	LV	-51		CHP-V			59	71
06	344659	22452		K1	LV	-51		CHP-V			97	90
06	344659	23550		K1	LV	-51		CHP-V			105	96

A04	2017/02/2013 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.	AG der Dillinger Hüttenwerke Postfach 1580, D-66748 Dillingen/Saar Inspection department	ADH	Inspector's stamp	Date 14.05.10	BM 1
QM-System: Certification as per ISO 9001		B. MUELLER Test House Manager				



DILLINGER HÜTTE

Erklärungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch	A08 Manufacturer's order/ A03 Certificate No.	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10	354135-003	6/...
MATERIAL TEST REPORT (MTR)				
A05 Established inspecting body	A06 Purchaser	B01 Product		
DH	Final receiver	HOT ROLLED PLATES		
B02 Steel design.				
SA516-70				
B03 Any suppl.	EDMONTON STEEL, EDMON	A07.1 No. ED10548-J1010-ER		
requirements	EDMONTON STEEL, EDMON	A07.2 No.		
DIL-HUE-3:R29-2010-01-31		SA20-85		

C70-C89 Chemical composition % - Heat analysis

	C70	C	SI	MN	P	S	N	CU	MO	NI	CR	V	NB	SN	TI
B07.2 Heat															
344652	Y	0.184	0.359	1.18	0.011	0.0008	0.0057	0.019	0.011	0.025	0.030	0.000	0.000	0.001	0.002
344653	Y	0.173	0.361	1.17	0.010	0.0009	0.0078	0.025	0.014	0.031	0.024	0.000	0.000	0.000	0.002
344655	Y	0.178	0.301	1.18	0.010	0.0007	0.0074	0.023	0.009	0.035	0.030	0.000	0.000	0.001	0.002
344657	Y	0.174	0.338	1.19	0.011	0.0009	0.0059	0.028	0.015	0.035	0.029	0.000	0.000	0.000	0.002
344659	Y	0.170	0.365	1.18	0.009	0.0009	0.0063	0.016	0.004	0.025	0.222	0.001	0.000	0.001	0.002
B07.2 Heat															
344652	Y	0.0000	0.0016	0.031											
344653	Y	0.0001	0.0016	0.034											
344655	Y	0.0001	0.0012	0.031											
344657	Y	0.0001	0.0016	0.027											
344659	Y	0.0001	0.0012	0.045											

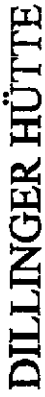
C94 Heat analysis Carbon equivalent / Alloying restrictions

	FO-02=	FO-51=	FO-55=	FO-78=	FO-91=
B07.2 Heat					
344652	0.39	0.000	0.09	0.04	6.4
344653	0.38	0.000	0.09	0.04	6.8
344655	0.39	0.000	0.10	0.04	6.6
344657	0.39	0.000	0.11	0.04	6.8
344659	0.41	0.001	0.27	0.23	6.9

C95 Ladle treatment

ITEM NO.: 01-06	HEAT OF THE INDICATED ITEM: VACUUM DEGASSED / SULPHIDE SHAPE CONTROL
-----------------	--

A04	20/12/2023 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.	AG der Dillinger Hüttenwerke Postfach 1580, D-66748 Dillingen/Saar Inspection department	Date 14.05.10	BM 1
				
QM-System: Certification as per ISO 9001		B. MUELLER Test House Manager		



INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991
MATERIAL TEST REPORT (MTR)

**A08/ Manufacturer's order/
A03 Certificate No.**

Summary

B02/ Stiel design.	SA516-70	SA20-S5
--------------------	----------	---------

B03 Any suppl. requirements **ASME-II-A:07+A09**
DIL-HUE-3:R29-201

C95 Further information about ladle treatment

ITEM NO.: 01-06

CALCIUM TREATED

C70-C99.Chemical composition % - Product analysis

B07.2	B07.1	C01	C	SI	MN	P	S	N	CU	MO	NI	CR	V	NB	SN	T
Heat	Test No.															
344652	32213	K1	0,182	0,353	1,16	0,011	0,0008	0,0056	0,018	0,010	0,023	0,030	0,001	0,000	0,000	0,002
344652	32216	K1	0,178	0,361	1,16	0,010	0,0010	0,0061	0,014	0,012	0,030	0,030	0,000	0,000	0,001	0,002
344653	30844	K1	0,178	0,358	1,16	0,009	0,0009	0,0067	0,025	0,014	0,029	0,023	0,001	0,000	0,000	0,002
344653	30846	K1	0,175	0,354	1,16	0,009	0,0010	0,0069	0,025	0,015	0,031	0,024	0,001	0,000	0,001	0,002
344653	32208	K1	0,180	0,366	1,16	0,010	0,0011	0,0061	0,020	0,012	0,025	0,027	0,000	0,000	0,001	0,002
344653	32209	K1	0,178	0,358	1,16	0,009	0,0011	0,0068	0,023	0,013	0,029	0,025	0,000	0,000	0,001	0,002
344655	28434	K1	0,178	0,291	1,16	0,009	0,0009	0,0066	0,022	0,009	0,035	0,029	0,000	0,000	0,001	0,002
344655	28435	K1	0,178	0,292	1,16	0,009	0,0009	0,0066	0,022	0,007	0,034	0,030	0,000	0,001	0,000	0,002
344655	30836	K1	0,175	0,302	1,16	0,010	0,0011	0,0067	0,022	0,009	0,035	0,029	0,000	0,000	0,001	0,002
344657	28431	K1	0,174	0,327	1,16	0,010	0,0009	0,0053	0,026	0,013	0,032	0,029	0,000	0,000	0,000	0,002
344659	23555	K1	0,169	0,361	1,16	0,008	0,0009	0,0063	0,012	0,004	0,019	0,210	0,001	0,000	0,000	0,002

B07.2	B07.1	C01	B	CA	AL-T
Heat	Test No.				
344652	32213	K1	0,0001	0,0017	0,032
344652	32216	K1	0,0002	0,0013	0,032
344653	30844	K1	0,0000	0,0015	0,034
344653	30846	K1	0,0002	0,0016	0,035
344653	32208	K1	0,0000	0,0016	0,032
344653	32209	K1	0,0001	0,0016	0,033
344655	28434	K1	0,0000	0,0010	0,030
344655	28435	K1	0,0001	0,0012	0,031

2017/02/2303 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.

QM-System: Certification as per ISO 9001

$$\frac{A}{B}$$

AG der Dillinger Hüttenwerke
Postfach 1580, D-66748 Dillingen/Saar
Inspection department

B. MUELLER
Test House Manager

Inspector's stamp Date 14.05.10

BM 1



DILLINGER HÜTTE

Erklärungen: siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004 INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+AI:1995 + AS PER ISO 10474:1991 MATERIAL TEST REPORT (MTR)		A10 Advice of dispatch No./ Date of dispatch 360093-14.05.10	A08 Manufacturer's order/ A03 Certificate No. 354135-003	Sheet 8/...
A05 Established inspecting body DH		A06 Purchaser EDMONTON STEEL, EDMONTON A07.1 No. ED10548-J1010-ER Final receiver EDMONTON STEEL, EDMONTON A07.2 No. SA20-S5		
B02/ Steel design. SA516-70				
B03 Any appl. requirements		ASME-II-A:07+A09 DIL-HUE-3:R29-2010-01-31		

C70-C99 Chemical composition % - Product analysis

B07.2 Heat	B07.1 Test No.	C01			
		B	CA	AL-T	
344655	30836	K1 0,0001	0,0014	0,030	
344657	28431	K1 0,0000	0,0014	0,027	
344659	23555	K1 0,0001	0,0012	0,034	

C94 Product analysis Carbon equivalent / Alloying restrictions

B07.2 Heat	B07.1 Test No.	C01			
		FO-02=	FO-51=	FO-55=	
344652	32213	K1 0,0001	0,0001	0,001	0,08
344652	32216	K1 0,0001	0,0001	0,000	0,09
344653	30844	K1 0,0001	0,0001	0,001	0,09
344653	30846	K1 0,0001	0,0001	0,001	0,10
344653	32208	K1 0,0001	0,0001	0,000	0,08
344653	32209	K1 0,0001	0,0001	0,000	0,09
344655	28434	K1 0,0001	0,0001	0,000	0,10
344655	28435	K1 0,0001	0,0001	0,001	0,09
344655	30836	K1 0,0001	0,0001	0,000	0,10
344657	28431	K1 0,0001	0,0001	0,000	0,10
344659	23555	K1 0,0001	0,001	0,001	0,25

C94 Carbon equivalent formula / Alloying restrictions

FO-02 = $C + (Mn/6) + (Cr+Mo+V)/5 + (Ni+Cu)/15$	
FO-51 = V + Nb	
FO-55 = $Cu+Mo+Ni+Cr$	
FO-78 = $Cr+Mo$	
FO-91 = Mn/C	

A04	Z01/Z02/Z03 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order.	AG der Dillinger Hüttenwerke Postfach 1880, D-66748 Dillingen/Saar Inspection department	A01
		ADB	
QM-System: Certification as per ISO 9001		Inspector's stamp Date 14.05.10	BM
Manufacturer's mark		Test House Manager B. MUELLER	



DILLINGER HÜTTE

Erläuterungen siehe Rückseite/Explications voir au verso/See reverse for explanations (www.dillinger.de/certificate)

A02 INSPECTION CERTIFICATE 3.1 AS PER EN 10204:2004		A10 Advice of dispatch No./ Date of dispatch		A03 Manufacturer's order/ A03 Certificate No.	Sheet
INSPECTION CERTIFICATE 3.1.B AS PER EN 10204:1991+A1:1995 + AS PER ISO 10474:1991		360093-14.05.10		354135-003	9
MATERIAL TEST REPORT (MTR)					
A05 Established inspecting body	A06 Purchaser	EDMONTON STEEL, EDMON		A07.1 No.	ED10548-J1010-ER
DH	Final receiver	EDMONTON STEEL, EDMON		A07.2 No.	
B02 Steel design.		SA20-S5			
B03 Any suppl. requirements		DIL-HUB-3:R29-2010-01-31			

D01 Marking and identification, surface appearance, shape and dimensional properties

ITEM NO.: 01-06
RESULT OF MARKING, SURFACE, SHAPE AND DIMENSIONS: NO REMARKS
SURFACE AS PER ASME-SA20
THICKNESS AS PER ASME-SA20
LENGTH AND WIDTH AS PER ASME-SA20
FLATNESS AS PER 1/2-ASME-SA20



A04	Z01/202/203 We hereby certify, that the above mentioned materials have been delivered in accordance with the terms of order. QM-System: Certification as per ISO 9001	3. pin	AG der Dillinger Hüttenwerke Postfach 1500, D-66748 Dillingen/Saar Inspection department	Inspector's stamp	Date	14.05.10	BM	1
		B. MOELLER Test House Manager		A03				

THESE ARE THE BEST

THEIR SAYS STEEL

TUBULAR PRODUCTS

CERTIFIED TEST REPORT
IN ACCORDANCE WITH ISO 10474/EN10204/DIN50049 "Type 3.1"

DATE: 06/01/12
TIME: 04:13:55
SERIAL NO: L0041424

[illegible]

DECIMAL POSITIONS FOR ELEMENTS ARE INDICATED BY THE LEFT MARGIN.		VERTICAL GOFFED LINE AND DECIMAL POINT PLACEMENTS REPORTED IN MASS FRACTION (%)	
		PAGE	1 OF 2

DATE: DEC. 11/12
SIGNATURE: *[Signature]*
MIN. THICK.: .514"; .520"

CONFORMS TO 2010 EDITION: 2011 ADDENDA





UNITED STATES STEEL

TUBULAR PRODUCTS

CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 18474/EN10204/MS0049 "type 3.1")

DATE: 06/01/12
TIME: 04:13:55
SERIAL NO: L0041424

BILL OF MATERIALS NO. D04533 01		SHIPPER NO.		P.O. NUMBER 118913-00		G.D. 24,000 (609.600)		WALL 0.500 (12.700)		IN (mm)						
MATERIAL CONC: FULL BODY NORMALIZED										IN (mm)						
PRODUCT IDENTIFICATION	FLAT	BOND	GRAIN SIZE	BIM COLLAPSE	DNR	TEST LOC.	TEMP	SIZE	CHARPY V-NOTCH IMPACT TESTING FT/LBS			% SHEAR				
									1	2	3	AVG	1	2	3	AVG
KA3971 X138NA	OK								166	211	153	176	80	100	80	86
					** END OF DATA THIS SHEET **											
LEGEND					1. TRANSVERSE		8. BODY		W. WELD		HAZ. HEAT AFFECTED ZONE					
TEST / INSPECTION					YES		RESULTS / COMMENTS									
FULL LENGTH VISUAL					X											
FULL LENGTH EAM					X											
FULL LENGTH MPI																
FULL LENGTH UT																
END AREA INSPECTION (PLAIN END)																
SPECIAL END AREA (SEAM INSP)																
FULL LENGTH DRIFT																
ADDITIONAL NOTES/COMMENTS																
MELTED AND MANUFACTURED IN THE USA. NO REPAIRS BY WELDING. NO MERCURY OR MERCURY COMPOUNDS ARE ADDED TO THE STEEL AND ALL MERCURY BEARING EQUIPMENT IS PROTECTED BY A DOUBLE BOUNDARY OF CONTAINMENT.																

FEDERAL STEEL SUPPLY
QA APPROVED
BY MB
DATE 10/25/12

THIS IS TO CERTIFY THAT THE PRODUCT DESCRIBED HEREIN WAS MANUFACTURED, SAMPLED, TESTED AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION AND FULFILLS THE REQUIREMENTS IN SUCH RESPECTS.

PREPARED BY THE OFFICE OF: R. HARRIS - MANAGER, Q.A.

DATE 06/01/12

12-0719 2 FLANGES



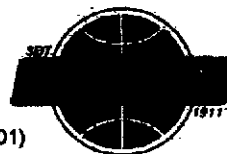
EN ISO 9001 : 2008

Zertifikat-Registrier-Nr.
44 100 071888

BEBITZ

Bereich Flansche / Flange Division

Flanschenwerk Bebitz GmbH - Lebendorfer Str. 1 - 06420 Bebitz / GERMANY (A01)
Tel. +49 34691 40 0 - Fax +49 3469140 329 - Email: flanges@bebitz.de



Abnahmeprüfzeugnis 3.1 / Inspection certificate 3.1 / Certificat de reception 3.1

nach (A02) / acc. DIN EN 10204 : 2005 Nr. (A03) / No.12-18377 Datum (Z02) / Date 21.08.2012

Zeichen des Herstellers (A04)
Manufacturer's brand



Stempel des Abnehmers (Z03)
Stamp of the testing engineer



Überprüft als Hersteller nach AD-Merkblatt W0 / TRD100 und VdTÜV Werkstoffblätter 350/3, 354, 399. / Approved as manufacturer acc. AD-Merkblatt W0 / TRD100 and VdTÜV Material Sheets 350/3, 354, 399.
Zertifiziert nach DGR 97/23/EG durch TÜV CERT Zertifizierungsst. für Druckgeräte der TÜV NORD GmbH Co KG, Benannte Stelle Nr. 0045. / Certified acc. to PED 97/23/EC, certifying body for pressure equipment TÜV NORD GmbH Co KG, registration no. 0045.

Besteller TRANS AM Piping Products Ltd.
(A06) 9335 Endeavor Drive S.E.
Customer CALGARY, ALBERTA T3S 0A1

Bestell-Nr (A07) / Order-No. CI-12-302
Auftrag (A08) / Order 3220838
Lieferschein / Delivery No. 3233736
Position (B07.1) / Item 6

Stück (B08) Bezeichnung (B01; B09 - B11)
Quantity Product

5 24 inch Welding Neck Flange 300 lbs XS raised face

Schmelze/Prüflos (B07)
Heat no./Test no.

H0742/3

Material LF2 Class 1 - ASTM A 350M-07 / ASME SA-350M
(B02; B05) forged 1050 - 1150°C / normalized 898 - 925°C, still air

Anford. ASME B 16.5-2009

(B03) NACE MR0175-2011 / MR0103-2010 - DIN EN ISO 15156-2 : 2009

Requirements 2011a ASME Boiler & Pressure Vessel Code - Section II Part A

Schmelzenanalyse (C71 - C92) / Ladle analysis

Erschmelzung (C70) / Melting process E

≤ 0.32 ✓
≤ 1.00 ✓

C	Si	Mn	P	S	Cr	Ni	Ti	Mo	Nb	V	N	Cu	Al	CEV
0,180	0,23	1,12	0,010	0,004	0,15	0,08	0,001	0,02	0,003	0,015		0,11	0,024	0,42

$$CEV = C + \frac{Mn}{6} + \frac{V + Mo + Cr}{5} + \frac{Ni + Cu}{15} \quad PREN = Cr + 3,3 \times Mo + 16 \times N$$

Mechanische Prüfungen / Mechanical tests

Probenlage (C02): q/t / Position of Specimen: q/t Zugversuch / Tensile Test - ASTM A 370						l ₀ = 4 d ₀	KBV / Charpy Impact Test DIN EN ISO 148-1			Härte (C32) Hardness ISO 6506-1
Temp (C03) ° C	Streckgr. (C11) / Yield strength 0,2% 1,0% MPa (N/mm²) MPa (N/mm²)		Zugfestigk. (C12) Tensile strength MPa (N/mm²)	Dehng. (C13) Elongation %	Einschnürrg. Red. of area %	Temp. (C03) ° C	Einzelwerte (C42) Single values J	MW (C43) Average J	HBW 2,5/187,5	
20	min 250		485	22,0	30	-46	20	27	137	
	max		655						187	
20	326✓		509✓	33,7✓	73✓	-50✓	140✓ 121✓ 110✓	123,7✓	153	
20	323✓		507✓	34,2✓	74✓	-50✓	114✓ 143✓ 126✓	123,7✓	150	
ASME SECTION II BY CALHEX INDUSTRIES LTD.										

CONFORMS TO 2010 EDITION: 2011 ADDENDA

DATE: DEC. 11/12

SIGNATURE: [Signature]

MIN. THK.:



Besichtigung und Ausmessung ohne Beanstandungen. (D01) / Results of inspection and dimension without objections.

Die gestellten Anforderungen sind erfüllt. (Z01) / The product meets the requirements.

R. Sparing,

Abnahmebeauftragter des Herstellers (Z02)

Inspection Representative of the Manufacturer

APZ wurde mit EDV erstellt und ist ohne Unterschrift gültig. /

This MTR was electronically generated and is valid without a signature.

Angaben in Klammern entsprechen den Vorgaben der DIN EN 10168 /
Data in parentheses refer to EN 10168.

24" CL 300 BLIND FLANGE RF

SAN ENG STEEL FORGING CO LTD
311, Jen Hsin Road, Jen Wu District
Kaohsiung, Taiwan, R.O.C.
TEL: 07-3724249 ; FAX: 07-3712823
URL: www.saneng.com.tw
e-mail: saneng@mts.seed.net.tw



MULTI-TEST CERTIFICATION

EN10204-3 1 B/DYN50049/3.1.B)

Customer TRANSAM PIPING PRODUCTS LTD.

Order No: 7005889(1)-T/A

Certificate No.: SE-5689A
Date: 08/31/2012
Page: 1 OF 1

URL: www.seahng.com.tw
e-mail: seahng@seahng.com.tw

Order No.: 7005888(1)-1/A

MATERIAL SPECIFICATIONS

DIMENSIONAL SPECIFICATIONS

PRODUCT

ASME B16.5-08
CSA Z245.12

ASTM A350 LF2-11 CL.1/ASME SA350 LF2-11 CL.1

FORGED CARBON STEEL FLANGES

Item No.	CODE NO	DESCRIPTION	QUANTITY	CHEMICAL COMPOSITION (%)	CE(*)								
C	Si	Mn	P	S	Cu	Ni	Mo	V	Nb	N			
Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
12 PCE	0.300	0.150	0.600	0.035	0.040	0.400	0.120	0.080	0.020	-	-	-	-
5 PCE	0.200	0.210	1.130	0.018	0.007	0.180	0.120	0.100	0.001	0.008	0.430	0.436	0.433
18 PCE	0.210	0.190	1.140	0.018	0.006	0.138	0.080	0.060	0.002	0.005	0.430	0.436	0.433

HEAT TREATMENT(°C)

□ N

Material Supplier

Impact Test
Temp: -46°C
Minimum: 20.0 Joule

RA(%)

Hardness
(HB)

E.L.(%)

Y.S.(MPa)

T.S.(MPa)

Heat No.

REMARKS
980 °CX3HRS
CONFORMS WITH NACE MR0103-10 AND NACE
MR0175/ISO15156 2-09
CONFORMS WITH 2245.12 CAT II OR 248 SOUR
SERVICE-OK FOR USE AS WELDING NECK AND
BLIND FLANGES ONLY
TEST SPECIMEN SIZE: 10X10
TEST SPECIMEN ORIENTATION: TRANSVERSE
IMPACT TEST TEMP: -46°C

*1: T.S. = Tensile Strength, Y.S. = Yield Strength, E.L. = Elongation, R.A. = Reduction of Area.

*2: N=Normalized, A=Annealed, Q=Quenched, T=Tempered, S=T-Solution Treated, S R=Stress Relieved, A.C=Air Cooled, F.C=Furnace Cooled, W.C=Water Cooled, O.C=Oil Cooled.

*3: C.E. Value = C + (Mn / 8) + (Cr + Mo + V) / 5 + (Ni + Cu) / 15

We hereby certify that the material has been tested in accordance with the above specification and also with the requirements called for by the above order.

Manager of Quality Assurance Dept

the money, serving the community, and the requirements called for by the above order.

MATERIAL CHECKED TO
ASME SECTION II BY
CAL HEX INDUSTRIES LTD.

DATE DEC. 11/12

2010-2011 FISCAL YEAR: ALL APPENDICES



ESSAR Steel Alloys Inc.

105 West Street, Sault Ste. Marie, Ontario Canada P6A 7B4

FALL ORDER
19992

-317404

CP

284093 -

2012/06/27

011/04/24

2

CHANGE TO SUBSECTION 1002.202 AND A

WILKINSON STEEL AND METALS INC.
9525-60TH AVENUE
EDMONTON ALBERTA
T6E 0C3

WILKINSON STEEL AND METALS INC.
C/O BATES EQUIPMENT
99525 60TH AVENUE
EDMONTON, ALBERTA T6E 0C3

WILL TEST REPORTS

ESBAR STEEL ALGOMA INC. HEREBY CERTIFIES THAT THE MATERIAL HEREIN DESCRIBED WAS MADE AND TESTED IN ACCORDANCE WITH THE RULES OF THE SPECIFICATION SHOWING ALL RESULTS HAVE BEEN OBTAINED IN ACCORDANCE WITH THE COMPANY'S STANDARD RECORD KEEPING PRACTICES.

COLLECTING NEW LITERATURE

K. UCHADPAGA

TEST CERT 1: CSTEPANIUKAWILKINSONSTEEL.COM TEST CERT 2: MEL ELI
ASAS 604-301-3244 PLATE TEST COUPON:

THIS WILL TEST REPORT MAY NOT BE
REPRODUCED EXCEPT IN FULL WITHOUT
WRITTEN APPROVAL OF ESSAR STEEL
MANAGEMENT. IF YOU RECEIVE THIS
DOCUMENT AND ARE NOT THE INTENDED
RECIPIENT, PLEASE CALL (708) 945-2624
TO COLLECT FOR INSTRUCTIONS ON METHOD
OF DISPOSAL OF DOCUMENT.

UNIT 1A TEST REPORTS REQUIRED

2000229923 PF

2012/07/01 12:55

IMPACT TESTS:

PLATE	HEAT NUMBER	SRC#	GAUGE IN	** ** *	COND	METH	DIR	TEST	SIZE	TEMP	** ** *	FULLSIZE	ENERGY
	5699M 01115	166"	3750	N	CVN	L	3/4	-50F	101	92	84	92	
	5699M 01116	166"	3750	N	CVN	L	3/4	-50F	85	101	102	96	

SPEC LAB
ASTM ALC
ASTM ALC

THEAT (MT 8)

HEAT	(WT %)	C	MN	P	S	SI	CR	NI	CU	MO	AL	CB	V	B	DO
5699M+		21	1.08	.011	.007	.29	.02	.02	.04	.00	.032	.000	.001	.0002	.40

≤ 0.32 ✓
 ≤ 1.00 ✓

THE TEST RESULTS AND VALUES REPORTED HEREIN INDICATE ONLY THAT (1) THE PARTICULAR STEEL FOR WHICH THIS CERTIFICATE IS ISSUED MEETS THE MINIMUM SPECIFIED YIELD STRENGTH AND (2) THE CHEMICAL ANALYSIS AND PHYSICAL PROPERTIES OF SUCH STEEL ARE IN CONFORMANCE WITH THE REQUIREMENTS OF THE SPECIFICATION INDICATED. THE RESULTS OR VALUES REPORTED HEREIN CAN NOT BE USED TO QUALIFY THE STEEL FOR ANY SPECIFICATION OTHER THAN THE ONE INDICATED AND CAN NOT BE RELIED UPON FOR ANY PURPOSE INCLUDING DESIGN OR CALCULATIONS AS REPRESENTING THE ACTUAL STRENGTH OF SUCH STEEL.

8" S/80 ASTM A/SA 333-6 HT. 268216



Austraße 25, 52249 Eschweiler
 Telefon 0 24 03 / 7 92 - 181 Verkauf - 275 Qualitätsstelle
 Telefax 0 24 03 / 7 92 - 180 Verkauf - 270 Qualitätsstelle

Anlage/Enclosure/Annexe N°: 1
 Werks-Nr./Our Order No.:
 N° Cde Usine: 354721 002 0 01

Prüfergebnis/Test results/Résultat des essais

Besichtigung und Ausmessung/
 results of inspection and measurement/
 Contrôle aspect et dimensions:

O. B. /OK/ SATISFAISANT

Ringaufdehnversuch/Ring expanding test/
 Essai d'anneau (traction):

Ringzugversuch/Ring tensile test/
 Essai d'anneau (évasement):

Ringflattversuch/Flattening test/
 Essai d'aplatissement:

O. B. /OK/ SATISFAISANT

Aufweitversuch/Flaring test/
 Essai d'évasement:

Drilltest/Drifttest/Contrôle de Mandrin:

Schmelzen-Nr./ Cast-No. N° Cousse	Rohr-Nr. Test-No. N° d'essai	Streckgrenze/ Yield stress/ Limite élastique R _e N/mm ²	Zugfestigkeit/ Tensile strength/ Résistance R _m N/mm ²	Bruch- dehnung/ Elongation/ Allongement A ₂ II %	beVal./ °C	Kerbschlagarbeit/Impact Value/ Essai de flexion par choc Joule			Mittel/ Average/ Moyen	Probe/Type/ Type:
						1.	2.	3.		
		290- 495	415- 625	MIN. 30	-45				27	ISO-V
268216		302 ✓ 307 ✓	448 ✓ 447 ✓	34 ✓ 36 ✓	-45 ✓ -45 ✓	147 ✓ 140 ✓	138 ✓ 142 ✓	155 ✓ 152 ✓	142 ✓ 145 ✓	

Technical requirements: * + ISO 15156-1/03 + ISO 15156-2/03*. The material conforms with NACE MR 0103. Hardness acc. to NACE MR 0175/03 max. 22 HRC.
 Test Pressure 207 bar is equivalent to 20,7 mpa.

ESW Röhrenwerke GmbH
 Eschweiler

ESCHWEILER, DEN 20.10.2006

Eschweiler, den

DIESES ZEUGNIS IST MASCHINELL ERSTELLT UND WIRD NICHT UNTERSCHRIEBEN

GEZ. DREXLER

Der Abnahmebeauftragte
 Work's Inspector
 L'expert d'usine

Bankkonto:
 Sparkasse Aachen,
 Konto-Nr.: 3 100 55
 BLZ 390 500 00
 USt-IdNr.: DE 121732288

Geschäftsführer:
 Dipl.-Betriebswirt Herbert Lenzen,
 Aufsichtsratsvorsitzender:
 Manfred Leiss
 Amtsgericht Aachen HRB 11392

Web: www.esw-rohre.de
 Mail: info@esw-rohre.de
 vertrieb@esw-rohre.de
 qualitaet@esw-rohre.de

Anlage zum Abnahmezeugnis des Auftrags/Enclosure to inspection certificate by Order-No.: 354721 002

Stahlsorte: Gr.6/Gr.290 Cat II

Schmelzen-Nr.: 268216

Schmelzenanalyse / Heat analysis / Analyse sur coulée [%]

	C	Si	Mn	P	S	Cr	Cu	Al	Mo	V	As	Sn	Nb	Ti	N	
268216	0,16	0,24	0,82	0,020	0,002	0,028	0,02		0,01	0,001	0,002	0,001	0,001	0,005	0,0040	
Check 1	0,17	0,22	0,85	0,017	0,001	0,030	0,02		0,02	0,002	0,002	0,004	0,002	0,003	0,0050	

ESW Röhrenwerke GmbH
Qualitätsstelle

CERTIFICATE OF COMPLIANCE

BRINNEL HARDNESS TEST RESULTS
PIN BRINNEL TESTER TO NACE MR0175

<u>Heat</u>	<u>Description</u>	<u>BHN</u>
268216	8" 5/80 (.500") SMLS ASTM /ASME A/SA-333 GR 6	125

Operator

Date:


RALPH GPETZ

November 18, 2008

SSAB

1/4" SA 516 702

HT # W2H505
PC # D01

Y571 Oct 12

Test Certificate

12400 Highway 43 North, Axis, Alabama 36505

Form TC1: Revision 1: Date 31 Oct 2000

Customer: SAMUEL & SON LIMITED (A DIVISION OF SAMUEL SALES) 2340 DIXIE ROAD MISSISSAUGA ON L4Y1Z7		Customer P.O. No.: U91205 & 41-337110		Mill Order No.: 41-337111-01		Shipping Manifest: AR145797	
Product Description: ASTM A516-70(10)/ASME SA516-70(11A) NACE MR0175 ANNEX A2.1.2 COMPLIANT LCVN 20 FT-LBS @ .50W/A673-P NORMALIZED		Ship Date: 04 Sep 12		Cert No: 681348938		(Page 1 of 1)	
Size: 0.250 X 120.0 X 480.0 (IN)							

Tested Pieces				Test Results				Chemical Analysis				Charpy Impact Tests				BDWTT			
Heat Id	Piece Id	Tested Thickness	YS (KSI)	UTS (KSI)	%RA	Elong %	2in 8in Dir	Average Hardness	Abs. Energy (FTLB)	% Shock	Tst Temp	Tst Dir	Tst Size	Tst Temp	Tst Dir	Tst Size	BDWTT Temp	% Shar	
E2H127	B08	0.246 (DISCRT)	56	77		29	T	165 HBW	36	38	37	37		50F	L	5.0			
W2H505	D01	0.251 (DISCRT)	54	75		23	T	159 HBW	52	47	34	38		50F	L	5.0			

Heat Id	C	Ma	P	S	Si	Mn	Al	Se	Al	Cu	Mo	Cr	Ni	Co	V	Ti	B	CEV	ORGN	
E2H127	.18	1.12	.010	.001	.20	.025	.024	.29	.14	.07	.07	.07	.14	.07	.002	.006	.007	.0000	.42	USA
W2H505	.18	1.12	.008	.002	.20	.027	.026	.26	.13	.10	.03	.10	.13	.03	.003	.006	.008	.0000	.42	USA

MERCURY IS NOT A METALLURGICAL COMPONENT OF THE STEEL AND NO MERCURY WAS INTENTIONALLY ADDED DURING THE MANUFACTURE OF THIS PRODUCT

KILLED STEEL, PRODUCED TO A FINE GRAIN PRACTICE

CEV (IIV) = C + MN/6 + (CR+MO+V)/5 + (NI+CU)/15

MTR EN 10204:2004 INSPECTION CERTIFICATE 3.1 COMPLIANT

CHARPY FULL SIZE EQUIVALENT = ABSORBED ENERGY AVG X 10 / TEST SIZE IN MM

NORMALIZED PLATES. HEATED AT 1665F FOR 15 MINUTES.

TEST COUPONS TAKEN FROM HEAT TREATED PLATE.

PRODUCTS SHIPPED:

W2H505 D01	6366524	PCES: 1, WGT: 4178	W2H505 D01	6366523	PCES: 1, WGT: 4178
W2H505 D01	6366521	PCES: 1, WGT: 4177	W2H505 D01	6366519	PCES: 1, WGT: 4177
W2H505 D01	6366518	PCES: 1, WGT: 4177	W2H505 D01	6366517	PCES: 1, WGT: 4178
E2H127 B08	6368185	PCES: 1, WGT: 4084	E2H127 B08	6368184	PCES: 1, WGT: 4080
E2H127 B08	6368186	PCES: 1, WGT: 4080	E2H127 B08	6368182	PCES: 1, WGT: 4082

MATERIAL CHECKED TO
ASME SECTION II BY
CALHEX INDUSTRIES LTD.

DATE: DEC. 11/12

SIGNATURE: *[Signature]*

MIN. THK.: .247", .245", .245", .245"

JOB # 12-0779
HEAT CODE # 8998
(W2H505-D01)

CONFORMS TO 2010 EDITION: 2011 ADDENDA



Cust Part #:

WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION

Justin Ward
SENIOR METALLURGIST - PRODUCT







SPECTRUM N.D.T. LTD

ULTRASONIC TEST REPORT

Client CALHEX Industries	JOB # 12-0779	Report # 140469				
	SER # N/A	Work Sheet # 31434				
Address Calgary, Alberta	Requested by Mr. A. Benns	Demo # 1018				
		Procedure# UP4 Rev. 1				
Work Description Inspection of Repad Splices weldments	Code ASME V Art. 4	Acceptance criteria ASME VIII Div.1, App.12				
Material / Thickness Carbon Steel, 1/4" Thk.	Surface Condition As Ground	Temperature 18 °C				
Instrument GE	Model USN 58L	Serial # 020L7T				
Sensitivity 3/32" Diameter SDH set at 80% FSH DAC	Couplant UT-X	Inspector K. Han				
Search Unit	Serial Number	Size	Ref Sensitivity	Scan Sensitivity		
0 Deg. 2.25 Mhz GAMMA	022877	1.0" Diameter	BWE 80%	+6 dB		
70 Deg. 4 Mhz Phoenix	B8304	10mm Diameter	80% FSH DAC	+ 6 dB		
60 Deg. 4 Mhz Phoenix	C3932	10mm Diameter	80% FSH DAC	+ 6 dB		
45 Deg. 4 Mhz Phoenix	C4883	10mm Diameter	80% FSH DAC	+ 6 dB		
Identification	Description	Result				
12-0779	Inspected Repad Splices welds L1 & L2 on nozzles: N1, N2, N3, N4	- ACCEPTABLE -				
Ind #	Depth (inch)	Length (inch)	Amplitude (dB)	Probe(s)	Remarks	Classification
A = Acceptable minor non reportable indication B = Acceptable reportable indication C = Rejectable indication						
Reg Hrs 2.0	OT1 Hrs	OT2 Hrs	Consumables			
CHANGES, MODIFICATIONS, ALTERATIONS OR ADDITIONAL WELDING WITHOUT RE-INSPECTION VOIDS REPORT.						
CLIENT 	INSPECTOR 	LEVEL CGSB L2 #16012 / ASNT L3 #148347	DATE Dec 12, 2012			



Radiographic Inspection Report

A circular stamp with a thick black border. Inside the circle, the letter 'M' is prominently displayed in a bold, serif font. Below the 'M', the text 'CATS 208' is written in a smaller, sans-serif font. There are some handwritten marks or scribbles below the text.

SPECTRUM NDT LTD.

Radiographic Inspection Report

RR #: 54530

CLIENT: Calhex

JOB LOCATION: Calgary, AB

JOB #: 12-0779

P.O. #: _____ DATE: Nov 20/12

ISOTOPE: IR¹⁹² FILM: GAVERT D4 ☐
 FILM/CASS: 1 D5 ☒
 TECH #1 D7 ☐
 EFSS: 3.5mm± OTHER: _____

CODE: UW51 ☐
 UW52 ☒
 B31.3 ☒ ☐ SC
 OTHER ☐

MATERIAL: ☒ CS ☐ SS
 VEIING ☒ SW ☒ EXPOSURE
☐ DW ☒

ABBREVIATIONS: (LEGEND)

IF - INCOMPLETE FUSION
 IP - INCOMPLETE PENETRATION
 S - SLAG

P - POROSITY
 I - ICICLES
 UC - UNDERCUT

BT - BURN THROUGH
 C - CRATER
 HL - HIGH-LOW

LC - LOW COVER
 CR - CRACK

FILM NO.	LOCATION	IF	IP	S	P	I	UC	BT	C	LC	CR	OK	REJ	REMARKS	SFD	DIA.	SOD	MSSOFD	THICK	# EXP	WS
C45	0-8											✓			12"	24"	11.5		0.5	1	G
N15	0-8				1							✓			9	8	8.5		0.5	1	A
N25	0-8											✓			↓	↓	↓		↓	↓	A
N45	0-8								2			✓			↓	↓	↓		↓	↓	A

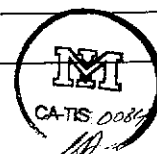
INSPECTOR: Steve Wolfe *[Signature]*

CLIENT REPRESENTATIVE: *[Signature]*

FINAL INTERPRETATION OF RADIOGRAPHS SHALL BE THE RESPONSIBILITY OF THE CLIENT OR THEIR REPRESENTATIVE.

ASNT II ☐
 ASNT III ☐
 CGSB II ☒ 13808

COMMENTS:



Radiographic Inspection Report



Lincoln Electric of Canada LP
179 Wicksteed Ave.
Toronto, ON M4G 2B9

CERTIFIED MATERIAL TEST REPORT**LINCOLN
ELECTRIC**

Product:	SUPERARC L-56	Size:	0.035" (0.9 mm)
Classification:	ER 70S-6	Q3 Lot No.:	12829712
Specification:	AWS A5.18	Heat No.:	C88620
Date Completed:	MARCH 23, 2012	Stock No.:	ED561008PIPE (44 lb. fibre spool)

This is to certify that SUPERARC L-56, Q3 Lot number 12829712, was tested using the GMAW process in accordance with the specification named above and concluded on the date shown, the results of which are shown below. The welding procedures and gas used are shown below. Mechanical properties and chemical results are taken from weld deposits in the as welded condition. This material was manufactured and supplied according to the Quality System Program of Lincoln Electric Company of Canada, Toronto, Ontario, which meets the requirements of ISO 9001:2008 and other specifications applicable. This material was manufactured under one lot control number and meets the requirements of AWS A5.01 Lot Classification Class S3.

Shielding Gas:75% Ar/25% CO₂, 45 CFHOperating Settings:

Wire Feed Speed (in/min)	600
Voltage, DC+ (volts)	27
Travel Speed (in/min)	12 - 14
Electrical Stickout (in)	3/4
Layers/Passes	6/16
Interpass Temperature (°F)	325

Tensile Properties:

Tensile Strength (psi)	87 890
Yield Strength (psi)	74 080
Elongation (%)	29

Impact properties, Charpy V-notch:

Average ft-lbs at -55°F

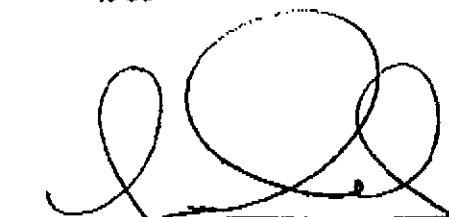
77
(79, 76, 75)Electrode Analysis:

% C	0.07
% Mn	1.46
% Si	0.85
% S	0.006
% P	0.005
% Cu (Total)	0.11

Weld Deposit Analysis:

% C	0.07
% Mn	1.25
% Si	0.69
% S	0.009
% P	0.004
% Cu	0.19


Technologist - Production Testing and
Certification


Quality Assurance Manager,
Consumables Division

October 30, 2012

Attention: Document Control
CALHEX INDUSTRIES LTD
9515-48 STREET SE
CALGARY, AB T2C 2R1

The design submission, tracking number 2012-07234, originally received on October 19, 2012 was surveyed and accepted for registration as follows:

CRN : V9688.2

Accepted on: October 30, 2012

Reg Type: New Design

Drawing No. : 12-0779-S/T Rev 0 As Noted

Description	MAWP	Design Temperature	MDMT
TS Internal Pressure	2758 kPa	70 ^o C	-45 ^o C
TS External Pressure	103 kPa	70 ^o C	-45 ^o C
SS Internal Pressure	2758 kPa	70 ^o C	-45 ^o C
SS External Pressure	103 kPa	70 ^o C	-45 ^o C

An invoice covering survey and registration fees will be forwarded from our Revenue Accounts.

If you have any question don't hesitate to contact me by phone at (780) 433-0281 ext 3335 or fax (780) 437-7787 or e-mail dedovic@absa.ca.

Sincerely,



DEDOVIC, BLAZO



CALHEX INDUSTRIES LTD
9515 48TH STREET SE
CALGARY AB T2C 2R1

Date: November 28, 2012
Account #: 39806
Journal #: 56001
Our File #: 5309600

Attn: DARREN KLADNIK

Re: Application for Design Registration

The design, as detailed in your, Ref: 12-0779, for a Heat Exchanger is accepted for registration as follows:

Registered To: CALHEX INDUSTRIES LTD CRN: V9688.21

Shell Side MDMT: -49 deg F

MAWT: 158 deg F

MAWP: 400 psig

Tube Side MDMT: -49 deg F

MAWT: 158 deg F

MAWP: 400 psig

Drawing #: 12-0779-S, 12-0779-T

Drawing Revision: 0 / 0

Conditions Of Registration:

1- Shell Side and Tube Side also designed for Full Vacuum @ 158 deg F.

	<u>Amount</u>	<u>HST</u>	<u>Total</u>
Fee for reviewing your design:	\$148.00	\$17.76	\$165.76
Total:	\$148.00	\$17.76	\$165.76
Less amount received with submission:			\$0.00
			\$165.76

An invoice for \$165.76 will follow.

Contact me if you have any questions.

ALIREZA BONAKDAR
(778) 396-2032
Alireza.Bonakdar@safetyauthority.ca
Design Engineer

cc:

Calhex Industries

Ltd.

Welding Procedures

Welding Procedure:

CX-1N

Rev. 4

March 26, 2008

Sheldon Alcock
CALHEX INDUSTRIES LTD
9515-48 STREET SE
CALGARY, AB T2C 2R1

Dear Sheldon Alcock,

The welding procedures received on March 17, 2008 are accepted for registration as follows:

Reg. No. : WP-2380.2

Accepted on: March 26, 2008

Tracking No. : 2008-01881

Reg Type : Revision To Acc. Design

Spec. No. : CX-1N REV 4

Registered under owner / manufacturer name CALHEX INDUSTRIES LTD

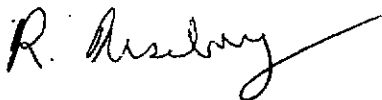
Please note the acceptance of the registration does not allow the use of this welding procedure in the construction, modification, or repair of any boiler, pressure vessel, pressure piping system or fitting in Alberta unless the contractor/manufacturer has registered a Quality Control system for such work with ABSA.

Welding procedures, which specify impact testing, have been accepted in accordance with A.S.M.E. Section IX only. Other A.S.M.E. Code Sections may have additional requirements respecting impact testing.

An invoice covering survey and registration fees will be forwarded from our Revenue Accounts.

Enclosed is a stamped welding procedure for your reference.

Sincerely,



ROSEBERG, BOB, P. Eng.
Design Survey Engineer

original

WELDING PROCEDURE SPECIFICATION NO.: CX-1N (Rev. 4)

WELDING PROCEDURE QUALIFICATION RECORD NO.(S): PQ1, PQ3, PQ16, PQ31, PQ32

QUALIFIED FOR

Base Metal (Typical): P1 Groups 1 & 2 to P1 Groups 1 & 2
(SA 333 Gr. 6, SA 350 Gr. LF2, SA 420 WPL6, SA 516 Gr. 70, etc.)
Process(es): GMAW / SMAW Weld Types: GROOVE & FILLET
Position: ALL POSITIONS Diameter: ALL DIAMETERS
Filler Metal: GMAW: ER70S-2 or 6 SMAW: E7018-1

BASE METAL CONDITIONS & GROOVE THICKNESS RANGE QUALIFIED:

NOTCH TOUGHNESS APPLICATIONS TO -46°C AS WELDED

BASE METAL THICKNESS RANGE 3.0 to 203 mm (0.119 to 8.00 in.) inclusive

COMBINED DEPOSITED WELD METAL THICKNESS

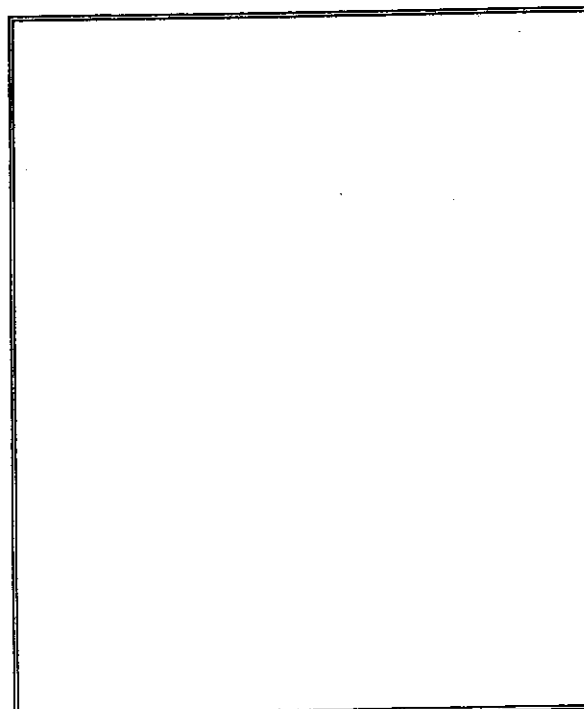
ASME B31.1 19.1 mm (0.750 in.) maximum
ASME B31.3 19.1 mm (0.750 in.) maximum
ASME SECT. VIII, DIV.1 38.1 mm (1.50 in.) maximum

ALBERTA BOILERS SAFETY ASSOCIATION
PROVINCE OF ALBERTA
SAFETY CODES ACT
WELDING PROCEDURE

Reg. No. WP 2380.2
Spec No. CX-1N (REV. 4)
Weld Process GMAW / SMAW
Matl. Gr. P No. 1 Gr. 1+2 to P No. 1 Gr. 1+2
Elec. Gr. F No. 6+4 A No. 1
Th. Qual. For 3 to 203 mm PWHT NO
CVN -46°C

Yr. 08 Mo. 03 Day 26 Signed R. ROSEBERG, P.ENG.
WELDING SPECIALIST

PROVINCIAL REGISTRATION



Calhex Industries
Ltd.

Welding Procedures

Welding Procedure:

CX-2N

Rev. 1



#200, 4208 - 97 Street
Edmonton, Alberta, Canada T6E 5Z9
Tel: (780) 437-9100 / Fax: (780) 437-7787

September 01, 2005

Sheldon Alcock
CALHEX INDUSTRIES LTD
9515 48 STREET SE
CALGARY, AB T2C 2R1

Dear Sheldon Alcock,

The welding procedures received on August 18, 2005 are accepted for registration as follows:

Reg. No. : WP-2380.2

Accepted on: September 01, 2005

Tracking No. : 2005-06606

Reg Type : Revision To Acc. Design

Spec. No. : CX-2N REV 1

Registered under owner / manufacturer name CALHEX INDUSTRIES LTD

Please note the acceptance of the registration does not allow the use of this welding procedure in the construction, modification, or repair of any boiler, pressure vessel, pressure piping system or fitting in Alberta unless the contractor/manufacturer has registered a Quality Control system for such work with ABSA.

Welding procedures, which specify impact testing, have been accepted in accordance with A.S.M.E. Section IX only. Other A.S.M.E. Code Sections may have additional requirements respecting impact testing.

An invoice covering survey and registration fees will be forwarded from our Revenue Accounts.

Enclosed is a stamped welding procedure for your reference.

Sincerely,

A handwritten signature in black ink, appearing to read 'R. Roseberg', with a long, sweeping horizontal stroke extending to the right.

ROSEBERG, BOB, P. Eng.
Design Survey Engineer

**CALHEX INDUSTRIES LTD.**9515-48th STREET S.E., Calgary, Alberta, T2C 2R1

Bus: (403) 225 - 4395 {CALHEX 5}

Fax: (403) 261 - 2761

WELDING PROCEDURE SPECIFICATION NO.: _____ CX-2N (Rev.1)

WELDING PROCEDURE QUALIFICATION RECORD NO. (S): _____ PQ4, PQ5, PQ16

QUALIFIED FOR

Base Metal (Typical): _____ P1 Groups 1 & 2 to P1 Groups 1 & 2
(SA 333 Gr. 6, SA 350 Gr. LF2, SA 420 WPL6, SA 516 Gr. 70, etc.)
Process(es): _____ SMAW Weld Types: _____ GROOVE & FILLET
Position: _____ ALL POSITIONS Diameter: _____ ALL DIAMETERS
Filler Metal: _____ E6010, E7018-1

BASE METAL CONDITIONS & GROOVE THICKNESS RANGE QUALIFIED:

BASE METAL THICKNESS RANGE

NOTCH TOUGHNESS APPLICATIONS TO -46°C AS WELDED

3.2 to 203 mm (0.125 to 8.00 in.) inclusive

COMBINED DEPOSITED WELD METAL THICKNESS

ASME B31.1 _____ 19.1 mm (0.750 in.) maximum

ASME B31.3 _____ 19.1 mm (0.750 in.) maximum

ASME SECT. VIII, DIV.1 _____ 38.1 mm (1.50 in.) maximum

ALBERTA BOILERS SAFETY ASSOCIATION

PROVINCE OF ALBERTA

SAFETY CODES ACT

WELDING PROCEDURE

Reg. No. WP _____ 2380.2

Spec No. _____ CX-2N (REV.1)

Weld Process _____ SMAW

Matl. Gr. P No. _____ 1 Gr. 1+2 to P No. _____ 1 Gr. 1+2

Elec. Gr. F No. _____ 3+4 A No. _____ 1

Th. Qual. For _____ 3.2 to 203 mm PWHT _____ NO

_____ CVN - 46°C

Yr. _____ Mo. _____ Day _____ Signed _____

R. ROSEBERG, P.ENG.
WELDING SPECIALIST

PROVINCIAL REGISTRATION

WELDERS LOG

[illegible]

Alberta

LABOUR

Form No. CB-43 (90/97)

Grade "B" Pressure Welders
Certificate of Competency

Glen D. Hansen

This is to Certify that
having complied with provisions of the Boilers and Pressure Vessels Act is
hereby granted a Grade "B" Pressure Welder's Certificate of Competency, and
is authorized to engage in pressure welding in accordance with the prescribed
Regulations.



Dated at Edmonton, this Second
day of April 19 91

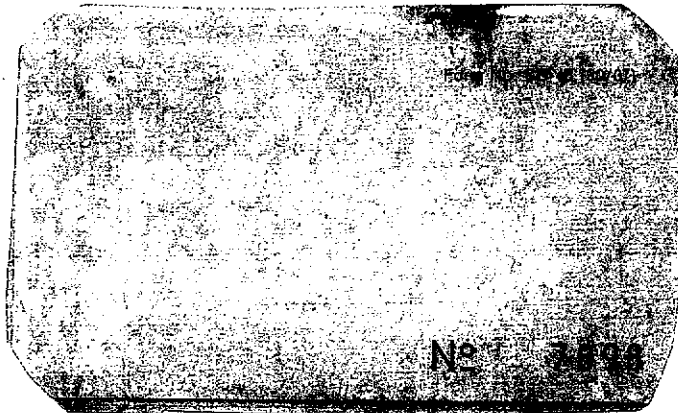
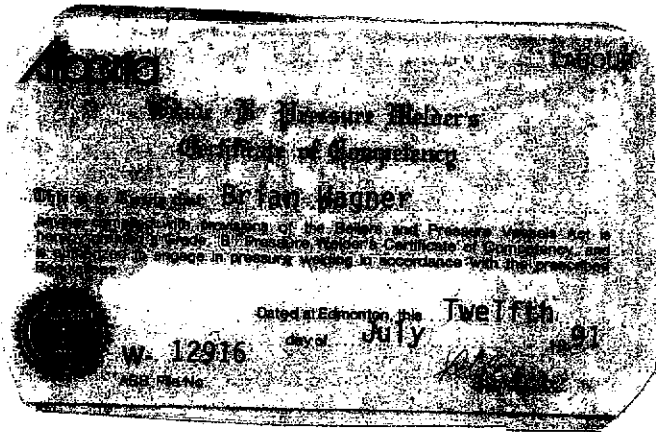
W- 12138

ABB File No.

Chief Inspector

No 7772

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CALHEX INDUSTRIES LTD.

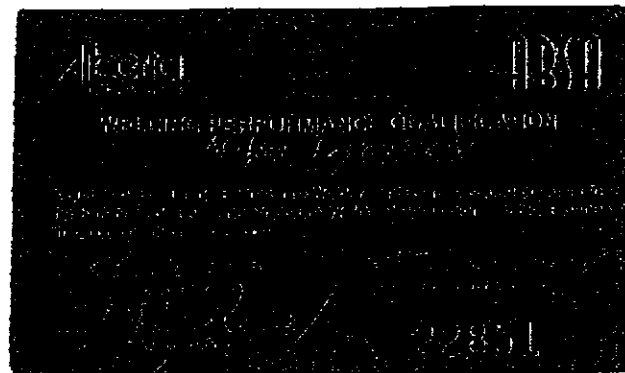
9515 - 48 th. Street S.E., Calgary, Alberta, T2C 2R1

Bus: (403) 225 - 4395 { CALHEX5 }

Fax: (403) 261 - 2761

WELDERS LOG

WELDERS NAME / FILE NUMBER	SYMBOL	PROCESS	BASE METALS	FILLER METAL "F" NUMBER(S)	BACKING	MINIMUM OD (in)	DEPOSIT THICKNESS (in)	POSITIONS	UPHILL / DOWNHILL	CORED / SOLID	INSERT	BACKING GAS	GTAW CURRENT	GMAW X-FER	EXPIRY DATE P.Q. CD.
Mike Tarantov W-22851	G	GMAW	P1	6	Optional	1	0.110"	0-45°	Vertical Down	N.A.	N.A.	N.A.	N.A.	S.C.	Dec. 2 - 2012
		SMAW	P1	4	Required	2.875"	0.488"	Flat	N.A.	N.A.	N.A.	N.A.	N.A.	N.A.	Dec. 2 - 2012
		SMAW	P1	3	Optional	1	0.250"	All	Vertical Up	N.A.	N.A.	N.A.	N.A.	N.A.	Dec. 2 - 2012
		SMAW	P1	4	Required	1	MAX	All	Vertical Up	N.A.	N.A.	N.A.	N.A.	N.A.	Dec. 2 - 2012
		GMAW	P1 or P8 - P8	6	Optional	1	0.110"	0-45° Flat	Vertical Down	N.A.	N.A.	Optional	N.A.	S.C.	Sept. 1, 2011
		SMAW	P1 or P8 - P8	5	Required	1	0.488"	Flat	Uphill	N.A.	N.A.	N.A.	N.A.	N.A.	Sept. 1, 2011
		GTAW	P1	6	Optional	2.875"	0.200"	Flat / Vertical	Uphill	N.A.	N.A.	Optional	DCEN	N.A.	April 15, 2010
		SMAW	P1	4	Required	2.875"	0.800" max	Flat / vertical	Uphill	N.A.	N.A.	N.A.	N.A.	N.A.	April 15, 2010
		GTAW	P1	6	Optional	1	0.188"	All	Uphill	N.A.	N.A.	Optional	DCEN	N.A.	May 4, 2012
		SMAW	P1	4	Required	1	0.684"	All	Uphill	N.A.	N.A.	N.A.	DCEN	N.A.	May 4, 2012
		GTAW	P1 or P8 - P8	6	Optional	2.875"	0.500"	Flat	N.A.	N.A.	N.A.	Required	DCEN	N.A.	May 4, 2012
		SMAW	P1 or P8 - P8	5	Required	2.875"	Max.	Flat	N.A.	N.A.	N.A.	Required	DCEN	N.A.	May 4, 2012
		GTAW	P10H to P10H	6	Optional	2.875"	0.200"	Flat	N.A.	N.A.	N.A.	Required	DCEN	N.A.	Aug. 7, 2012
		SMAW	P10H to P10H	5	Required	2.875"	0.274"	Flat	N.A.	N.A.	N.A.	Required	N.A.	N.A.	Aug. 7, 2012
		GMAW (STT)	P10H to P10H	6	Optional	2.875"	0.110"	0-45° Flat	Vertical Down	N.A.	N.A.	Required	N.A.	N.A.	Aug. 5, 2012
		SMAW	P10H to P10H	5	Required	2.875"	0.664"	Flat	N.A.	N.A.	N.A.	N.A.	N.A.	S.C.	Aug. 5, 2012
		GMAW (STT)	P10H to P10H	6	Optional	2.875"	0.110"	30°-60° Flat	Vertical Down	N.A.	N.A.	Required	N.A.	N.A.	Aug. 23, 2012
		SMAW	P10H to P10H	5	Required	2.875"	Max.	Flat	N.A.	N.A.	N.A.	N.A.	N.A.	S.C.	Aug. 23, 2012





9515 - 48 th. Street S.E., Calgary, Alberta, T2C 2R1

Fax: (403) 261 - 2761

[illegible]

Alberta
Municipal Affairs
and Housing

23875

Grade "B" Pressure Welder's

Certificate of Competency

This is to certify that **Michael Montgomery**
having complied with provisions of the Safety Codes Act, is authorized to engage
in pressure welding in accordance with the prescribed Regulations.

ADSA
the pressure equipment safety authority



W-23875

File no.

City of Edmonton
December 01, 2009

[Signature]
Chief Inspector and Administrator

FORM U-1 MANUFACTURER'S DATA REPORT FOR PRESSURE VESSELS (2010)
As Required by the Provisions of the ASME Boiler and Pressure Vessel Code Rules, Section VIII, Division 1

A 626024

1. Manufactured and certified by **CALHEX INDUSTRIES LTD. 9515 48TH STREET S.E., CALGARY, ALBERTA, CANADA T2C 2R1**
(Name and address of Manufacturer)

2. Manufactured for **Husky Oil Operations Ltd. 707 - 8th Avenue S.W. Calgary, AB T2P 1H5**
(Name and address of Purchaser)

3. Location of installation **Husky Oil Ansell Gas Plant Edson, AB LSD# - 07-27-051-19-W5M**
(Name and address)

4. Type **Horizontal** **Heat Exchanger** **12-0779**
(Horizontal, vertical, or sphere) (Tank, separator, jkt. vessel, heat exh., etc.) (Manufacturer's serial number)

V9688.21 **12-0779-S Rev. 0 & T Rev. 0** **2012**
(CRN) (Drawing No.) (National Board Number.) (Year Built)

5. ASME Code, Section VIII, Div. 1 **2010 & 2011** **2714**
(Edition and Addenda (date)) (Code Case Number) (Special Service per UG-120(d))

Items 6-11 incl. to be completed for single wall vessels, jackets of jacketed vessels, shell of heat exchangers, or chamber of multi-chamber vessels.

6. Shell (a) Number of course(s): **2** (b) Overall length (ft & in.): **47' - 8.750"**

Course(s)			Material	Thickness		Long. Joint (Cat. A)			Circum. Joint (Cat. A, B, & C)			Heat Treatment	
No.	Diameter, in.	Length (ft & in.)	Spec./Grade or Type	Nom.	Corr.	Type	Full, Spot, None	Eff.	Type	Full, Spot, None	Eff.	Temp.	Time
1	23"	39' - 8.750"	SA333-6	0.500"	0.0625"	S	None	0.85	7/1	Spot *	0.70	-	-
1	23"	8' - 0"	SA333-6	0.500"	0.0625"	S	None	0.85	7/1	Spot *	0.70	-	-

7. Heads: (a) (b)

(Material spec. number, grade or type) (H.T. - time & temp.) (Material spec. number, grade or type) (H.T. - time & temp.)

	Location (Top, Bottom, Ends)	Thickness		Radius		Elliptical Ratio	Conical Apex Angle	Hemispherical Radius	Flat Diameter	Side to Pressure		Category A		
		Min.	Corr.	Crown	Knuckle					Convex	Concave	Type	Full, Spot, None	Eff.
(a)														
(b)														

If removable, bolts used (describe other fastening)

8. Type of jacket **Jacket closure** (Describe as ogee and weld, bar, etc.)

If bar, give dimensions If bolted, describe or sketch.

9. MAWP **400** **15** psi at max. temp. **163** **163** °F Min. design metal temp. **-49** °F at **400** psi.
(Internal) (External) (Internal) (External)

10. Impact test **No. exempt per UCS-66(a)(c)(d)(Kg), Fig. UCS-66 Note (c) & UCS-67(a)2.** at test temperature of **-** °F.
(Indicate yes or no and the component(s) impact tested)

11. Hydro., pneu., or comb. test pressure **520 psi** Proof test **-**

Items 12 and 13 to be completed for tube sections.

12. Tubesheet: **SA516-70N** **23"** **1.5625"** **0.125"** **Welded**
(Stationary (material spec. no.)) (Diameter, (subject to press.)) (Nominal thickness) (Corr. Allow.) (Attachment (welded or bolted))

(Floating (material spec. no.)) (Diameter) (Nominal thickness) (Corr. Allow.) (Attachment)

13. Tubes **SA179 **** **0.750"** **16 BWG** **440** **Straight**
(Material spec. no., grade or type) (O.D.) (Nominal thickness) (Number) (Type (straight or U))

Items 14-18 incl. to be completed for inner chambers of jacketed vessels or channels of heat exchangers.

14. Shell: (a) No. of course(s) **2** (b) Overall length (ft & in.): **2' - 10"**

Course(s)			Material	Thickness		Long. Joint (Cat. A)			Circum. Joint (Cat. A, B, & C)			Heat Treatment	
No.	Diameter	Length	Spec./Grade or Type	Nom.	Corr.	Type	Full, Spot, None	Eff.	Type	Full, Spot, None	Eff.	Temp.	Time
2	23"	1' - 5"	SA333-6	0.500"	0.0625"	S	None	1.0	1/7	Spot *	0.70	-	-

15. Heads: (a) **SA350-LF2 CL.1** (b) **SA350-LF2 CL.1**
(Material spec. number, grade or type) (H.T. - Time & Temp.) (Material spec. number, grade or type) (H.T. - Time & Temp.)

	Location (Top, Bottom, Ends)	Thickness		Radius		Elliptical Ratio	Conical Apex Angle	Hemispherical Radius	Flat Diameter	Side to Pressure		Category A		
		Min.	Corr.	Crown	Knuckle					Convex	Concave	Type	Full, Spot, None	Eff.
(a)	End	2.75"	0.0625"						36"					
(b)	End	2.75"	0.0625"						36"					

If removable, bolts used (describe other fastening).

(24) 1.50" x 9.250" Lg. SA193-B7 UNC Studs / (48) 1.50" SA194-2H UNC Nuts
(Material spec. number, grade, size, number)

FORM U-1 (Back)

16. MAWP 400 15 psi at max. temp. 158 158 °F Min. design metal temp. -49 °F at 400 Psi
 (Internal) (External) (Internal) (External)
17. Impact test No, exempt UCS-66(a)(c)(d)(g), Fig. UCS-66 Note (c) & UCS-67(a)2. at test temperature of - °F.
 (Indicate yes or no and the component(s) impact tested)
18. Hydro., pneu., or comb. test press. 520 psi Proof test -
19. Nozzles, inspection, and safety valve openings:

Purpose (Inlet, Outlet, Drain, etc.)	No.	Diameter or Size	Flange Type	Material		Nozzle Thickness		Reinforcement Material	Attachment Detail		Location (Insp. Open.)
				Nozzle	Flange	Nom.	Corr.		Nozzle	Flange	
Shellside Inlet	1	8" 300 CL	RFWN	SA333-6	SA350-LF2 CL.1	0.344"	0.0625"	SA516-70N	UW16.1c	BW	Shell Top
Shellside Outlet	1	8" 300 CL	RFWN	SA333-6	SA350-LF2 CL.1	0.344"	0.0625"	SA516-70N	UW16.1c	BW	Shell Bottom
Tubeside Inlet	1	8" 300 CL	RFWN	SA333-6	SA350-LF2 CL.1	0.344"	0.0625"	SA516-70N	UW16.1c	BW	Channel Bottom
Tubeside Outlet	1	8" 300 CL	RFWN	SA333-6	SA350-LF2 CL.1	0.344"	0.0625"	SA516-70N	UW16.1c	BW	Channel Top
T.I.	4	1"	CPLG	SA350-LF2 CL.1	-	6000 CL	0.0625"	-	UW16.1a	-	Inlets/Outlets
P.I.	4	¾"	CPLG	SA350-LF2 CL.1	-	6000 CL	0.0625"	-	UW16.1a	-	Inlets/Outlets
Vent	1	1"	CPLG	SA350-LF2 CL.1	-	6000 CL	0.0625"	-	UW16.1a	-	Channel Top
Drain	1	1"	CPLG	SA350-LF2 CL.1	-	6000 CL	0.0625"	-	UW16.1a	-	Channel Bottom

20. Supports: Skirt No Lugs 4 Legs n/a Other Saddles Attached Welded to Shell & Channel Covers
 (Yes/no) (Number) (Number) (Describe) (Where and how)

21. Manufacturer's Partial Data Reports properly identified and signed by Commissioned Inspectors have been furnished for the following items of the report:
 (list the name of part, item number, Manufacturer's name and identifying number):

22. Remarks: (2) 24" 300 CL RFWN Channel Flanges - SA350-LF2 CL.1

SAFETY VALVES: P.S.V. on piping per UG-125 (g) to be installed by owner. CUBIC CAPACITY: 123.04 cu. ft.

SURFACE AREA: 4146.9 sq. ft.

SERVICE: Inlet Gas Heat Exchanger * RT2 - Spot per UW-11(a)(5)(b). ** Tube Length - 48' - 0" Lg.

ITEM #: E-102B Constructed to Drawing # 12-0779-S Rev. 1 & T Rev. 0.

CERTIFICATE OF SHOP COMPLIANCE

We certify that the statements made in this report are correct and that all details of design, material, construction, and workmanship of this vessel conform to the ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1.

U Certificate of Authorization Number.

33238

Expires

April 22

, 20 14

Date DEC 14 2012 Name

Calhex Industries Ltd.

Signed

(Manufacturer)

(Representative)

CERTIFICATE OF SHOP INSPECTION

I, the undersigned, holding a valid commission issued by the National Board of Boiler and Pressure Vessel Inspectors and/or the State or Province of ALBERTA and employed by ABSA of CALGARY, AB, CANADA have inspected

the pressure vessel described in this Manufacturer's Data Report on

, 20 14, and state that, to the best of my knowledge and belief, the

Manufacturer has constructed this pressure vessel in accordance with ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. By signing this certificate neither the Inspector nor his/her employer makes any warranty, expressed or implied, concerning the pressure vessel described in this Manufacturer's Data Report. Furthermore, neither the Inspector nor his/her employer shall be liable in any manner for any personal injury or property damage or a loss of any kind arising from or connected with this inspection.

Date DEC 14 2012 Signed

(Authorized Inspector)

Commissions

NB14678 AB428
 (National Board (incl. endorsements), State, Province, and number)

CERTIFICATE OF FIELD ASSEMBLY COMPLIANCE

We certify that the statements on this report are correct and that the field assembly construction of all parts of this vessel conforms with the requirements of ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1.

U Certificate of Authorization Number

Expires

, 20

Date Name

Signed

(Assembler)

(Representative)

CERTIFICATE OF FIELD ASSEMBLY INSPECTION

I, the undersigned, holding a valid commission issued by the National Board of Boiler and Pressure Vessel Inspectors and/or the State or Province of _____ and employed by _____ of _____

have compared the statements in this Manufacturer's Data Report with the described pressure vessel and state that parts referred to as data items

not included in the certificate of shop inspection, have been inspected by me and to the best of my knowledge and belief, the Manufacturer has constructed and assembled this pressure vessel

in accordance with ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. The described vessel was inspected and subjected to a hydrostatic test of _____ psi. By

signing this certificate neither the Inspector nor his/her employer makes any warranty, expressed or implied, concerning the pressure vessel described in this Manufacturer's Data Report.

Furthermore, neither the Inspector nor his/her employer shall be liable in any manner for any personal injury or property damage or a loss of any kind arising from or connected with this inspection.

Date Signed

Commissions

(Authorized Inspector)

(National Board (incl. endorsements), State, Province and number.)

**CALHEX INDUSTRIES LTD.**

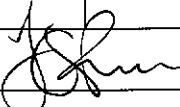
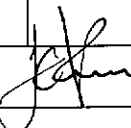
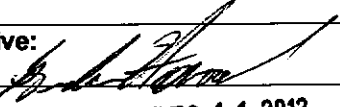
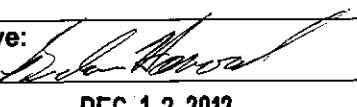
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Bus: (403) 225 - 4395

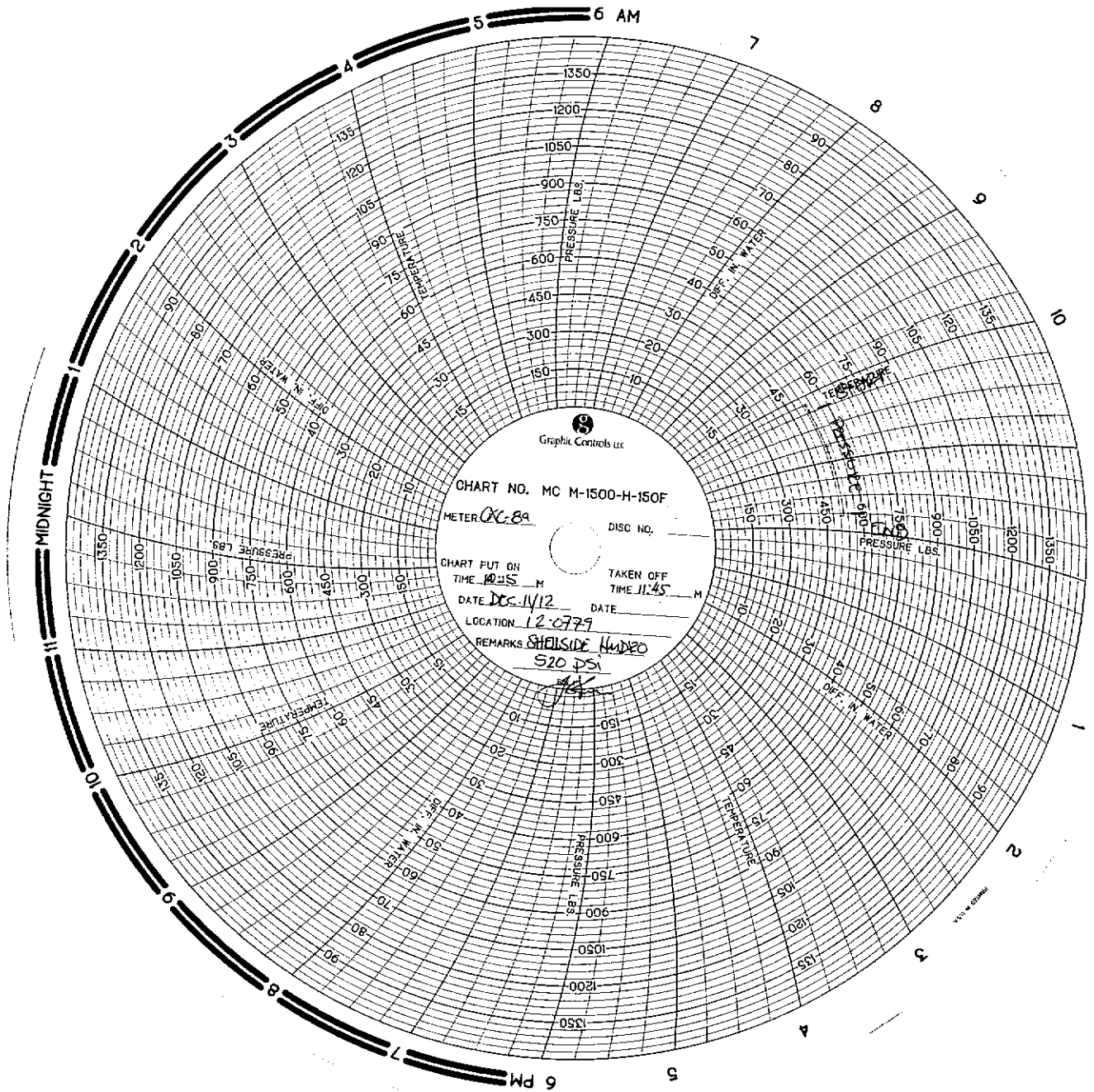
{ CALHEX5 }

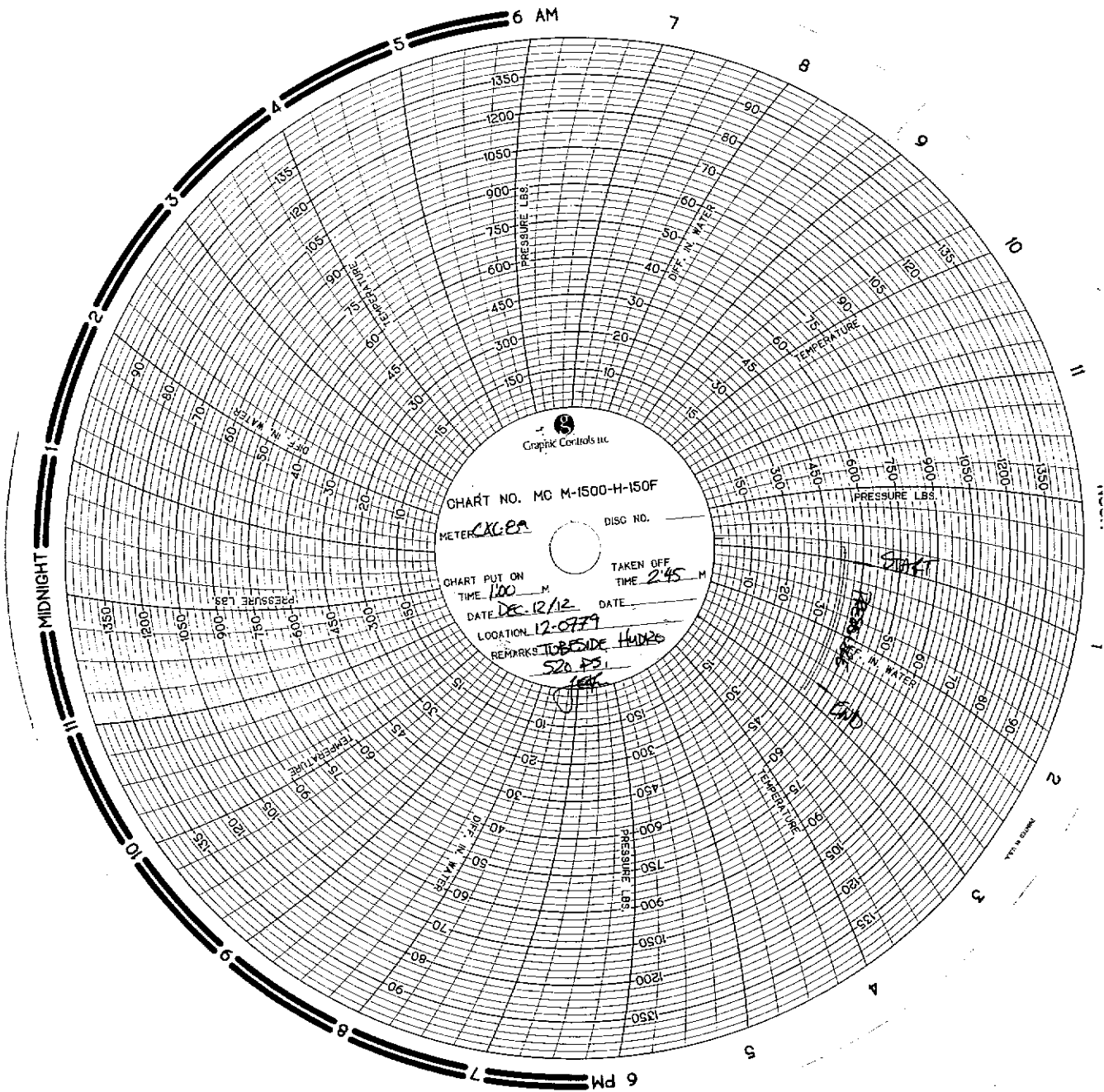
Fax: (403) 261 - 2761

HYDROSTATIC TEST REPORT

CUSTOMER:		Excelsior Engineering	
OWNER:		Husky Oil Operations	
ITEM #:		E-102B	
JOB #:		12-0779	
		SHELLSIDE	TUBESIDE
DESIGN PRESSURE:		400 psi	400 PSI
HYDROSTATIC TEST PRESSURE:		520 PSI	520 PSI
	DATE:	DEC 11 2012	DATE: DEC 12 2012
Calhex Representative: 		Calhex Representative: 	
Customer Representative: 		Customer Representative: 	
DATE: DEC 11 2012		Date: DEC 12 2012	
Gauges - CXG-2 & CXG-39		Gauges - CXG-2 & CXG-39	
Remarks:			
Hydro-tested min. 1 hour. No leaks detected.			







**CALHEX INDUSTRIES LTD.**

9515- 48 th. Street S.E., Calgary, Alberta, T2C 2R1

Bus: (403) 225 - 4395

{CALHEX5}

Fax: (403) 261 - 2761

TRAVEL SHEET (FRONT)

DO NOT START CONSTRUCTION WITHOUT AI REVIEW										TRAVEL SHEET REVISION NO.: 0	
AI REVIEW: <u>NA</u>		REVIEW DATE: NOV 12 2012									
Customer:	Excelsior Engineering	OWNER:	Husky Oil Operations	PROJECT:	Ansell Gas Plant	PO#	8400547676				
SERIAL NO.: 12-0779		JOB NO.: 12-0779-S & T		VESSEL TYPE: Inlet Gas Heat Exchanger		Tag# E-102B					
DRAWING NO.: 12-0779-S&T		DWG. REVISION NO.: 0 & 0		TRAVEL SHEET INITIATION BY: <u>JK</u>				NOV 10 2012			
Seq.	Item	Comments	Q.C.I.	Date	A.I. Hold Points	A.I.	Date	Owner / Customer Rep.	Date		
1.	Calculations in File	Approved by Customer and ABSA	<u>OK</u>	NOV 10 2012		TD DEC 14 2012		* <u>NA</u> 03 Dec 2012			
2.	Release of App'd Dwg.	Approved by Customer and ABSA	<u>OK</u>	NOV 10 2012		NA NOV 12 2012		* <u>NA</u> 03 Dec 2012			
3.	Heat Numbers Recorded	2010 Edition 2011 add	<u>OK</u>	DEC 11 2012		NA DEC 11 2012		* <u>NA</u> 12 Dec 2012			
4.	MTRs Checked		<u>OK</u>	DEC 11 2012		TD DEC 14 2012		* <u>NA</u> 12 Dec 2012			
5.	Examination of Material (UG-93)		<u>OK</u>	DEC 11 2012							
6.	WPS(s) Checked	(-49 °F) Lot# <u>12829H2</u>	<u>OK</u>	DEC 11 2012				* <u>NA</u> 17 Dec 2012			
7.	Welder(s) Qualified		<u>OK</u>	DEC 11 2012				* <u>NA</u> 17 Dec 2012			
8.	Thicknesses Verified & Recorded		<u>OK</u>	DEC 11 2012		TD DEC 14 2012		* <u>NA</u> 12 Dec 2012			
9.	Shell(s) & Head(s) Fit-up Inspection		<u>OK</u>	DEC 11 2012		TD DEC 12 2012		* <u>NA</u> 12 Dec 2012			
10.	Nozzles & Fittings Fit-up Inspection		<u>OK</u>	DEC 11 2012							
11.	Nozzle Orientation		<u>OK</u>	DEC 11 2012							
12.	Nozzle & Flange Rating Checked		<u>OK</u>	DEC 11 2012							
13.	Impact Testing	No, exempt per UCS-46(a)(1)&(4)&(6), Fig. UCS-46 Note (c) & UCS-47(a)(1)	N/A								
14.	Internals Checked	N1- plus All Drains to be flush	<u>OK</u>	DEC 11 2012							
15.	Final Internal Inspection	Shellside - Tubeside -	<u>OK</u>	NOV 20 2012		NA NOV 28 2012		** <u>NA</u> 11 Dec 2012			
16.	Bundle Insertion		<u>OK</u>	DEC 11 2012		NA DEC 11 2012		<u>NA</u> 11 Dec 2012			
17.	Weld Size Checked	As per weld detail	<u>OK</u>	DEC 11 2012							
18.	Welder I.D. Checked		<u>OK</u>	DEC 11 2012							
19.	Final External Inspection	2-N/P - 2-LL	<u>OK</u>	DEC 11 2012		TD DEC 12 2012		<u>NA</u> 11 Dec 2012			
20.	Radiography	Shellside - N/A PER UW 13.2(d)	N/A			TD DEC 14 2012					
a).	Radiography	Tubeside- N/A PER UW 13.2(d)	<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 12 Dec 2012			
21.	MPI- UG-93 - Tubesheets A & B Beveled Edges before welding		<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 12 Dec 2012			
	MPI- UG-93 - Tubesheets A & B Beveled Edges AFTER welding		<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 12 Dec 2012			
	UT- Cat. D's -		N/A			TD DEC 14 2012		<u>NA</u> 12 Dec 2012			
	MPI-S/S Temp's / Fillet Welds-Cat. D's - Saddle to Shell-N/P		<u>OK</u>	DEC 12 2012							
	MPI-T/S- Temp's / Fillet Welds-Cat. D's / L/R lugs		<u>OK</u>	DEC 12 2012							
	HT - <200 BHN- AFTER PWHT -		N/A								
22.	Final Ext. Prior to P.W.H.T. -		N/A								
23.	PWHT Chart Checked		N/A								
24.	Hydrostatic Test - 1 Hr Report & CHART	Shellside: Gauge: 520 psi CXG- 1 & CXG- 3A	<u>OK</u>	DEC 11 2012		NA DEC 11 2012		** <u>NA</u> 11 Dec 2012			
24.a	Hydrostatic Test - 1 Hr Report & CHART	Tubeside: Gauge: 520 psi CXG- 2 & CXG- 3A	<u>OK</u>	DEC 12 2012		TD DEC 12 2012		** <u>NA</u> 12 Dec 2012			
25.	CRN Drawing: (AB) (BC)	CRN# <u>V9125</u> - 2	<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 17 Dec 2012			
26.	N.C.R.	Approved:	<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 18 Dec 2012			
27.	Nameplate Stamping	Imp. / CAUTION	<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 18 Dec 2012			
28.	Manuf. Data Report Completed & Verified	U1 - FULL VACUUM	<u>OK</u>	DEC 12 2012		TD DEC 14 2012		<u>NA</u> 18 Dec 2012			
29.	Nameplate Installation	IMP / Caution	<u>OK</u>	DEC 18 2012				<u>NA</u> 18 Dec 2012			
30.	Final Paint - As per Drawing	WOOD Covers / Rust Prev.	<u>OK</u>	DEC 18 2012				<u>NA</u> 18 Dec 2012			
31.	INSULATION-		<u>OK</u>	DEC 18 2012				<u>NA</u> 18 Dec 2012			
32.	Shipping and Release		<u>OK</u>	DEC 18 2012				<u>NA</u> 18 Dec 2012			
33.	Final Documentation	Manufacturer's Data Book	<u>OK</u>	DEC 18 2012				<u>NA</u> 18 Dec 2012			

The Authorized Inspector shall be present with the Travel Sheet prior to construction so that he can designate additional inspection points and/or Hold Points. Any revisions shall be marked with a delta symbol with revision number and described at the bottom of this page.

* Denotes an A.I. Inspection Point

** Denotes an A.I. Hold Point

* Low Temp.

M

CA-TIS 0534



CALHEX INDUSTRIES LTD.

9515-48TH STREET S.E., Calgary, Alberta, T2C 2R1

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TRAVEL SHEET (BACK)

MATERIAL THICKNESS VERIFICATION AND IDENTIFICATION				WELD I.D. / WELDER SYMBOLS / FIT-UP						
Description	Thickness	Material Spec. & Grade	Heat & Plate Identifier or Material Tracking Number	Weld I.D.	Welder Symbol	Fit-Up Exam	Weld I.D.	Welder Symbol	Fit-Up Exam	Verify Type 1 Joint
Tubes	0.750" 14 BWG	SA179	193100 / 213254							
Tubesheet A	1.5625" (1.568")	SA516-70N	B663				C3	J	JOK	JOK
Tubesheet B	1.5625" (1.570")	SA516-70N	B663				C5	J	JOK	JOK
Shell Cylinder	24" XH (.514")	SA333-6	B959				C4	G	JOK	JOK
Chan. Cylinder	24" XH (.514")	SA333-6	B959				C2	J	JOK	JOK
Channel Cover	24" 300 CL RF BL	SA350-LF2 CL.1	198658							
Channel RFWN	24" 300 CL RFWN	SA350-LF2 CL.1	H0742/3				C1	B	JOK	JOK
Chan. Cylinder	24" XH (.514")	SA333-6	B959				C6	J	JOK	JOK
Channel Cover	24" 300 CL RF BL	SA350-LF2 CL.1	198658							
Channel RFWN	24" 300 CL RFWN	SA350-LF2 CL.1	H0742/3				C7	A	JOK	JOK
Saddle Repad	0.375" (.390")	SA516-70N	B947							
Saddle Repad	0.375" (.390")	SA516-70N	B947							
Saddle Repad	0.375" (.390")	SA516-70N	B947							

ATTACHMENT AND / OR NOZZLE MATERIAL THICKNESS VERIFICATION AND IDENTIFICATION						WPS# / WELDER SYMBOLS / FIT-UP			
Mark	Mat. I.D.	Neck	Fitting	Flange	Repad or Attachment	Cat. B	Cat. C	Cat. D	Pad OD
N1 C1b C2b	Spec.-Grd.	SA333-6	SA350-LF2 CL.1	SA350-LF2 CL.1	SA516-70N		A A	J J	12.625"
	Thk./Rating	8" XH (.527")	1" 8 3/4" 6000 CL CPLG	8" 300 CL RFWN	0.250" (.245")			B B	
	Heat# or ID	B368	403B / 404B	12/30011	B998		CX-1N	CX-2N	JOK
N2 C1c C2c	Spec.-Grd.	SA333-6	SA350-LF2 CL.1	SA350-LF2 CL.1	SA516-70N		A A	J J	12.625"
	Thk./Rating	8" XH (.527")	1" 8 3/4" 6000 CL CPLG	8" 300 CL RFWN	0.250" (.245")			B B	
	Heat# or ID	B368	403B / 404B	12/30011	B998		CX-1N	CX-2N	JOK
N3 C1d C2d	Spec.-Grd.	SA333-6	SA350-LF2 CL.1	SA350-LF2 CL.1	SA516-70N		A A	J J	12.625"
	Thk./Rating	8" XH (.527")	1" 8 3/4" 6000 CL CPLG	8" 300 CL RFWN	0.250" (.245")			B B	
	Heat# or ID	B368	403B / 404B	12-30011	B998		CX-1N	CX-2N	JOK
N4 C1a C2a	Spec.-Grd.	SA333-6	SA350-LF2 CL.1	SA350-LF2 CL.1	SA516-70N		A A	J J	12.625"
	Thk./Rating	8" XH (.527")	1" 8 3/4" 6000 CL CPLG	8" 300 CL RFWN	0.250" (.245")			B B	
	Heat# or ID	B368	403B / 404B	12-30011	B998		CX-1N	CX-2N	JOK
C3a	Spec.-Grd.		SA350-LF2 CL.1					A J	
	Thk./Rating		1" 6000 CL CPLG						
	Heat# or ID		403B					CX-2N	JOK
C3b	Spec.-Grd.		SA350-LF2 CL.1					A J	
	Thk./Rating		1" 6000 CL CPLG						
	Heat# or ID		403B					CX-2N	JOK
	Spec.-Grd.								
	Thk./Rating								
	Heat# or ID								



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***PROCOAT COATINGS LTD
QUALITY CONTROL INSPECTION REPORT***

DATE: December 18, 2012

CUSTOMER: Calhex Industries Ltd.

CUSTOMER JOB: 12-0779

PROCOAT WORK ORDER #: 1010-12-12

ITEM DESCRIPTION: (1) Vessel (NEN 23 x 576 – 25500lbs)





PROCOAT COATINGS LTD SURFACE PREPARATION INSPECTION REPORT

DATE: December 13, 2012

INSPECTION

SANDBLASTER: James

SURFACE PREP: SSPC-SP6

PROFILE THICKNESS: 2.5 - 3.0mils

ABRASIVE USED: 30/50 Silica

EQUIPMEN: 375 CFM Compressor

NOZZLE: #6

COMMENTS: Surface preparation met SPEC requirement and the project was released for coating.

SURFACE PREP CONDITIONS

AIR TEMP: 2°C

SUBSTRATE TEMP: 1.5°C

RELATIVE HUMIDITY: 29%

DEW POINT: -13°C

Procoat Coating Inspection Report

Date	13-Dec-12	13-Dec-12		
Coat	1st	2nd		
Avg.	1.8	3.8		
DFT(mil) High	2	4.2		
Low	1.6	3.3		
No. of reads	263	244		
Applicator	Lloyd	Lloyd		
Product	Rust-oleum Industrial Choice	Rust-oleum Enamel		
Color	Grey	Silver Grey		
Batch #	206331	245484		
	P25151	P20242		
Air Temp (C)	23	23		
Steel Temp(C)	23	23		
Humidity (%)	29%	29%		
Dew Point (C)	-13	-13		
Comments:				